To: James Merten, PE, City of Neenah, City Traffic Engineer
From: Eric Frailing, PE, PTOE, MSA Professional Services, Inc.
Brian Huibregtse, PE, PTOE, MSA Professional Services, Inc.
Subject: Winneconne Ave \& Commercial St Intersection Control Evaluation Summary
Date: February 22, 2023

## INTRODUCTION

MSA Professional Services, Inc. (MSA) was asked to complete an intersection control evaluation (ICE) for the intersection of Winneconne Avenue at Commercial Street, in Neenah, Wisconsin (city). The west ${ }^{1}$ and north legs of the intersection are also part of STH 114 as well as the Wisconsin Department of Transportation (WisDOT) Connecting Highways system.

The intersection was identified by the city as having ongoing issues with safety, operations, and capacity and was targeted for investigation of potential improvements. Initial operation reviews indicated regular queues of 200 - 300-feet on all approaches with the existing configuration and traffic signal control. The southbound right-turn movement was calculated to be nearing capacity under current conditions. Over the last five years of available crash data, the intersection experienced 34 crash events. The eastbound approach experienced eight front-to-rear (rear-end)-type of crashes, the most of any other approach or crash manner. Of the 34 crash events, eight involved injuries, none of which were worse than severity level B (suspected minor injury). No fatalities were reported during the period. Roadway conditions were noted as a possible factor in at least ten of the overall crashes (snow, slush, ice, or wet pavement). Failure to yield was cited in 11 of the overall crashes.

In order to identify viable alternatives and ultimately recommend one for improving operations and safety, Phase I and Phase II ICE reports were completed for the intersection, following WisDOT reporting standards.

## PHASE IICE

The Phase I ICE investigation focused on determining what potential improvements were viable for the intersection based on a high-level review of the identified issues and space available. Results from the Phase I analyses indicated the following alternatives were viable and should be analyzed further as part of a more detailed Phase II ICE report:

[^0]1. Modified Traffic Signal - Lane modifications and updated signal phasing
2. Roundabout, 4-Leg - Convert the existing intersection into a multilane roundabout
3. Roundabout, 5-Leg - Convert the existing intersection into a multilane roundabout which realigns Church Street to be part of the main intersection.

## PHASE II ICE

The Phase II ICE investigation used the viable alternatives from the Phase I ICE report and looked more in-depth at existing (2022) design year (2042) operations, projected safety performance using the Interactive Highway Safety Design Model (IHSDM) procedures, conceptual level intersection layouts, business and right-of-way (R/W) impacts, and estimated construction costs. Conceptual layouts for the three alternatives are included in the Phase II ICE report.

Results of the analyses indicated that all alternatives are expected to provide acceptable levels of operation (delay, queue, and capacity) through the design year. The roundabout alternatives are expected to provide the most significant and longest-lasting operational and capacity benefits but would cost the most to construct and would have the greatest R/W and business impacts. Including estimated R/W acquisition costs, the four-leg roundabout alternative is expected to cost $\$ 1.8$ million more than the modified traffic signal alternative. Both roundabout alternatives would require the purchase of the entire parcel in the northwest corner of the intersection, whereas the modified traffic signal would only require a small strip of R/W to be acquired. The roundabouts would also require the purchase and relocation of the commercial pylon signs for parcels in the north and southeast corners, in addition to relocation of the "Welcome to Historic Downtown Neenah" monument sign and adjacent flagpole. These impacts are shown in Figure 1 and Figure 2.


Figure 1, The existing monument sign, flagpole, and commercial pylon sign in the northeast corner


Figure 2, The existing commercial pylon sign in the southeast corner

For safety and geometric constraint reasons, access between Winneconne Avenue and Church Street would be restricted to right-in/right-out movements only for the modified traffic signal and 4-leg roundabout alternatives. The existing intersection of Winneconne Avenue at Church Street
is within the functional area of the intersection of Winneconne Avenue at Commercial Street. This proximity results in a larger number of conflict points (places where vehicle paths overlap) in a smaller area, which results in a higher probability for crashes to occur.

The roundabout alternatives are expected to generate the largest numbers of crashes, showing an increase over the no-build alternative. Recent studies have shown increases in the overall number of crashes occur when multilane roundabouts are constructed; however, the magnitude of injuries are lower than other intersection types. Due to the geometric design of a roundabout, the most severe manners of collision (head-on and T-bone) which result in K and A -level severity injuries (fatal and suspected serious injury), are all but completely eliminated. Other intersection types such as stop or traffic signal control do not have physical barriers preventing vehicles from colliding in this manner, while also allowing for faster approach speeds prior to any impact.

When construction costs and projected safety benefits are compared, the modified traffic signal alternative has a benefit/cost ratio of 0.46; the 4-leg roundabout alternative is -2.47. (Note, due to limitations of the IHSDM, a benefit/cost ratio for a 5-leg roundabout is not able to be calculated. It is expected to be lower than the 4-leg alternative.)

The 5-leg roundabout alternative is the only alternative that does not have a significant impact to the Valley Transit (Route 32) line that uses Winneconne Avenue and Church Street. Turn movement restrictions would require at least part of the bus route to be moved to a different street in order to access northbound Church Street with the modified traffic signal alternative. The 5-leg roundabout alternative would still allow direct access to northbound Church Street within the intersection. Indirect access to northbound Church Street would be allowed with the 4-leg roundabout alternative; however, this would require the bus to make a U-turn at the roundabout in order to turn right onto northbound Church Street.

## CONCLUSIONS

Conclusions discussed below are based on the results of the alternatives considered in the Phase II ICE investigation. Development changes being considered for the adjacent properties could allow for some modifications of the alternatives investigated as part of the formal Phase II ICE. Additional analysis would be necessary to determine the impacts "fine tuning" the proposed alternatives, such as modifications of downstream lane configurations (lane reductions/merges) or other geometric adjustments and could be done as a preferred alternative is selected.

Based on the raw results of the Phase II ICE investigation, the modified traffic signal is the preferred option. The modified traffic signal has the best benefit/cost ratio, reduces the expected number of crashes, results in the least amount of R/W impacts, and does not require any businesses to be acquired. Unlike the roundabout alternatives, the modified traffic signal has reduced operations (higher delay and queues, lower residual capacity). The modified traffic signal improves on existing operations through the design year, just not to the same extent as the roundabout alternatives. The modified traffic signal alternative does not significantly reduce the likelihood of severe crashes (injury level B, A, or fatalities (K)). However, in the last five years, crashes of this injury magnitude were not reported.

In order to accommodate the design vehicle movements along the STH 114 portions of the intersection, the stop bars for the southbound and eastbound approaches need to be relocated upstream of the intersection in order to allow the design vehicles enough room to complete their
maneuvers. The eastbound stop bar could remain in its current location; however, in order to accommodate the southbound right turn, additional R/W would be necessary as well as the relocation of at least one significant utility pole.

Restricting access to Church Street down to right-in and right-out movements will impact the existing Route 32 Valley Transit bus line, as it currently turns left from eastbound Winneconne Avenue onto northbound Church Street. The bus line would need to be modified to accommodate this new restriction. Several potential alternatives exist, including:

- Moving northbound operations to Commercial Street and using Church Street for southbound operations
- Relocating the eastbound left-turn to Isabella Street, then using Adams Street to reconnect with Church Street

Current cost estimates included implementing traffic signal changes necessary to accommodate the proposed lane adjustments only, as crash patterns did not indicate the need for additional signalization infrastructure changes for the other intersection approaches. Any further changes would require an increase in funding, but could all be implemented at the same time.

## Additional considerations that could be evaluated with the development of further design plans could include:

- Install a raised median on the north approach to separate the southbound right-turn lane from the through lane. The raised median would allow a place of pedestrian refuge, shortening the distance that would need to be crossed at one time, in addition to providing additional signal timing flexibility. Installation of such an island would significantly increase the alternative's impacts to the property in the northwest corner of the intersection and Church Street.
- Install a raised median on the west approach to separate the eastbound and westbound lanes. The physical barrier would better prevent left turns to and from Church Street than if regulatory signs were used alone. Addition of the median would increase the R/W impacts as well:
- Northern Shift
- No R/W would need to be acquired on the south side of the approach
- Creates additional impacts for design vehicles completing southbound right turns from Commercial Street
- Southern Shift
- Creates new R/W impacts on the south side of the road where there were few or none previously
- Allows for realignment of the eastbound left-turn lanes. This could reduce the impacts these left turns have on the southbound approach lanes.
- Upgrading to monotube and signal head-per-lane for all approaches. This would maximize signal visibility, which could further reduce the incidence of front-to-rear crashes. It would also bring the signal infrastructure to the latest WisDOT design standards. Depending on the size of poles needed, additional utility modification may be required in order to accommodate the new poles and associated foundations.
- Converting five-section, protected/permissive left-turn signals to four-section flashing yellow arrow (FYA) indications. This conversion not only offers additional crash reduction potential, but also offers more signal phasing flexibility to accommodate future growth.
- Adding pedestrian push buttons for calling pedestrian phases. Currently, the pedestrian phase is called with every green light. When there are no pedestrians present, this results in additional phase time being used for a phase that may not need it, when it could be used to instead serve other phases requiring more time. It could also allow for conflicting pedestrian phases to be served sooner. Given the existing traffic signal pole layout, additional "pedestrian button poles" may be needed in order to comply with ADA and PROWAG location regulations.
- Adding emergency vehicle preemption (EVP). EVP can allow for certain emergency vehicles to pass through the intersection faster by being able to call for their own green light indication. This equipment does require transponder equipment to be installed on each emergency vehicle in order for it to be effective. The signal infrastructure could be installed now to save implementation costs later.

Implementing some or all of the additional traffic signal modifications listed above, beyond what is required for the modified traffic signal alternative would require additional discussion and further investigation to determine a better cost estimate. Simultaneous implementation would have several benefits, including better public perception of only making modifications at one time rather than coming back later for additional work. Completing all the work at once would increase the overall implementation cost estimate, but it would have cost efficiencies with construction mobilization and necessary underground rewiring to accommodate the new signals. It could also offer additional timing flexibilities to better accommodate future growth.

Attachment A : Phase 2 ICE Report (Text \& Attachments)
Attachment B : Phase 1 ICE Report (Text Only)

## Project and Analyst Information:

| Project ID: | $\mathrm{n} / \mathrm{a}$ |
| ---: | :--- |
| Project Type: | Other |
| Location: | STH 114 (Winneconne Avenue) at STH 114 (Commercial Street) <br> City of Neenah <br> Winnebago County <br> Northeast Region |
| Analyst: | Eric Frailing, PE, PTOE |
| Agency: | MSA Professional Service, Inc |
| Date: | February 2023 |

## Background Information:

| Project Need: | Safety and Operations |
| ---: | :--- |
| Project | The objective of the proposed project is to reduce the number of severe injury crashes while <br> Obproving intersection operations. A Phase I ICE report identified three feasible alternatives for <br> further consideration to meet the proposed objectives: Modified Traffic Signal, 4-Leg Roundabout, <br> and a 5-Leg Roundabout. These intersection alternatives are evaluated in this Phase II ICE report in <br> order to determine the optimal intersection modification to meet the operational needs of the <br> intersection without sacrificing safety. |
| Additional | The City of Neenah has identified the intersection of STH 114 (Winneconne Avenue) at STH 114 <br> Information: <br> (Commercial Street) as a target for improvements due to ongoing operational/capacity and safety <br> issues. The area is surrounded by mostly commercial developments, with residential development <br> surrounding the commercial development. Valley Transit operates bus routes through the area. <br> Routes currently use all approaches of this intersection except for the east leg of the intersection. Bus <br> routes are also shown to use Church Street as well. A project location map is included in Attachment <br> 2. <br> A construction year has not been formally identified; however, it is assumed that construction is |
| desired to occur as soon as financially feasible and practical. For the purposes of completing IHSDM |  |
| analyses, a construction year of 2023 was selected, with the first year of the evaluation period (the |  |
| first year the roadway is open to traffic after the proposed construction is completed) being 2024. |  |

## Existing Crash Information:

## Observed Crash History:

A total of 34 crashes were reported at this intersection from 2017-2021. Seven of the crashes resulted in injuries. A crash diagram is provided in Attachment 3.

Years: 2017-2021

| Crash Type | Fatal | Injury A | Injury B | Injury C | KABC | PDO | Total |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Rear-End <br> (Front-to-Rear) | 0 | 0 | 0 | 2 | 2 | 14 | 16 |


| Crash Type | Fatal | Injury A | Injury B | Injury C | KABC | PDO | Total |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Angle (Front-to-Side) | 0 | 0 | 2 | 0 | 2 | 6 | 8 |
| Single Vehicle - <br> Other | 0 | 0 | 3 | 0 | 3 | 1 | 4 |
| Sideswipe - Same <br> Direction | 0 | 0 | 0 | 0 | 0 | 3 | 3 |
| Head-On (Front-to- <br> Front) | 0 | 0 | 0 | 1 | 1 | 1 | 2 |
| Sideswipe - Opposite <br> Direction | 0 | 0 | 0 | 0 | 0 | 1 | 1 |
| Total | 0 | 0 | 5 | 3 | 8 | 26 | 34 |

(add more rows as needed)

## Crash Trends:

The intersection has a significant number of front-to-rear crash events, with most occurring on the eastbound approach. The majority of this crash type were property damage only; however, two were of severity C (possible injury). Higher numbers of these crashes are common for traffic signals versus stop or yield-controlled intersections. Front-to-side crash events were the next most common, with no particular approach having a significant number of this crash type. Two of these crashes resulted in severity B (suspected minor injury) magnitude injuries. Three of the single-vehicle crashes resulted in injuries - all severity B (suspected minor injury) magnitude injuries. One of these events involved a pedestrian being struck by a southbound left-turning vehicle; one of the events involved a bicyclist being struck by a southbound right-turning vehicle.

## Contributing Factors:

Weather may have been a factor in two of the crashes (rain). Road conditions may have been a factor in at least ten crashes: five wet, three snow, one slush, and one ice. Drug impairment was cited in two crashes. Failure to yield was cited in 11 crashes. Distracted driving was identified in nine crashes. Disregard of a red light was cited in three crashes. Speed was cited in two crashes (too fast for conditions). Improper crossing was cited in the crash that involved a pedestrian.

## Additional Modes of Transportation:

| Mode | Need? <br> Yes/No | Nearby Generators and Existing Facilities | Volume |  |
| :--- | :--- | :--- | :--- | :--- |
|  |  | Yes | Sidewalk is provided on both sides of the street for all <br> approaches. Except for the eastbound channelized right-turn <br> lane, crosswalks and pedestrian signals (no call buttons) are <br> present across all approaches of the intersection. The right-turn <br> lane has a crosswalk, with a Yield sign present prior to the <br> crosswalk. No bicycle lanes are present on any of the <br> approaches, no is width available to add them with the existing <br> cross section of pavement. Several schools and parks exist just <br> outside of a quarter-mile radius of this intersection. Numerous <br> commercial businesses are present directly adjacent to the <br> intersection. | Varies |

(add more rows as needed)

Other Information: The approaches to this intersection are classified as "Major Urban Streets" by the Winnebago County Bicyclist Map. As such, bicycling conditions are not presented for these streets and "are likely to have high volumes of traffic".

## Summary Tables:

## Descriptions:

| Alt. | Traffic Control | Description of Alternative |
| :---: | :--- | :--- |
| 1 | Modified Traffic Signal | An exclusive southbound right-turn lane would be added. The eastbound <br> approach would add an additional exclusive left-turn lane and its phasing <br> would switch from protected/permissive to protected only operations. The <br> eastbound approach would also implement signal head-per-lane indications <br> to accommodate the phasing change. Church Street would be restricted to <br> right-in/right-out access. Accommodation of the design vehicles require the <br> stop bars for the eastbound and southbound left-turn lanes to be pulled <br> further upstream from the intersection in order to avoid more extensive <br> modifications and ROW acquisitions to the northwest corner. |
| 2 | Roundabout - 4-Leg | The existing intersection would be converted into a multilane roundabout <br> with two-lane approaches for all directions. Church Street would be |
| restricted to right-in/right-out access. |  |  |

Alternative concept layouts are included in Attachments 4A-C.

## Costs and Impacts:

| Alt. | Traffic Control | Construction <br> Cost | Real Estate Impacts |  |  | Environmental Impacts |  |
| :---: | :--- | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | \# Build | \# Acres | Cost | Impact Type | \# Acres |  |
| 1 | Modified Traffic <br> Signal | $\$ 272,400$ | 0 | 0.04 | $\$ 15,800$ | Choose an item. |  |
| 2 | Roundabout - 4- <br> Leg | $\$ 1,478,300$ | 1 | 0.71 | $\$ 370,700$ | Choose an item. |  |
| 3 | Roundabout - 5- <br> Leg | $\$ 1,680,500$ | 1 | 0.70 | $\$ 373,100$ | Choose an item. |  |

Environmental impact evaluations will be completed as the project progresses. Based on preliminary schematics, the roundabout alternatives are expected to have the highest impacts if environmental resources are found. Preliminary cost estimates are included in Attachment 5.

Safety Performance:

| Alt. | Traffic Control | Analysis Period | KABC | PDO | Total |
| :---: | :--- | :---: | :---: | :---: | :---: |
| - | Existing Conditions | $2017-2021$ | 8 | 26 | 34 |
| - | Future No-Build | $2024-2033$ | 17.9 | 31.6 | 49.5 |
| 1 | Modified Traffic Signal | $2024-2033$ | 16.6 | 28.8 | 45.4 |
| 2 | Roundabout -4-Leg | $2024-2033$ | 23.4 | 129.2 | 152.6 |
| 3 | Roundabout -5-Leg | $2024-2033$ | $\mathrm{n} / \mathrm{a}$ | $\mathrm{n} / \mathrm{a}$ | $\mathrm{n} / \mathrm{a}$ |

Safety performance was evaluated using safety performance functions based on Wisconsin-calibrated data in the IHSDM 2020 release for the 10-year period of 2024 to 2033.

Note that the IHSDM tool does not currently have data sets which cover 5-leg roundabouts. Based on crash frequency prediction models found in NCHRP Report $672^{1}, 5-$ leg roundabouts with two circulating lanes are expected to have higher crash frequencies for both injury and PDO crash types. Therefore, for the purpose of this report, 5-leg roundabouts will be assumed to have poorer benefit/cost ratios and higher present value of crash costs than a 4-leg roundabout.

Traffic volumes for 2031 were grown based on a conservative growth rate for background traffic determined values used in the Phase I ICE report. An economic analysis of the safety performance for the analysis period of 2024 to 2033 was also completed with the Wisconsin-calibrated data in the IHSDM. The modified traffic signal alternative has a higher Benefit/Cost ratio than either roundabout alternative:

- Alternative 1, Modified Traffic Signal: 0.46
- Alternative 2, Roundabout - 4-Leg: -2.47
- Alternative 3, Roundabout -5-Leg: <-2.47 (estimated)

The roundabout alternative is predicted to have a higher number of crashes than the modified traffic signal alternative, both from an injury/fatal event and property damage only event perspectives. However, the expected injury severity of any roundabout crashes is expected to be less than the traffic signal alternatives. Present value of crash cost for the alternatives over the 10 -year period are:

- Alternative 1, Modified Traffic Signal: \$1,688,557
- Alternative 2, Roundabout - 4-Leg: $\$ 6,604,387$
- Alternative 3, Roundabout - 5-Leg: >\$6,604,387 (estimated)

Full IHSDM analysis output is included in Attachment 6. Supporting traffic volumes and operational analyses are included in Attachments 7 and 8, respectively.

## Recommendation:

Alternative: Modified Traffic Signal
Influencing Expected operations (delay and queues) are better with either roundabout alternative, with both Factors: roundabouts expected to be able to accommodate more traffic than the modified traffic signal alternative.

The 4-leg roundabout alternative requires Church Street to intersect Winneconne Avenue within the functional area of the roundabout exit path and places the associated pedestrian crossing of Winneconne Avenue in higher-speed/more vulnerable location. The pedestrian crossing location also requires users to travel further out of their way to cross the west side of the intersection. The 5-leg roundabout alternative improves both of the aforementioned deficiencies (Church Street alignment and pedestrian crossing location). However, multilane 5-leg roundabouts are more difficult to direct motorists through without additional guide signs and spiraling lanes within the circulatory roadway.

The modified traffic signal alternative is the best alternative when compared for construction costs, business and right-of-way impacts, utility impacts, and ease (time) to implement/construct. Because

[^1]of the geometric design of the roundabout, fatal and high-level injury crashes (A and B-level) are less likely than a stop or traffic signal-controlled intersection. However, less severe injury (C-level) and property damage only crashes typically are higher for multilane roundabouts than the other intersection types.

Based on the calculated cost and safety benefits, the modified traffic signal is the preferred intersection alternative at this location.

## Existing \& Future No-Build Conditions:

Practicality:

| Public Opinion: | Formal public involvement meetings have not occurred with the proposed alternatives. <br> Complaints have been previously received regarding the current operational and safety of the <br> existing intersection configuration. |
| ---: | :--- |
| Business Impacts: | None |
| ROW Impacts: | None |
| Utility Impacts: | None |
| Cost Estimate: | $\$ 0$ |
| Additional Info: | The no-build scenario does not address the existing safety and operational issues, nor <br> concerns with future traffic volumes. |

## Safety Analysis:

Safety Performance Measures:

|  | Analysis Period | KABC | PDO | Total |
| :--- | :---: | :---: | :---: | :---: |
| Existing Conditions | $2017-2021$ | 8 | 26 | 34 |
| Future No-Build | $2024-2033$ | 17.9 | 31.6 | 49.5 |

## Operational Analysis:

| Warrant Analysis: | n/a |
| ---: | :--- |
| Queue Impacts: | Existing and projected queues are expected to impact access to existing driveways on all <br> approaches. |
| Additional Capacity: | None. At least one movement is near capacity, with several projected to be over capacity or <br> acceptable levels of delay during the design year. |
| Railroad Impacts: | None |
| Additional Info: |  |

Operational Performance Measures:

| Year: 2022 | Existing Conditions |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| AM Peak | EB |  |  | WB |  |  | NB |  |  | SB |  |  |
|  | L | T | R | L | - | T/R | L | - | T/R | L/T | - | T/R |
| \# Lanes | 1 | 1 | 1 | 1 | - | 1 | 1 | - | 1 | 1 | - | 1 |
| LOS | C | C | C | C | - | D | C | - | C | D | - | D |
| Delay (s) | 30.7 | 25.3 | 23.3 | 25.9 | - | 49.2 | 28.6 | - | 20.5 | 42.6 | - | 51.6 |
| v/c | 0.76 | 0.45 | 0.27 | 0.12 | - | 0.80 | 0.74 | - | 0.47 | 0.54 | - | 0.73 |
| Queue (ft.) | 175 | 225 | 50 | 25 | - | 350 | 200 | - | 250 | 200 | - | 200 |
| Storage (ft.) | n/a | n/a | 150 | 260 | - | n/a | 670 | - | n/a | n/a | - | n/a |
| PM Peak | EB |  |  | WB |  |  | NB |  |  | SB |  |  |
|  | L | T | R | L | - | T/R | L | - | T/R | L/T | - | T/R |
| \# Lanes | 1 | 1 | 1 | 1 | - | 1 | 1 | - | 1 | 1 | - | 1 |
| LOS | C | C | C | C | - | D | C | - | C | D | - | F |
| Delay (s) | 29.3 | 24.2 | 22.6 | 25.0 | - | 44.9 | 29.2 | - | 24.1 | 44.7 | - | 83.2 |
| v/c | 0.75 | 0.41 | 0.27 | 0.15 | - | 0.75 | 0.74 | - | 0.59 | 0.65 | - | 0.99 |
| Queue (ft.) | 200 | 200 | 50 | 50 | - | 325 | 100 | - | 325 | 325 | - | 325 |
| Storage (ft.) | n/a | $\mathrm{n} / \mathrm{a}$ | 150 | 260 | - | n/a | 670 | - | n/a | n/a | - | n/a |

Additional $\quad$ Queues are 95th-percentile, rounded to the nearest 25 ft ( 25 ft minimum)
Information

| Year: 2042 | Future No-Build Conditions (Design Year) |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| AM Peak | EB |  |  | WB |  |  | NB |  |  | SB |  |  |
|  | L | T | R | L | - | T/R | L | - | T/R | L/T | - | T/R |
| \# Lanes | 1 | 1 | 1 | 1 | - | 1 | 1 | - | 1 | 1 | - | 1 |
| LOS | F | C | C | C | - | F | F | - | C | E | - | F |
| Delay (s) | 81.9 | 28.7 | 24.2 | 26.8 | - | 110.0 | 80.6 | - | 26.1 | 63.2 | - | 152.3 |
| v/c | 1.03 | 0.57 | 0.33 | 0.18 | - | 1.09 | 1.01 | - | 0.65 | 0.86 | - | 1.18 |
| Queue (ft.) | 350 | 250 | 25 | 50 | - | 450 | 325 | - | 325 | 250 | - | 250 |
| Storage (ft.) | n/a | n/a | 150 | 260 | - | n/a | 670 | - | $\mathrm{n} / \mathrm{a}$ | $\mathrm{n} / \mathrm{a}$ | - | n/a |
| PM Peak | EB |  |  | WB |  |  | NB |  |  | SB |  |  |
|  | L | T | R | L | - | T/R | L | - | T/R | L/T | - | T/R |
| \# Lanes | 1 | 1 | 1 | 1 | - | 1 | 1 | - | 1 | 1 | - | 1 |
| LOS | D | C | C | C | - | E | C | - | C | E | - | F |
| Delay (s) | 47.8 | 23.9 | 22.0 | 25.0 | - | 56.1 | 32.6 | - | 29.6 | 56.8 | - | 185.0 |
| v/c | 0.91 | 0.47 | 0.30 | 0.18 | - | 0.88 | 0.78 | - | 0.72 | 0.84 | - | 1.27 |
| Queue (ft.) | 350 | 225 | 50 | 50 | - | 425 | 125 | - | 400 | 450 | - | 450 |
| Storage (ft.) | n/a | n/a | 150 | 260 | - | n/a | 670 | - | $\mathrm{n} / \mathrm{a}$ | $\mathrm{n} / \mathrm{a}$ | - | n/a |

[^2]
## Alt. 1: Modified Traffic Signal:

Practicality:

| Public Opinion: | Formal public involvement meetings have not occurred with the proposed alternatives. <br> Complaints have been previously received regarding the current operational and safety of the <br> existing intersection configuration. |
| ---: | :--- |
| Business Impacts: | None |
| UOW Impacts: | 0.04-acres |
| Cost Estimate: | $\$ 340,000$ |
| Additional Info: | Restricting turn movements to/from Church Street are expected to improve safety and <br> operations for general traffic along Winneconne Avenue. However, adjustments to the Route <br> 32 bus that uses Church Street will be necessary. Accommodation of the design vehicles <br> require the stop bars for the eastbound and southbound left-turn lanes to be pulled further <br> upstream from the intersection. If the eastbound left-turn stop bars remain in their current <br> location, the impacts to the parcel in the northwest quadrant would have more significant <br> ROW impacts. Additionally, at least one significant utility pole would need to be relocated to <br> accommodate the new curb line. |

## Safety Analysis:

| Conflict Points: | - Alt. 1: Modified Traffic Signal: 40 (excluding Church Street) <br>  <br>  <br> Vulnerable Users: <br> - Alt. 2: Roundabout - 4-Leg: 24 (excluding Church Street) <br> - Alt. 3: Roundabout - 5-Leg: 28 |
| :---: | :---: |
| Pedestrians, bicyclists |  | | Accommodation of the design vehicles require the stop bars for the eastbound and |
| :--- |
| Adional Info: |
|  |
| southbound left-turn lanes to be pulled further upstream from the intersection in order to |
| avoid more extensive modifications and ROW acquisitions to the northwest corner. |

Crash Trend(s) and Contributing Factors:
-

Conflict Points:

Additional Info:

Additional signal heads and signal phasing/operation improvements may reduce the number of front-to-rear manner of collision events. Modification of signal phasing and capacity improvements may also reduce the number of front-to-side manner of collision crashes. (Vehicle-vehicle conflicts only)

- Existing intersection: 34 (excluding Church Street)

Safety Performance Measures:

|  | Analysis Period | KABC | PDO | Total |
| :--- | :---: | :---: | :---: | :---: |
| Existing Conditions | $2017-2021$ | 8 | 26 | 34 |
| Future No-Build | $2024-2033$ | 17.9 | 31.6 | 49.5 |
| Alt. 1: Modified Traffic Signal: | $2024-2033$ | 16.6 | 28.8 | 45.4 |

## Operational Analysis:

| Warrant Analysis: | $\mathrm{n} / \mathrm{a}$ |
| :---: | :--- |
| Queue Impacts: | The 95 <br> th <br> percentile queues for southbound right-turns are not able to be accommodated in <br> exception of the 2042 AM peak period, the $50^{\text {th }}$ percentile queues are expected to be <br> ex |

Phase II: ICE Report
accommodated through the design year without the additional acquisition. Similar business driveway access is expected with the proposed alternative.
Analysis indicates the modified traffic signal can accommodate approximately $27 \%$ more

## Additional Capacity:

 traffic (above 2022 volumes). This additional capacity is accommodated without additional lanes.Railroad Impacts:

None
The currently proposed modifications to the existing traffic signals do not include EVP, adding pedestrian call buttons, flashing yellow arrow (FYA) conversion or full implementation of signal head-per-lane in the alternative cost estimates. Crash patterns do not indicate there are current safety issues that would trigger implementation of FYAs or signal head-per-lane for the southbound, westbound, or northbound approaches. The addition of pedestrian call buttons would allow for additional traffic signal time split variations, which have the potential of small additional operational improvements.

Existing overhead utilities and narrow terraces may make signal head-per-lane implementation more challenging. Unknown underground utility impacts will need to be considered as well. From a public perception and construction/mobilization impact perspective, signal improvements for all approaches may be more prudent.

Should the modified traffic signal alternative be selected, additional discussions will need to occur to determine if full-intersection signalization improvements are desirable by the city. Additional features such as signal head-per-lane, FYAs, EVP, pedestrian call buttons have proactive operational and safety benefits; however, there would be additional costs above what is estimated as part of this Phase II ICE report in order to implement them. The magnitude of the additional costs would need further investigation to determine the extents of utility impacts created by additional monotube signal structures as well as necessary infrastructure needed to implement pedestrian call buttons which comply with PROWAG and ADA standards.

Operational Performance Measures:

| Year: 2022 | Alt. 1: Modified Traffic Signal |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| AM Peak | EB |  |  | WB |  |  | NB |  |  | SB |  |  |
|  | L | T | R | L | - | T/R | L | - | T/R | L/T | T | R |
| \# Lanes | 2 | 1 | 1 | 1 | - | 1 | 1 | - | 1 | 1 | 1 | 1 |
| LOS | D | C | C | C | - | D | C | - | C | D | D | C |
| Delay (s) | 50.3 | 23.7 | 21.8 | 23.1 | - | 38.9 | 22.0 | - | 22.1 | 38.4 | 39.0 | 28.7 |
| v/c | 0.80 | 0.42 | 0.25 | 0.12 | - | 0.69 | 0.57 | - | 0.49 | 0.31 | 0.33 | 0.32 |
| Queue (ft.) | 125 | 200 | 50 | 25 | - | 300 | 175 | - | 250 | 150 | 150 | 100 |
| Storage (ft.) | 150 | n/a | 150 | 260 | - | n/a | 670 | - | n/a | n/a | n/a | 105 |
| PM Peak | EB |  |  | WB |  |  | NB |  |  | SB |  |  |
|  | L | T | R | L | - | T/R | L | - | T/R | L/T | T | R |
| \# Lanes | 2 | 1 | 1 | 1 | - | 1 | 1 | - | 1 | 1 | 1 | 1 |
| LOS | D | C | C | C | - | D | B | - | C | D | D | C |
| Delay (s) | 49.6 | 24.1 | 22.5 | 23.6 | - | 40.2 | 20.0 | - | 24.2 | 35.8 | 36.3 | 26.7 |
| v/c | 0.80 | 0.41 | 0.26 | 0.15 | - | 0.70 | 0.42 | - | 0.59 | 0.34 | 0.36 | 0.40 |
| Queue (ft.) | 150 | 200 | 50 | 50 | - | 300 | 100 | - | 350 | 175 | 175 | 150 |
| Storage (ft.) | 150 | n/a | 150 | 260 | - | n/a | 670 | - | n/a | n/a | n/a | 105 |

Additional $\quad$ Queues are 95th-percentile, rounded to the nearest 25 ft ( 25 ft minimum)
Information

Year: 2042
Alt. 1: Modified Traffic Signal

| AM Peak | EB |  |  | WB |  |  | NB |  |  | SB |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | L | T | R | L | - | T/R | L | - | T/R | L/T | T | R |
| \# Lanes | 2 | 1 | 1 | 1 | - | 1 | 1 | - | 1 | 1 | 1 | 1 |
| LOS | D | C | C | C | - | D | D | - | C | D | D | D |
| Delay (s) | 53.4 | 22.9 | 20.5 | 22.4 | - | 50.7 | 54.9 | - | 30.6 | 44.0 | 45.6 | 38.5 |
| v/c | 0.84 | 0.51 | 0.30 | 0.16 | - | 0.87 | 0.91 | - | 0.70 | 0.47 | 0.51 | 0.69 |
| Queue (ft.) | 150 | 250 | 25 | 25 | - | 400 | 300 | - | 350 | 150 | 150 | 225 |
| Storage (ft.) |  | n/a | 150 | 260 | - | n/a | 670 | - | n/a | n/a | n/a | 105 |
| PM Peak | EB |  |  | WB |  |  | NB |  |  | SB |  |  |
|  | L | T | R | L | - | T/R | L | - | T/R | L/T | T | R |
| \# Lanes | 2 | 1 | 1 | 1 | - | 1 | 1 | - | 1 | 1 | 1 | 1 |
| LOS | D | C | C | C | - | D | C | - | C | D | D | C |
| Delay (s) | 52.1 | 24.0 | 22.1 | 23.6 | - | 47.5 | 22.4 | - | 29.3 | 39.7 | 40.7 | 29.1 |
| v/c | 0.83 | 0.46 | 0.30 | 0.18 | - | 0.81 | 0.52 | - | 0.72 | 0.44 | 0.47 | 0.49 |
| Queue (ft.) | 175 | 225 | 50 | 50 | - | 400 | 125 | - | 425 | 200 | 200 | 200 |
| Storage (ft.) |  | n/a | 150 | 260 | - | n/a | 670 | - | n/a | n/a | n/a | 105 |


| Additional | Queues are 95th-percentile, rounded to the nearest 25 ft (25 ft minimum) |
| :--- | :--- | Information

Alt. 2: Roundabout - 4-Leg:
Practicality:
Public Opinion: $\begin{aligned} & \text { Formal public involvement meetings have not occurred with the proposed alternatives. Given }\end{aligned}$ the magnitude of ROW impacts, it is not expected to be the preferred option.
The Boost Mobile parcel on the northwest corner of Winneconne Avenue at Commercial Street would need to be acquired. The Dairy Queen, Walgreens, Mobil fuel station, Tobacco Outlet Plus and the residential property on the northwest corner of Winneconne Avenue at
Business Impacts: Church Street would all require varying levels of right-of-way acquisitions. The Dairy Queen and Walgreens pylon signs would need to be relocated. Walgreen's western-most driveway along Winneconne Avenue would need to be closed and operations consolidated to the existing driveway further east on Winneconne Avenue.
ROW Impacts:
0.71-acres

Several overhead utility poles will need to be relocated along the north side of Winneconne Avenue, and along the east side of Commercial Street, south of the intersection.
Cost Estimate:

Additional Info:
\$2,110,000
Restricting turn movements to/from Church Street are expected to improve safety and operations for general traffic along Winneconne Avenue. However, adjustments to the Route 32 bus that uses Church Street will be necessary. The roundabout design would allow a natural place for the Route 32 bus to make a U-turn in order to access northbound Church Street from eastbound Winneconne Avenue.

The flagpole and "Historic Downtown Neenah" monument sign in the northeast corner will need to be relocated.

## Safety Analysis:

Crash Trend(s) being Improved with Alt.:


Geometric Concerns:
Sideswipe and head-on crashes should be significantly reduced and likely eliminated altogether, given the geometric design of a roundabout.
Maintaining access between Winneconne Avenue and Church Street requires an intersection to be placed closer to the roundabout than is desirable. The angle of intersection is such that a channelizing island cannot be placed on the Church Street approach to further force southbound traffic to make right turns only. This alignment also forces the crosswalk for crossing the westbound exit lane to be further away from the roundabout, forcing pedestrians to travel further out of their way in addition to being placed in a position where exiting roundabout traffic is able to achieve higher speeds.

Additional Info:

Safety Performance Measures:

|  | Analysis Period | KABC | PDO | Total |
| :--- | :---: | :---: | :---: | :---: |
| Existing Conditions | $2017-2021$ | 8 | 26 | 34 |
| Future No-Build | $2024-2033$ | 17.9 | 31.6 | 49.5 |
| Alt. 2: Roundabout - 4-Leg: | $2024-2033$ | 23.4 | 129.2 | 152.6 |

## Operational Analysis:

Warrant Analysis: $\quad \mathrm{n} / \mathrm{a}$

| Queue Impacts: | Except for the southbound approach, expected $95^{\text {th }}$ percentile queues are not anticipated to <br> impact adjacent business access. |
| ---: | :--- |
| Additional Capacity: | Analysis indicates the modified traffic signal can accommodate approximately 36\% more <br> traffic (above 2022 volumes). This additional capacity is accommodated without additional <br> lanes. |
| Railroad Impacts: | None |
| Additional Info: |  |

Operational Performance Measures:

| Year: 2022 | Alt. 2: Roundabout - 4-Leg |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| AM Peak | EB |  |  | WB |  |  | NB |  |  | SB |  |  |
|  | L/T | - | T/R | L/T | - | T/R | L/T | - | T/R | L/T | - | T/R |
| \# Lanes | 1 | - | 1 | 1 | - | 1 | 1 | - | 1 | 1 | - | 1 |
| LOS | A | - | A | B | - | B | B | - | B | B | - | B |
| Delay (s) | 9.4 | - | 9.2 | 12.8 | - | 11.9 | 11.4 | - | 10.9 | 12.0 | - | 11.4 |
| v/c | 0.47 | - | 0.47 | 0.39 | - | 0.39 | 0.47 | - | 0.47 | 0.46 | - | 0.46 |
| Queue (ft.) | 75 | - | 75 | 50 | - | 50 | 75 | - | 75 | 75 | - | 75 |
| Storage (ft.) | n/a | - | n/a | n/a | - | n/a | n/a | - | n/a | n/a | - | n/a |
| PM Peak | EB |  |  | WB |  |  | NB |  |  | SB |  |  |
|  | L/T | - | T/R | L/T | - | T/R | L/T | - | T/R | L/T | - | T/R |
| \# Lanes | 1 | - | 1 | 1 | - | 1 | 1 | - | 1 | 1 | - | 1 |
| LOS | A | - | A | B | - | A | A | - | A | B | - | B |
| Delay (s) | 9.3 | - | 9.1 | 10.2 | - | 9.6 | 9.1 | - | 8.8 | 10.4 | - | 10.6 |
| v/c | 0.44 | - | 0.44 | 0.31 | - | 0.31 | 0.37 | - | 0.37 | 0.47 | - | 0.50 |
| Queue (ft.) | 75 | - | 75 | 25 | - | 25 | 50 | - | 50 | 75 | - | 75 |
| Storage (ft.) | n/a | - | n/a | n/a | - | n/a | $\mathrm{n} / \mathrm{a}$ | - | n/a | n/a | - | n/a |

Additional $\quad$ Queues are 95th-percentile, rounded to the nearest 25 ft ( 25 ft minimum)
Information

Year: 2042
Alt. 2: Roundabout - 4-Leg

| AM Peak | EB |  |  | WB |  |  | NB |  |  | SB |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | L/T | - | T/R | L/T | - | T/R | L/T | - | T/R | L/T | - | T/R |
| \# Lanes | 1 | - | 1 | 1 | - | 1 | 1 | - | 1 | 1 | - | 1 |
| LOS | B | - | B | C | - | C | C | - | C | C | - | C |
| Delay (s) | 12.3 | - | 11.9 | 18.7 | - | 17.2 | 16.1 | - | 15.3 | 17.2 |  | 16.2 |
| v/c | 0.58 | - | 0.58 | 0.52 | - | 0.52 | 0.60 | - | 0.60 | 0.60 |  | 0.60 |
| Queue (ft.) | 125 | - | 125 | 75 | - | 75 | 100 | - | 100 | 100 |  | 100 |
| Storage (ft.) | n/a | - | n/a | n/a | - | n/a | n/a | - | n/a | n/a |  | n/a |
| PM Peak | EB |  |  | WB |  |  | NB |  |  | SB |  |  |
|  | L/T | - | T/R | L/T | - | T/R | L/T | - | T/R | L/T | - | T/R |
| \# Lanes | 1 | - | 1 | 1 | - | 1 | 1 | - | 1 | 1 | - | 1 |
| LOS | B | - | B | B | - | B | B | - | B | B | - | B |
| Delay (s) | 12.2 | - | 11.8 | 13.7 | - | 12.7 | 11.9 | - | 11.3 | 14.4 | - | 14.8 |
| v/c | 0.56 | - | 0.56 | 0.42 | - | 0.42 | 0.48 | - | 0.48 | 0.60 | - | 0.63 |
| Queue (ft.) | 100 | - | 100 | 50 | - | 50 | 75 | - | 75 | 125 | - | 125 |
| Storage (ft.) | n/a | - | n/a | n/a | - | n/a | n/a | - | n/a | n/a | - | n/a |

[^3]Alt. 3: Roundabout - 5-Leg:
Practicality:

Public Opinion: | Formal public involvement meetings have not occurred with the proposed alternatives. Given |
| :--- | :--- | the magnitude of ROW impacts, it is not expected to be the preferred option.

The Boost Mobile parcel on the northwest corner of Winneconne Avenue at Commercial Street would need to be acquired. The Dairy Queen, Walgreens, Mobil fuel station, Tobacco Outlet Plus and the residential property on the northwest corner of Winneconne Avenue at Business Impacts: Church Street would all require varying levels of right-of-way acquisitions. The Dairy Queen and Walgreens pylon signs would need to be relocated. Walgreen's western-most driveway along Winneconne Avenue would need to be closed and operations consolidated to the existing driveway further east on Winneconne Avenue.
ROW Impacts:
0.70-acres

Several overhead utility poles will need to be relocated along the north side of Winneconne Avenue, and along the east side of Commercial Street, south of the intersection.
Cost Estimate:
\$2,350,000
Incorporating Church Street into the main intersection will allow for safer access from Winneconne Avenue without having to change the Route 32 bus path.
Additional Info:
The flagpole and "Historic Downtown Neenah" monument sign in the northeast corner will need to be relocated.

## Safety Analysis:

Crash Trend(s) being
Improved with Alt.:

Geometric Concerns:

Additional Info:

Sideswipe and head-on crashes should be significantly reduced and likely eliminated altogether, given the geometric design of a roundabout.
Maintaining access between Winneconne Avenue and Church Street requires an intersection to be placed closer to the roundabout than is desirable. The angle of intersection is such that a channelizing island cannot be placed on the Church Street approach to further force southbound traffic to make right turns only. This alignment also forces the crosswalk for crossing the westbound exit lane to be further away from the roundabout, forcing pedestrians to travel further out of their way in addition to being placed in a position where exiting roundabout traffic is able to achieve higher speeds.
The IHSDM tool does not currently have data sets which cover 5-leg roundabouts. Based on crash frequency prediction models found in NCHRP Report 672 ${ }^{2}$, 5-leg roundabouts with two circulating lanes are expected to have higher crash frequencies for both injury and PDO crash types. Therefore, for the purpose of this report, 5-leg roundabouts will be assumed to have poorer benefit/cost ratios and higher present value of crash costs than a 4-leg roundabout.

Safety Performance Measures:

|  | Analysis Period | KABC | PDO | Total |
| :--- | :---: | :---: | :---: | :---: |
| Existing Conditions | $2017-2021$ | 8 | 26 | 34 |
| Future No-Build | $2024-2033$ | 17.9 | 31.6 | 49.5 |
| Alt. 3: Roundabout - 5-Leg: | $2024-2033$ | $\mathrm{n} / \mathrm{a}$ | $\mathrm{n} / \mathrm{a}$ | $\mathrm{n} / \mathrm{a}$ |

[^4]| Operational Analysis: |  |
| ---: | :--- |
| Warrant Analysis: | $\mathrm{n} / \mathrm{a}$ |
| Queue Impacts: | Except for the southbound approach, expected $95^{\text {th }}$ percentile queues are not anticipated to <br> impact adjacent business access. |
| Additional Capacity: | Analysis indicates the modified traffic signal can accommodate approximately 30\% more <br> traffic (above 2022 volumes). This additional capacity is accommodated without additional <br> lanes. |
| Railroad Impacts: | None |
| Additional Info: | WB-65s are not able to make the hard southbound right turn from Commercial Street onto <br> Church Street. Given the surrounding street network, this is not a significant concern. WB-50s <br> would be able to make this movement. |

Operational Performance Measures:

| Year: 2022 | Alt. 3: Roundabout - 5-Leg |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| AM Peak | EB |  |  | WB |  |  | NB |  |  | SB |  |  |
|  | L/T | - | T/R | L/T | - | T/R | L/T | - | T/R | L/T | - | T/R |
| \# Lanes | 1 | - | 1 | 1 | - | 1 | 1 | - | 1 | 1 | - | 1 |
| LOS | A | - | A | B | - | B | B | - | B | B | - | B |
| Delay (s) | 10.0 | - | 9.8 | 13.7 | - | 12.7 | 12.3 | - | 11.7 | 12.9 | - | 12.2 |
| v/c | 0.49 | - | 0.49 | 0.40 | - | 0.40 | 0.49 | - | 0.49 | 0.48 | - | 0.48 |
| Queue (ft.) | 75 | - | 75 | 50 | - | 50 | 75 | - | 75 | 75 | - | 75 |
| Storage (ft.) | n/a | - | n/a | n/a | - | n/a | n/a | - | n/a | n/a | - | n/a |
| PM Peak | EB |  |  | WB |  |  | NB |  |  | SB |  |  |
|  | L/T | - | T/R | L/T | - | T/R | L/T | - | T/R | L/T | - | T/R |
| \# Lanes | 1 | - | 1 | 1 | - | 1 | 1 | - | 1 | 1 | - | 1 |
| LOS | B | - | A | B | - | B | B | - | A | B | - | B |
| Delay (s) | 10.1 | - | 9.8 | 11.2 | - | 10.4 | 10.1 | - | 9.6 | 11.6 | - | 11.8 |
| v/c | 0.48 | - | 0.48 | 0.33 | - | 0.33 | 0.40 | - | 0.40 | 0.50 | - | 0.53 |
| Queue (ft.) | 75 | - | 75 | 25 | - | 25 | 50 | - | 50 | 75 | - | 100 |
| Storage (ft.) | n/a | - | n/a | n/a | - | n/a | $\mathrm{n} / \mathrm{a}$ | - | n/a | n/a | - | n/a |

Additional $\quad$ Queues are 95th-percentile, rounded to the nearest 25 ft ( 25 ft minimum)
Information

Year: 2042
Alt. 3: Roundabout - 5-Leg

| AM Peak | EB |  |  | WB |  |  | NB |  |  | SB |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | L/T | - | T/R | L/T | - | T/R | L/T | - | T/R | L/T | - | T/R |
| \# Lanes | 1 | - | 1 | 1 | - | 1 | 1 | - | 1 | 1 | - | 1 |
| LOS | B | - | B | C | - | C | C | - | C | C | - | C |
| Delay (s) | 13.4 | - | 13.0 | 20.6 | - | 18.9 | 18.0 |  | 17.0 | 19.2 | - | 18.0 |
| v/c | 0.61 | - | 0.61 | 0.55 | - | 0.55 | 0.63 | - | 0.63 | 0.63 | - | 0.63 |
| Queue (ft.) | 150 | - | 150 | 75 | - | 75 | 125 | - | 125 | 100 | - | 100 |
| Storage (ft.) | n/a | - | n/a | n/a | - | n/a | n/a | - | n/a | n/a | - | n/a |
| PM Peak | EB |  |  | WB |  |  | NB |  |  | SB |  |  |
|  | L/T | - | T/R | L/T | - | T/R | L/T | - | T/R | L/T | - | T/R |
| \# Lanes | 1 | - | 1 | 1 | - | 1 | 1 | - | 1 | 1 | - | 1 |
| LOS | B | - | B | C | - | B | B | - | B | C | - | C |
| Delay (s) | 13.7 | - | 13.2 | 15.4 | - | 14.3 | 13.6 | - | 12.9 | 17.0 | - | 17.3 |
| v/c | 0.60 | - | 0.60 | 0.45 | - | 0.45 | 0.51 | - | 0.51 | 0.64 | - | 0.67 |
| Queue (ft.) | 125 | - | 125 | 50 | - | 50 | 75 | - | 75 | 125 | - | 150 |
| Storage (ft.) | n/a | - | n/a | n/a | - | n/a | $\mathrm{n} / \mathrm{a}$ | - | n/a | n/a | - | n/a |

[^5]Operational Performance Measures:

| Year: 2022 | Alt. 3: Roundabout - 5-Leg |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| AM Peak | SB Church St |  |  |  |  |  |  |  |  |  |  |  |
|  | - | All | - | - | - | - | - | - | - | - | - | - |
| \# Lanes | - | 1 | - | - | - | - | - | - | - | - | - | - |
| LOS | - | C | - | - | - | - | - | - | - | - | - | - |
| Delay (s) | - | 15.2 | - | - | - | - | - | - | - | - | - | - |
| v/c | - | 0.27 | - | - | - | - | - | - | - | - | - | - |
| Queue (ft.) | - | 25 | - | - | - | - | - | - | - | - | - | - |
| Storage (ft.) | - | n/a | - | - | - | - | - | - | - | - | - | - |
| PM Peak | SB Church St |  |  |  |  |  |  |  |  |  |  |  |
|  | - | All | - | - | - | - | - | - | - | - | - | - |
| \# Lanes | - | 1 | - | - | - | - | - | - | - | - | - | - |
| LOS | - | B | - | - | - | - | - | - | - | - | - | - |
| Delay (s) | - | 12.6 | - | - | - | - | - | - | - | - | - | - |
| v/c | - | 0.17 | - | - | - | - | - | - | - | - | - | - |
| Queue (ft.) | - | 25 | - | - | - | - | - | - | - | - | - | - |
| Storage (ft.) | - | n/a | - | - | - | - | - | - | - | - | - | - |
| Additional Information | Queues are 95th-percentile, rounded to the nearest 25 ft ( 25 ft minimum) |  |  |  |  |  |  |  |  |  |  |  |


| Year: 2042 | Alt. 3: Roundabout - 5-Leg |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| AM Peak | SB Church St |  |  |  |  |  |  |  |  |  |  |  |
|  | - | All | - | - | - | - | - | - | - | - | - | - |
| \# Lanes | - | 1 | - | - | - | - | - | - | - | - | - | - |
| LOS | - | C | - | - | - | - | - | - | - | - | - | - |
| Delay (s) | - | 22.6 | - | - | - | - | - | - | - | - | - | - |
| v/c | - | 0.39 | - | - | - | - | - | - | - | - | - | - |
| Queue (ft.) | - | 50 | - | - | - | - | - | - | - | - | - | - |
| Storage (ft.) | - | n/a | - | - | - | - | - | - | - | - | - | - |
| PM Peak | SB Church St |  |  |  |  |  |  |  |  |  |  |  |
|  | - | All | - | - | - | - | - | - | - | - | - | - |
| \# Lanes | - | 1 | - | - | - | - | - | - | - | - | - | - |
| LOS | - | C | - | - | - | - | - | - | - | - | - | - |
| Delay (s) | - | 17.5 | - | - | - | - | - | - | - | - | - | - |
| v/c | - | 0.25 | - | - | - | - | - | - | - | - | - | - |
| Queue (ft.) | - | 25 | - | - | - | - | - | - | - | - | - | - |
| Storage (ft.) | - | n/a | - | - | - | - | - | - | - | - | - | - |
| Additional Information | Queues are 95th-percentile, rounded to the nearest 25 ft ( 25 ft minimum) |  |  |  |  |  |  |  |  |  |  |  |

## Attachments:

(Provide attachments outline in FDM 11-25-3 Attachment 3.7 as appropriate)

1. ICE Report Checklist
2. Project Location Map
3. Intersection Crash Diagram
4. Conceptual Layouts
a. Alternative 1: Modified Traffic Signal
b. Alternative 2: Roundabout 4-Leg
c. Alternative 3: Roundabout 5-Leg
5. Preliminary Design Estimate of Probable Cost
6. IHSDM Crash Prediction Evaluations
7. Traffic Volumes
8. Traffic Analysis Output Reports

## ICE SUBMITTAL CHECKLIST

| Level of ICE (Check Applicable Box): | \ Phase II: Alternative Selection ICE |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Documentation | Submittal Requirements |  | Submittal to City |  | Submittal to BTO |  |
|  | Phase I ICE | Phase II ICE | Included | N/A | Included | N/A |
| Report |  |  |  |  |  |  |
| - Phase I: ICE Memorandum <br> - Phase I: ICE Brainstorming Guide <br> - Phase II: ICE Worksheet | Required <br> Required $N / A$ | $\begin{aligned} & \mathrm{N} / \mathrm{A} \\ & \mathrm{~N} / \mathrm{A} \end{aligned}$ <br> Required | $\begin{aligned} & \Gamma \\ & \Gamma \\ & \nabla \end{aligned}$ | $\sqrt{V}$ <br> $\sqrt{V}$ $\Gamma$ | $\begin{aligned} & \ulcorner \\ & \ulcorner \\ & \square \end{aligned}$ | $\begin{aligned} & \Gamma \\ & \Gamma \\ & \Gamma \end{aligned}$ |
| Project Description |  |  |  |  |  |  |
| - Project Location Map <br> - Aerial Photo of Intersection | Required <br> Optional | Required <br> Optional | $\nabla$ $\nabla$ | $\begin{aligned} & \Gamma \\ & \Gamma \end{aligned}$ | $\begin{aligned} & \Gamma \\ & \Gamma \end{aligned}$ | $\begin{aligned} & \Gamma \\ & \Gamma \end{aligned}$ |
| Traffic Volume Data |  |  |  |  |  |  |
| - Turning Movement Counts (field count data) <br> - Segment Traffic Forecasts <br> - Intersection Traffic Forecasts | Optional <br> Optional <br> Optional | Required <br> Required <br> Required | $\begin{aligned} & \nabla \\ & \Gamma \\ & \nabla \end{aligned}$ | $\begin{aligned} & \Gamma \\ & \nabla \\ & \Gamma \end{aligned}$ | $\begin{aligned} & \ulcorner \\ & \ulcorner \\ & \square \end{aligned}$ | $\begin{aligned} & \ulcorner \\ & \ulcorner \\ & \square \end{aligned}$ |
| Safety Considerations |  |  |  |  |  |  |
| - Intersection Crash Diagram with summary of crashes <br> - Predictive Safety Analysis | Required <br> Optional | Required <br> Required | $\begin{aligned} & \nabla \\ & \nabla \end{aligned}$ | $\begin{aligned} & \Gamma \\ & \Gamma \end{aligned}$ | $\begin{aligned} & \Gamma \\ & \Gamma \end{aligned}$ | $\begin{aligned} & \Gamma \\ & \Gamma \end{aligned}$ |
| Additional Modes of Transportation |  |  |  |  |  |  |
| - Wisconsin Bike Map (bike rating) <br> - 5-Year Summary of OSOW and Long Truck Routes | Optional <br> Optional | Optional <br> Optional |  | $\nabla$ $\nabla$ | $\begin{aligned} & \Gamma \\ & \Gamma \end{aligned}$ | $\begin{aligned} & \Gamma \\ & \Gamma \end{aligned}$ |
| Operational Analysis (as applicable) ${ }^{(a)}$ |  |  |  |  |  |  |
| - AWSC Warrants <br> - Traffic Signal Warrants <br> - Model Files for HCS, Sidra, \& Synchro | Optional <br> Optional <br> Optional <br> (a) | Required <br> Required <br> Required | $\begin{aligned} & \Gamma \\ & \Gamma \\ & \nabla \end{aligned}$ | $\begin{aligned} & \nabla \\ & \nabla \\ & \Gamma \end{aligned}$ | Not Appl |  |

 DT1887 and DT2291 to BTO for all HCM-based and microsimulation analyses that is conducted.

## ICE SUBMITTAL CHECKLIST


(b) If Sidra analysis is conducted, submit copies of all five worksheets listed below.
(c) If Synchro analysis is conducted, submit both the intersection report (signalized or unsignalized as applicable) and the HCM 6 th Edition report (signalized summary, AWSC or TWSC as applicable)
 should be submitted along with the ICE report to ensure that all SimTraffic analyses referenced in the ICE report has gone through the Traffic Model Peer Review Process


SCALE: 1:5280


SCALE: 1:100





| ITEM | ITEM DESCRIPTION | UNIT | QUANTITY | UNIT PRICE |  | TAL |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | REMOVALS | LS | 1 | \$18,000.00 | \$ | 18,000 |
| SUBIOTALREMOVALS |  |  |  |  | \$ | 18,000 |
| 2 | EARTHWORK |  | \% of Items 1 \& 3-4 | N/A | \$ | - |
| 2.01 | Excavation Common | CY | 230 | \$26.00 | \$ | 6,000 |
| SUBIOTAL EARIHMORK |  |  |  |  | \$ | 6,000 |
| 3 |  |  |  |  |  |  |
| 3.02 | Base Aggregate Dense 1 1/4" | TON | 200 | \$22.00 | \$ | 4,400 |
| SUBIOTAL BASE |  |  |  |  | \$ | 4,400 |
| 4 | PAVEM ENT |  |  |  |  |  |
| 4.01 | Concrete Pavement 8" | SY | 220 | \$100.00 | \$ | 22,000 |
| SUBIOTALPAVEMENT |  |  |  |  | \$ | 22,000 |
| 5 | ROADWAY M ISCELLANEOUS |  | \% of Items 1 \& 3-4 | N/A | \$ | - |
|  | Concrete Curb and Gutter | LF | 230 | \$30.00 | \$ | 6,900 |
| 5.07 | Concrete Curb Pedestrian | LF | 20 | \$50.00 | \$ | 1,000 |
| 5.08 | Concrete Sidewalk 5-Inch | SF | 150 | \$10.00 | \$ | 1,500 |
| SUBIOTALROADWAY MISCELANEOUS |  |  |  |  | \$ | 9,400 |
| 6 | DRAINAGE/ STORM SEWER | LS | 1 | \$5,000.00 | \$ | 5,000 |
| SUBIOTAL DRAINAGE/ STORM SEWER |  |  |  |  | \$ | 5,000 |
| SUBTOTAL ROADWAY COSTS (ITEMS 1-6) |  |  |  |  | \$ | 64,800 |
| 7 | TRAFFIC SIGNALS | LS | 1 | \$66,000.00 | \$ | 66,000 |
| 8 | ITS | LS | 1 | \$45,000.00 | \$ | 45,000 |
| 9 | TRAFFIC CONTROL | LS | 1 | \$20,000.00 | \$ | 20,000 |
| 10 | EROSION CONTROL | LS | 5 \% of Items 1-6 | N/A | \$ | 3,200 |
| 11 | LIGHTING | LS | 0 |  | \$ | - |
| 12 | SIGNING/ M ARKING | LS | 1 | \$24,000.00 | \$ | 24,000 |
| 13 | WETLAND M ITIGATION | LS | 0 |  | \$ | - |
| 14 | HAZM AT | LS | 0 |  | \$ | - |
| 15 | ROADWAY INCIDENTALS | LS | 30 \% of Items 1-6 | N/A | \$ | 19,400 |
| TOTAL ROADWAY COSTS (Items 1-15) |  |  |  |  | \$ | 242,400 |
| 16 | STRUCTURES |  |  |  |  |  |
| TOTAL STRUCTURE COSTS |  |  |  |  | \$ | - |
| 17 | M OBILIZATION | LS | 1 | \$30,000.00 | \$ | 30,000 |
| CONSTRUCTION SUBTOTAL (Items 1-17) |  |  |  |  | \$ | 272,400 |
| 18 | E\&C | LS | 15 \% of Items 1-17 | N/A | \$ | 40,900 |
| 19 | ROW Acquisition | LS | 1 | \$20,000.00 | \$ | 20,000 |
| TOTAL PROJECT COST |  |  |  |  | \$ | 340,000 |

## Assumptions

Pavement Structure: 8" Concrete over 8" Base Aggregate
Signal pole and accessories in northwest quadrant are moved to new location with new signal heads
Eastbound far-side signal replaced with monotube with signal heads per lane
Westbound far-side, right-side signal replaced with new signal heads
Improvements constructed under traffic

Winneconne Avenue \& Commercial Street, Neenah, WI
4 Leg Roundabout Alternative
Project ID: MSA \#07578063
Winnebago County Date: 1/ 31/ 2023

| ITEM | ITEM DESCRIPTION | UNIT |  | QUANTITY | UNIT PRICE | TOTAL |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | REMOVALS | LS |  | 1 | \$70,000.00 | \$ | 70,000 |
| SUBTOTALREMOVALS |  |  |  |  |  | \$ | 70,000 |
| 2 | EARTHWORK |  |  | \% of Items 1 \& 3-4 | N/A | \$ | - |
| 2.01 | Excavation Common | CY |  | 5,500 | \$18.00 | \$ | 99,000 |
| 2.05 | Select Borrow | CY |  | 1,100 | \$12.00 | \$ | 13,200 |
| SUBTOTALEARTHWORK |  |  |  |  |  | \$ | 112,200 |
| 3 | BASE |  |  |  |  |  |  |
| 3.02 | Base Aggregate Dense 11/4" | TON |  | 3,500 | \$20.00 | \$ | 70,000 |
| SUBTOTALBASE |  |  |  |  |  | \$ | 70,000 |
| 4 | PAVEM ENT |  |  |  |  |  |  |
| 4.01 | Concrete Pavement 8 " | SY |  | 5,100 | \$60.00 | \$ | 306,000 |
| 4.05 | Concrete Driveway 6" | SY |  | 160 | \$70.00 | \$ | 11,200 |
| 4.21 | Concrete Truck Apron 12" | SY |  | 380 | \$90.00 | \$ | 34,200 |
| 4.22 | Coloring Concrete WisDOT Red | CY |  | 130 | \$90.00 | \$ | 11,700 |
| SUBIOTAL PAVEMENT |  |  |  |  |  | \$ | 363,100 |
| 5 | ROADWAY M ISCELLANEOUS |  |  | \% of Items 1 \& 3-4 | N/A | \$ |  |
| 5.01 | Concrete Curb and Gutter | LF |  | 2,920 | \$25.00 | \$ | 73,000 |
| 5.08 | Concrete Sidewalk 4-Inch | SF |  | 3,600 | \$6.00 | \$ | 21,600 |
| 5.09 | Concrete Sidewalk 5-Inch | SF |  | 6,300 | \$9.00 | \$ | 56,700 |
| SUBIOTALROADWAY MISCEILANEOUS |  |  |  |  |  | \$ | 151,300 |
| 6 | DRAINAGE/ STORM SEWER | LS |  | 1 | \$30,000.00 | \$ | 30,000 |
| SUBTOTALDRAINAGE/STORM SEWER |  |  |  |  |  | \$ | 30,000 |
| SUBTOTAL ROADWAY COSTS (ITEM S 1-6) |  |  |  |  |  | \$ | 796,600 |
| 7 | TRAFFIC SIGNALS | LS |  | 0 |  | \$ |  |
| 8 | ITS | LS |  | 0 |  | \$ |  |
| 9 | TRAFFIC CONTROL | LS |  | \% of Items 1-6 | N/A | \$ | 119,500 |
| 10 | EROSION CONTROL | LS |  | \% of Items 1-6 | N/A | \$ | 23,900 |
| 11 | LIGHTING | LS |  | 1 | \$40,000.00 | \$ | 40,000 |
| 12 | SIGNING/ M ARKING | LS |  | 1 | \$110,000.00 | \$ | 110,000 |
| 13 | WETLAND MITIGATION | LS |  | 0 |  | \$ |  |
| 14 | HAZM AT | LS |  | 0 |  | \$ |  |
| 15 | ROADWAY INCIDENTALS | LS |  | \% of Items 1-6 | N/A | \$ | 278,800 |
| TOTAL ROADWAY COSTS (Items 1-15) |  |  |  |  |  | \$ | 1,368,800 |
| 16 | STRUCTURES |  |  |  |  |  |  |
| TOTAL STRUCTURE COSTS |  |  |  |  |  | \$ |  |
| 17 | MOBILIZATION | LS | 8 | \% of Items 1-16 | N/A | \$ | 109,500 |
| CONSTRUCTION SUBTOTAL (Items 1-17) |  |  |  |  |  | \$ | 1,478,300 |
| 18 | E\&C | LS | 12 | \% of Items 1-17 | N/A | \$ | 177,400 |
| 19 | ROW Acquisition | LS |  | 1 | \$450,000.00 | \$ | 450,000 |
| TOTAL PROJECT COST |  |  |  |  |  | \$ | 2,110,000 |

## Assumptions

Pavement Structure: 8" Concrete over 8" Base Aggregate
Signing/ M arking includes two overhead sign structures
Intersection is constructed under traffic
ROW Acquisition includes moving two signs

## Winneconne Avenue \& Commercial Street, Neenah, WI

5 Leg Roundabout Alternative
Project ID: M SA \#07578063
Winnebago County
Date: 1/ 31/2023

| ITEM | ITEM DESCRIPTION | UNIT | QUANTITY | UNIT PRICE |  | OTAL |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | REM OVALS | LS | 1 | \$70,000.00 | \$ | 70,000 |
| SUBTOTALREMOVALS |  |  |  |  | \$ | 70,000 |
| 2 | EARTHWORK |  | \% of Items 1 \& 3-4 | N/A | \$ |  |
| 2.01 | Excavation Common | CY | 6,500 | \$18.00 | \$ | 117,000 |
| 2.05 | Select Borrow | CY | 1,300 | \$12.00 | \$ | 15,600 |
| SUBTOTALEARTHMORK |  |  |  |  | \$ | 132,600 |
| 3 | BASE |  |  |  |  |  |
| 3.02 | Base Aggregate Dense $11 / 4{ }^{\prime \prime}$ | TON | 3,900 | \$20.00 | \$ | 78,000 |
| SUBIOTALBASE |  |  |  |  | \$ | 78,000 |
| 4 | PAVEM ENT |  |  |  |  |  |
| 4.01 | Concrete Pavement 8" | SY | 5,800 | \$60.00 | \$ | 348,000 |
| 4.05 | Concrete Driveway 6" | SY | 230 | \$70.00 | \$ | 16,100 |
| 4.21 | Concrete Truck Apron 12" | SY | 490 | \$90.00 | \$ | 44,100 |
| 4.22 | Coloring Concrete WisDOT Red | CY | 160 | \$90.00 | \$ | 14,400 |
| SUBIOTALPAVEMENT |  |  |  |  | \$ | 422,600 |
| 5 | ROADWAY MISCELLANEOUS |  | \% of Items 1 \& 3-4 | N/A | \$ |  |
| 5.01 | Concrete Curb and Gutter | LF | 3,500 | \$25.00 | \$ | 87,500 |
| 5.07 | Concrete Sidewalk 4-Inch | SF | 3,700 | \$6.00 | \$ | 22,200 |
| 5.08 | Concrete Sidewalk 5-Inch | SF | 6,800 | \$9.00 | \$ | 61,200 |
| SUBTOTALROADWAYMISCEIANEOUS |  |  |  |  | \$ | 170,900 |
| 6 | DRAINAGE/ STORM SEWER | LS | 1 | \$35,000.00 | \$ | 35,000 |
| SUBTOTALDRAINAGE/STORM SEWER |  |  |  |  | \$ | 35,000 |
| SUBTOTAL ROADWAY COSTS (ITEMS 1-6) |  |  |  |  | \$ | 909,100 |
| 7 | TRAFFIC SIGNALS | Each | 0 |  | \$ |  |
| 8 | ITS | LS | 0 |  | \$ |  |
| 9 | TRAFFIC CONTROL | LS | 15 \% of Items 1-6 | N/A | \$ | 136,400 |
| 10 | EROSION CONTROL | LS | $3 \%$ of Items 1-6 | N/A | \$ | 27,300 |
| 11 | LIGHTING | LS | 1 | \$50,000.00 | \$ | 50,000 |
| 12 | SIGNING/ M ARKING | LS | 1 | \$115,000.00 | \$ | 115,000 |
| 13 | WETLAND MITIGATION | LS | 0 |  | \$ |  |
| 14 | HAZMAT | LS | 0 |  | \$ |  |
| 15 | ROADWAY INCIDENTALS | LS | $35 \%$ of Items 1-6 | N/A | \$ | 318,200 |
| TOTAL ROADWAY COSTS (Items 1-15) |  |  |  |  | \$ | 1,556,000 |
| 16 | STRUCTURES |  |  |  |  |  |
| TOTAL STRUCTURE COSTS \$ |  |  |  |  |  |  |
| 17 | MOBILIZATION | LS | 8 \% of Items 1-16 | N/A | \$ | 124,500 |
| CONSTRUCTION SUBTOTAL (Items 1-17) |  |  |  |  | \$ | 1,680,500 |
| 18 | E\&C | LS | $12 \%$ of Items 1-17 | N/A | \$ | 201,700 |
| 19 | ROW Acquisition | LS | 1 | \$460,000.00 | \$ | 460,000 |
| TOTAL PROJECT COST |  |  |  |  | \$ | 2,350,000 |

## Assumptions

Pavement Structure: 8" Concrete over 8" Base Aggregate
Signing/ M arking includes two overhead sign structures
Intersection is constructed under traffic
ROW Acquisition includes moving three signs

# Interactive Highway Safety Design Model 

## Crash Prediction Evaluation Report

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## Report Overview

Report Generated: Feb 2, 2023 4:36 PM<br>Report Template: System: Single Page, 508 Compliant [System] (sscpm5, Nov 17, 2021 8:25 AM)

Evaluation Date: Thu Feb 02 16:35:56 CST 2023
IHSDM Version: v16.0.0 (Sep 30, 2020)
Site Set Crash Prediction Module: v|ModuleInfo.moduleVersion| (|ModuleInfo.moduleDate|)

User Name: efrailing
Organization Name:
Phone:
E-Mail:

Project Title: Winneconne Ave at Commercial St
Project Comment: Created Fri Jan 27 08:43:01 CST 2023
Project Unit System: U.S. Customary

Site Set: Existing Traffic Signal
Site Set Comment: Created Fri Jan 27 09:36:34 CST 2023
Site Set Version: v1

Evaluation Title: 2024-2033 Traffic Signal Analysis, WisDOT
Evaluation Comment: Created Thu Feb 02 16:35:34 CST 2023
Policy for Superelevation: AASHTO 2011 U.S. Customary
Calibration: WisDOT_Calibration_v16-2
Crash Distribution: WisDOT_Distributions_v16-2
Model/CMF: WisDOT_Models_v16-2
Note: A Model Data Set other than the HSM (Highway Safety Manual) Configuration was selected for this Evaluation. If Crash Modification Factors (CMFs) were modified, then the results will not be in accordance with the HSM (see HSM Appendix to Part C, section A.1.3).
First Year of Analysis: 2024
Last Year of Analysis: 2033
Empirical-Bayes Analysis: None

## Disclaimer Regarding Crash Prediction Method

## IMPORTANT NOTICE ABOUT COMPARING RESULTS FROM HIGHWAY SAFETY MANUAL FIRST EDITION (2010) MODELS TO RESULTS FROM NEW MODELS DEVELOPED UNDER NCHRP PROJECTS 17-70 AND 17-58

Since the publication of the Highway Safety Manual - First Edition (HSM-1), in 2010 by the American Association of State

Highway and Transportation Officials (AASHTO), multiple research efforts have been undertaken through the National Cooperative Highway Research Program (NCHRP) to develop safety performance models for road segment and intersection facility types that were not initially reflected in the HSM-1, in order to expand the breadth and depth of the HSM in the future.

The IHSDM Crash Prediction Module (CPM) is intended as a faithful implementation of HSM Part C predictive methods. As NCHRP projects to develop new predictive methods for the HSM are completed, FHWA works to incorporate the new methods into IHSDM, sometimes in advance of publication in the HSM. The following new crash predictive methods have been accepted by NCHRP project panels and incorporated into IHSDM, while pending AASHTO's approval for incorporation into a future edition of the HSM:

- Roundabouts: completed in 2018 under NCHRP Project 17-70, the new methods will provide improved outcomes for the safety analysis of roundabouts.
- 6+ lane and one-way urban/suburban arterials (including models for segments and intersections): completed under NCHRP Project 17-58.

However, in the absence of local calibration factors (see HSM-1 Part C, Appendix A for guidance on calibration of the predictive models), it is neither appropriate nor advisable to directly compare the results from new models (from NCHRP Projects 17-58 and 17-70) to results from HSM-1 models, as the models were not calibrated to the same base state data sets, and consequently can produce unexpected results. If local calibration factors are available and applied to both new models and HSM-1 models, then it may be appropriate to directly compare the results.[Note: Work being performed under NCHRP Project 17-72 (Update of Crash Modification Factors for the Highway Safety Manual) is expected to re-calibrate many of the old (HSM-1) and new (e.g., NCHRP 17-70) models to data from a single (or small number of) states, that would allow results from all models to be directly compared.]

The models produced for NCHRP Project 17-70 have independent value in terms of informing the design of a roundabout and assessing the effects of different design characteristics on the expected safety performance of a roundabout.

The HSM-1 interim method previously included in IHSDM for evaluating roundabouts on urban/suburban arterials (i.e., evaluating an existing intersection and then applying a Crash Modification Factor for replacing the existing intersection with a roundabout) has been deactivated in IHSDM, to minimize any confusion with the new roundabout methodology.

## Section Types

## Urban Arterial Site Set CPM Evaluation

Site Type

Type: 4SG
Calibration Factor: 1

Table 1. Evaluation and Crash Data (CSD) (if applicable) Intersection Sites

| $\left\|\begin{array}{c} \mathrm{sit} \\ \mathrm{e} \\ \mathrm{~N} \end{array}\right\|$ | Type | Highway | $\underset{\substack{\text { Site } \\ \text { Description }}}{\text { and }}$ | Major AADT | Minor AADT | Number of Aproac hes with Left- Turn Lanes | Number of Approas hes with Right- Turn Lanes | $\left\|\begin{array}{c} \text { Presen } \\ \text { ce of } \\ \text { Lighti } \\ \text { ng } \end{array}\right\|$ | Number of Approat hes ith Perrissi ve Left Turn Phasing | Number <br> of <br> oproac <br> hes with <br> Perrissi <br> veProte <br> cted or <br> Protete <br> d/Permi <br> ssive <br> seft- <br> Lurn <br> Thasing | Number of Approac hes with Protece d Left Turn Phasing | Number <br> of <br> Aproac <br> hes on <br> which <br> Rhigh <br> Turn on <br> Red is <br> Rrohibit <br> ed | Presen ce of Red Light Came Cam ras <br> Presen RedLight ras | Pedestrian Volumes Crossing all and Insectio n Less (crossings/ day) | Max. Number of Lanes Crossed by Pedestria ns | Number of Bus Bithos within 1000 fof Intersectio $n$ $n$ | Number of Schools within 1000 ft of Intersectio | Number of Alcohol Sales Establishme nts within 1000 ft of Intersection |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | $\begin{gathered} 4 \mathrm{GG} 2 \times 2 \\ \text { les } \end{gathered}$ | Winneco | $\begin{array}{r} \text { Winneconne } \\ \text { Ave \& } \\ \text { Commercial } \\ \text { Street } \\ \hline \end{array}$ | 2024: 16238; 2025: 16372; 2026: 16506; 2027: 16640; 2028: 16774; 2029: 16908; 2030: 17042; 2031: 17176; 2032: 17310; 2033: 17444 | 202: 14571; 2025: 14691; 2026: 14812; 2027: 14932; 2028: 15535; 2033: 15655 | 3 | 1 | yes | 1 | 3 | 0 | 0 | no | 240 | 4 | 4 | 1 | 2 |

Table 2. Predicted Crash Frequencies and Rates by Site

| Site <br> No. | Type | Highway | Site Description | Total Predicted Crashes for Evaluation Period | Predicted <br> Total Crash Frequency (crashes/yr) | Predicted FI <br> Crash <br> Frequency <br> (crashes/yr) | Predicted PDO Crash Frequency (crashes/yr) | Predicted Intersection Travel Crash Rate (crashes/million veh) | Intersection Crash Rate (crashes/yr) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 4SG | Winneconne Ave | Winneconne Ave \& Commercial Street | 49.508 | 4.9508 | 1.7902 | 3.1606 | 0.42 | 4.9508 |
|  |  | Total | Total | 49.508 | 4.9508 | 1.7902 | 3.1606 | 0.42 | 4.9508 |

Table 3. Predicted Crash Frequencies by Year (4SG)

| Year | Total Crashes | FI Crashes | Percent FI (\%) | PDO Crashes | Percent PDO (\%) |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 2024 | 4.74 | 1.72 | 36.218 | 3.02 | 63.782 |
| 2025 | 4.79 | 1.73 | 36.205 | 3.05 | 63.795 |
| 2026 | 4.83 | 1.75 | 36.191 | 3.08 | 63.809 |
| 2027 | 4.88 | 1.76 | 36.178 | 3.11 | 63.822 |
| 2028 | 4.93 | 1.78 | 36.166 | 3.15 | 63.834 |
| 2029 | 4.97 | 1.80 | 36.154 | 3.18 | 63.846 |
| 2030 | 5.02 | 1.81 | 36.142 | 3.21 | 63.858 |
| 2031 | 5.07 | 1.83 | 36.130 | 3.24 | 63.870 |
| 2032 | 5.12 | 1.85 | 36.119 | 3.27 | 63.881 |
| 2033 | 5.17 | 1.86 | 36.108 | 3.30 | 63.892 |
| Total | 49.51 | 17.90 | 36.160 | 31.61 | 63.840 |
| Average | 4.95 | 1.79 | 36.160 | 3.16 | 63.840 |

Note: Fatal and Injury Crashes and Property Damage Only Crashes do not necessarily sum up to Total Crashes because the distribution of these three crashes had been derived independently.

Table 4. Predicted 4SG Crash Type Distribution

| Element Type | Crash Type | FI <br> Crashes | Percent FI (\%) | PDO <br> Crashes | $\begin{aligned} & \text { Percent } \\ & \text { PDO (\%) } \end{aligned}$ | Total Crashes | Percent Total (\%) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Intersection | Collision with Animal | 0.00 | 0.0 | 0.05 | 0.1 | 0.05 | 0.1 |
| Intersection | Collision with Bicycle | 0.67 | 1.5 | 0.00 | 0.0 | 0.67 | 1.5 |
| Intersection | Collision with Fixed Object | 0.00 | 0.0 | 0.00 | 0.0 | 0.00 | 0.0 |
| Intersection | Non-Collision | 0.00 | 0.0 | 0.00 | 0.0 | 0.00 | 0.0 |
| Intersection | Collision with Other Object | 0.00 | 0.0 | 0.00 | 0.0 | 0.00 | 0.0 |
| Intersection | Other Single-vehicle Collision | 0.01 | 0.0 | 0.05 | 0.1 | 0.07 | 0.1 |
| Intersection | Collision with Parked Vehicle | 0.00 | 0.0 | 0.00 | 0.0 | 0.00 | 0.0 |
| Intersection | Collision with Pedestrian | 3.88 | 8.6 | 0.00 | 0.0 | 3.88 | 8.6 |
| Intersection | Total Intersection Single Vehicle Crashes | 4.57 | 10.1 | 0.10 | 0.2 | 4.67 | 10.4 |
| Intersection | Angle Collision | 5.50 | 12.2 | 8.80 | 19.5 | 14.30 | 31.7 |
| Intersection | Head-on Collision | 0.00 | 0.0 | 0.00 | 0.0 | 0.00 | 0.0 |
| Intersection | Other Multi-vehicle Collision | 0.30 | 0.7 | 2.51 | 5.6 | 2.81 | 6.2 |
| Intersection | Rear-end Collision | 6.16 | 13.7 | 11.51 | 25.5 | 17.66 | 39.1 |
| Intersection | Sideswipe | 0.56 | 1.2 | 5.12 | 11.3 | 5.68 | 12.6 |
| Intersection | Total Intersection Multiple Vehicle Crashes | 12.52 | 27.7 | 27.94 | 61.9 | 40.45 | 89.6 |
| Intersection | Total Intersection Crashes | 17.08 | 37.9 | 28.04 | 62.1 | 45.13 | 100.0 |
|  | Total Crashes | 17.08 | 37.9 | 28.04 | 62.1 | 45.13 | 100.0 |

Note: Fatal and Injury Crashes and Property Damage Only Crashes do not necessarily sum up to Total Crashes because the distribution of these three crashes had been derived independently.

# Interactive Highway Safety Design Model 

## Crash Prediction Evaluation Report

## Disclaimer

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## Notice

The use of the IHSDM software is being done strictly on a voluntary basis. In exchange for provision of IHSDM, the user agrees that the Federal Highway Administration (FHWA), U.S. Department of Transportation and any other agency of the Federal Government shall not be responsible for any errors, damage or other liability that may result from any and all use of the software, including installation and testing of the software. The user further agrees to hold the FHWA and the Federal Government harmless from any resulting liability. The user agrees that this hold harmless provision shall flow to any person to whom or any entity to which the user provides the IHSDM software. It is the user's full responsibility to inform any person to whom or any entity to which it provides the IHSDM software of this hold harmless provision.

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## Report Overview

Report Generated: Feb 2, 2023 4:38 PM<br>Report Template: System: Single Page, 508 Compliant [System] (sscpm5, Nov 17, 2021 8:25 AM)

Evaluation Date: Thu Feb 02 16:38:16 CST 2023
IHSDM Version: v16.0.0 (Sep 30, 2020)
Site Set Crash Prediction Module: v|ModuleInfo.moduleVersion| (|ModuleInfo.moduleDate|)

User Name: efrailing
Organization Name:
Phone:
E-Mail:

Project Title: Winneconne Ave at Commercial St
Project Comment: Created Fri Jan 27 08:43:01 CST 2023
Project Unit System: U.S. Customary

Site Set: Modified Traffic Signal
Site Set Comment: Copied from Existing Traffic Signal (v1)
Site Set Version: v1

Evaluation Title: 2024-2033 Modified Traffic Signal Analysis, WisDOT
Evaluation Comment: Created Thu Feb 02 16:37:58 CST 2023
Policy for Superelevation: AASHTO 2011 U.S. Customary
Calibration: WisDOT_Calibration_v16-2
Crash Distribution: WisDOT_Distributions_v16-2
Model/CMF: WisDOT_Models_v16-2
Note: A Model Data Set other than the HSM (Highway Safety Manual) Configuration was selected for this Evaluation. If Crash Modification Factors (CMFs) were modified, then the results will not be in accordance with the HSM (see HSM Appendix to Part C, section A.1.3).
First Year of Analysis: 2024
Last Year of Analysis: 2033
Empirical-Bayes Analysis: None

## Disclaimer Regarding Crash Prediction Method

## IMPORTANT NOTICE ABOUT COMPARING RESULTS FROM HIGHWAY SAFETY MANUAL FIRST EDITION (2010) MODELS TO RESULTS FROM NEW MODELS DEVELOPED UNDER NCHRP PROJECTS 17-70 AND 17-58

Since the publication of the Highway Safety Manual - First Edition (HSM-1), in 2010 by the American Association of State

Highway and Transportation Officials (AASHTO), multiple research efforts have been undertaken through the National Cooperative Highway Research Program (NCHRP) to develop safety performance models for road segment and intersection facility types that were not initially reflected in the HSM-1, in order to expand the breadth and depth of the HSM in the future.

The IHSDM Crash Prediction Module (CPM) is intended as a faithful implementation of HSM Part C predictive methods. As NCHRP projects to develop new predictive methods for the HSM are completed, FHWA works to incorporate the new methods into IHSDM, sometimes in advance of publication in the HSM. The following new crash predictive methods have been accepted by NCHRP project panels and incorporated into IHSDM, while pending AASHTO's approval for incorporation into a future edition of the HSM:

- Roundabouts: completed in 2018 under NCHRP Project 17-70, the new methods will provide improved outcomes for the safety analysis of roundabouts.
- 6+ lane and one-way urban/suburban arterials (including models for segments and intersections): completed under NCHRP Project 17-58.

However, in the absence of local calibration factors (see HSM-1 Part C, Appendix A for guidance on calibration of the predictive models), it is neither appropriate nor advisable to directly compare the results from new models (from NCHRP Projects 17-58 and 17-70) to results from HSM-1 models, as the models were not calibrated to the same base state data sets, and consequently can produce unexpected results. If local calibration factors are available and applied to both new models and HSM-1 models, then it may be appropriate to directly compare the results.[Note: Work being performed under NCHRP Project 17-72 (Update of Crash Modification Factors for the Highway Safety Manual) is expected to re-calibrate many of the old (HSM-1) and new (e.g., NCHRP 17-70) models to data from a single (or small number of) states, that would allow results from all models to be directly compared.]

The models produced for NCHRP Project 17-70 have independent value in terms of informing the design of a roundabout and assessing the effects of different design characteristics on the expected safety performance of a roundabout.

The HSM-1 interim method previously included in IHSDM for evaluating roundabouts on urban/suburban arterials (i.e., evaluating an existing intersection and then applying a Crash Modification Factor for replacing the existing intersection with a roundabout) has been deactivated in IHSDM, to minimize any confusion with the new roundabout methodology.

## Section Types

## Urban Arterial Site Set CPM Evaluation

## Site Type

Type: 4SG
Calibration Factor: 1

Table 1. Evaluation and Crash Data (CSD) (if applicable) Intersection Sites

| $\left\|\begin{array}{c\|} \text { sit } \\ \mathrm{e} \\ \mathrm{~N} \\ \mathrm{o} \end{array}\right\|$ | Type | Highway | $\underset{\text { Description }}{\text { Site }}$ | Major AADT | Minor AADT | Number of of Aproac hes with Left- Turn Lanes | Number of Aproac hes with Right- Turn Lanes | $\left\{\left.\begin{array}{c} \text { Presen } \\ \text { ce of } \\ \text { Lighti } \\ \text { ng } \end{array} \right\rvert\,\right.$ | Number of Aproac hes with Permisi ve Left Turn Phasing | Number <br> of <br> Aproac <br> hhes with <br> Permisi <br> ve/Prote <br> ceted <br> crotecte <br> PdTecti <br> daPerme <br> ssive <br> Left- <br> Turn <br> Phasing | Number of Approac hes with Protece d Left Turn Phasing | Number of Approac hes on which Right Turn on Red Rrobibit ed | Presen ce of RedLight Came ras | Pedestrian Volumes Crossing all and Intectio neess (crossings/ day) | Max. Number of Lanes Crossed by Pedestria ns | Number of Bus Stops within 1000 fof Intersectio $n$ | Number of Schools within 1000 ft of Intersectio $n$ $n$ | Number of Alcohol Sales Establishme nts within 1000 ft of Intersection |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | $\left.\begin{array}{\|c} 4 \mathrm{SG} 2 \times 2 \\ \mathrm{le5} \end{array} \right\rvert\,$ | Winneco nne Ave | $\begin{array}{r} \text { Winneconne } \\ \text { Ave \& } \\ \text { Commercial } \\ \text { Street } \end{array}$ | 2024: 16238; 2025: 16372; 2026: 16506; 2027: 16640; 2028: 16774; 2029: 16908; 2030: 17042; 2031: 17176; 2032: 17310; 2033: 17444 | $\begin{aligned} & \text { 2024: 14571; 2025: 14691; 2026: 14812; 2027: 14932; 2028: } \\ & \text { 15053; 2029: 15173; 2030: 15294; 2031: 15414; 2032: } \\ & \text { 15535; 2033: } 15655 \end{aligned}$ | 3 | 2 | yes | 1 | 2 | 1 | 0 | no | 240 | 4 | 4 | 1 | 2 |

Table 2. Predicted Crash Frequencies and Rates by Site

| Site <br> No. | Type | Highway | Site Description | Total Predicted Crashes for Evaluation Period | Predicted <br> Total Crash Frequency (crashes/yr) | Predicted FI <br> Crash <br> Frequency <br> (crashes/yr) | Predicted PDO Crash Frequency (crashes/yr) | Predicted Intersection Travel Crash Rate (crashes/million veh) | Intersection Crash Rate (crashes/yr) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 4SG | Winneconne Ave | Winneconne Ave \& Commercial Street | 45.398 | 4.5398 | 1.6639 | 2.8759 | 0.39 | 4.5398 |
|  |  | Total | Total | 45.398 | 4.5398 | 1.6639 | 2.8759 | 0.39 | 4.5398 |

Table 3. Predicted Crash Frequencies by Year (4SG)

| Year | Total Crashes | FI Crashes | Percent FI (\%) | PDO Crashes | Percent PDO (\%) |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 2024 | 4.35 | 1.60 | 36.724 | 2.75 | 63.276 |
| 2025 | 4.39 | 1.61 | 36.707 | 2.78 | 63.293 |
| 2026 | 4.43 | 1.63 | 36.691 | 2.81 | 63.309 |
| 2027 | 4.47 | 1.64 | 36.675 | 2.83 | 63.325 |
| 2028 | 4.52 | 1.66 | 36.659 | 2.86 | 63.341 |
| 2029 | 4.56 | 1.67 | 36.644 | 2.89 | 63.356 |
| 2030 | 4.60 | 1.69 | 36.629 | 2.92 | 63.371 |
| 2031 | 4.65 | 1.70 | 36.615 | 2.95 | 63.385 |
| 2032 | 4.69 | 1.72 | 36.600 | 2.97 | 63.400 |
| 2033 | 4.74 | 1.73 | 36.587 | 3.00 | 63.413 |
| Total | 45.40 | 16.64 | 36.652 | 28.76 | 63.348 |
| Average | 4.54 | 1.66 | 36.652 | 2.88 | 63.348 |

Note: Fatal and Injury Crashes and Property Damage Only Crashes do not necessarily sum up to Total Crashes because the distribution of these three crashes had been derived independently.

Table 4. Predicted 4SG Crash Type Distribution

| Element Type | Crash Type | FI <br> Crashes | Percent FI (\%) | PDO <br> Crashes | $\begin{aligned} & \text { Percent } \\ & \text { PDO (\%) } \end{aligned}$ | Total Crashes | Percent Total (\%) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Intersection | Collision with Animal | 0.00 | 0.0 | 0.05 | 0.1 | 0.05 | 0.1 |
| Intersection | Collision with Bicycle | 0.61 | 1.5 | 0.00 | 0.0 | 0.61 | 1.5 |
| Intersection | Collision with Fixed Object | 0.00 | 0.0 | 0.00 | 0.0 | 0.00 | 0.0 |
| Intersection | Non-Collision | 0.00 | 0.0 | 0.00 | 0.0 | 0.00 | 0.0 |
| Intersection | Collision with Other Object | 0.00 | 0.0 | 0.00 | 0.0 | 0.00 | 0.0 |
| Intersection | Other Single-vehicle Collision | 0.01 | 0.0 | 0.05 | 0.1 | 0.06 | 0.1 |
| Intersection | Collision with Parked Vehicle | 0.00 | 0.0 | 0.00 | 0.0 | 0.00 | 0.0 |
| Intersection | Collision with Pedestrian | 3.88 | 9.4 | 0.00 | 0.0 | 3.88 | 9.4 |
| Intersection | Total Intersection Single Vehicle Crashes | 4.50 | 10.9 | 0.09 | 0.2 | 4.60 | 11.1 |
| Intersection | Angle Collision | 5.01 | 12.1 | 8.01 | 19.3 | 13.02 | 31.4 |
| Intersection | Head-on Collision | 0.00 | 0.0 | 0.00 | 0.0 | 0.00 | 0.0 |
| Intersection | Other Multi-vehicle Collision | 0.27 | 0.7 | 2.29 | 5.5 | 2.56 | 6.2 |
| Intersection | Rear-end Collision | 5.61 | 13.5 | 10.47 | 25.3 | 16.07 | 38.8 |
| Intersection | Sideswipe | 0.51 | 1.2 | 4.66 | 11.2 | 5.17 | 12.5 |
| Intersection | Total Intersection Multiple Vehicle Crashes | 11.39 | 27.5 | 25.42 | 61.4 | 36.81 | 88.9 |
| Intersection | Total Intersection Crashes | 15.89 | 38.4 | 25.52 | 61.6 | 41.41 | 100.0 |
|  | Total Crashes | 15.89 | 38.4 | 25.52 | 61.6 | 41.41 | 100.0 |

Note: Fatal and Injury Crashes and Property Damage Only Crashes do not necessarily sum up to Total Crashes because the distribution of these three crashes had been derived independently.

# Interactive Highway Safety Design Model 

## Crash Prediction Evaluation Report

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## Report Overview

Report Generated: Feb 2, 2023 4:40 PM<br>Report Template: System: Single Page, 508 Compliant [System] (sscpm5, Nov 17, 2021 8:25 AM)

Evaluation Date: Thu Feb 02 16:40:32 CST 2023
IHSDM Version: v16.0.0 (Sep 30, 2020)
Site Set Crash Prediction Module: v|ModuleInfo.moduleVersion| (|ModuleInfo.moduleDate|)

User Name: efrailing
Organization Name:
Phone:
E-Mail:

Project Title: Winneconne Ave at Commercial St
Project Comment: Created Fri Jan 27 08:43:01 CST 2023
Project Unit System: U.S. Customary

Site Set: 4-Leg Roundabout
Site Set Comment: Created Fri Jan 27 11:25:57 CST 2023
Site Set Version: v1

Evaluation Title: 2024-2033 4-Leg Roundabout Analysis, WisDOT
Evaluation Comment: Created Thu Feb 02 16:40:11 CST 2023
Policy for Superelevation: AASHTO 2011 U.S. Customary
Calibration: WisDOT_Calibration_v16-2
Crash Distribution: WisDOT_Distributions_v16-2
Model/CMF: WisDOT_Models_v16-2
Note: A Model Data Set other than the HSM (Highway Safety Manual) Configuration was selected for this Evaluation. If Crash Modification Factors (CMFs) were modified, then the results will not be in accordance with the HSM (see HSM Appendix to Part C, section A.1.3).
First Year of Analysis: 2024
Last Year of Analysis: 2033
Empirical-Bayes Analysis: None

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## IMPORTANT NOTICE ABOUT COMPARING RESULTS FROM HIGHWAY SAFETY MANUAL FIRST EDITION (2010) MODELS TO RESULTS FROM NEW MODELS DEVELOPED UNDER NCHRP PROJECTS 17-70 AND 17-58

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Highway and Transportation Officials (AASHTO), multiple research efforts have been undertaken through the National Cooperative Highway Research Program (NCHRP) to develop safety performance models for road segment and intersection facility types that were not initially reflected in the HSM-1, in order to expand the breadth and depth of the HSM in the future.

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- Roundabouts: completed in 2018 under NCHRP Project 17-70, the new methods will provide improved outcomes for the safety analysis of roundabouts.
- 6+ lane and one-way urban/suburban arterials (including models for segments and intersections): completed under NCHRP Project 17-58.

However, in the absence of local calibration factors (see HSM-1 Part C, Appendix A for guidance on calibration of the predictive models), it is neither appropriate nor advisable to directly compare the results from new models (from NCHRP Projects 17-58 and 17-70) to results from HSM-1 models, as the models were not calibrated to the same base state data sets, and consequently can produce unexpected results. If local calibration factors are available and applied to both new models and HSM-1 models, then it may be appropriate to directly compare the results.[Note: Work being performed under NCHRP Project 17-72 (Update of Crash Modification Factors for the Highway Safety Manual) is expected to re-calibrate many of the old (HSM-1) and new (e.g., NCHRP 17-70) models to data from a single (or small number of) states, that would allow results from all models to be directly compared.]

The models produced for NCHRP Project 17-70 have independent value in terms of informing the design of a roundabout and assessing the effects of different design characteristics on the expected safety performance of a roundabout.

The HSM-1 interim method previously included in IHSDM for evaluating roundabouts on urban/suburban arterials (i.e., evaluating an existing intersection and then applying a Crash Modification Factor for replacing the existing intersection with a roundabout) has been deactivated in IHSDM, to minimize any confusion with the new roundabout methodology.

## Section Types

## Roundabout Site Set CPM Evaluation

## Site Type

Type: Roundabout USA 42R
Calibration Factor: USA 42R $=1.0$

Table 1. Evaluation and Crash Data (CSD) (if applicable) Roundabout - Homogeneous Sites

| Site No. | Type | Roundabout | Site Description | Area Type | Entering AADT |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | 42R - Roundabout with 4 legs and two circulating lanes | Winneconne Ave | Winneconne Ave \& Commercial St | Urban |  |

Table 2. Predicted Crash Frequencies and Rates by Site

| $\begin{aligned} & \text { Site } \\ & \text { No. } \end{aligned}$ | Type | Roundabout | Site Description | Total Predicted Crashes for Evaluation Period | Predicted Total Crash Frequency (crashes/yr) | Predicted FI Crash Frequency (crashes/ $/ \mathbf{y r}$ ) | Predicted PDO Crash Frequency (crashes/yr) | Predicted Intersection Travel Crash Rate (crashes/million veh) | Intersection Crash Rate (crashes/yr) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 42R - Roundabout with 4 legs and two circulating lanes | Winneconne Ave | Winneconne Ave \& Commercial St | 152.616 | 15.2616 | 2.3422 | 12.9194 | 3.27 | 15.2616 |
|  |  | Total | Total | 152.616 | 15.2616 | 2.3422 | 12.9194 | 3.27 | 15.2616 |

Table 3. Predicted Crash Frequencies by Year (Roundabout USA 42R)

| Year | Total Crashes | FI Crashes | Percent FI (\%) | PDO Crashes | Percent PDO (\%) |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 2024 | 14.63 | 2.23 | 15.277 | 12.39 | 84.723 |
| 2025 | 14.77 | 2.26 | 15.293 | 12.51 | 84.707 |
| 2026 | 14.91 | 2.28 | 15.308 | 12.63 | 84.692 |
| 2027 | 15.05 | 2.31 | 15.323 | 12.74 | 84.677 |
| 2028 | 15.19 | 2.33 | 15.339 | 12.86 | 84.661 |
| 2029 | 15.33 | 2.35 | 15.354 | 12.98 | 84.646 |
| 2030 | 15.47 | 2.38 | 15.369 | 13.09 | 84.631 |
| 2031 | 15.61 | 2.40 | 15.383 | 13.21 | 84.617 |
| 2032 | 15.75 | 2.43 | 15.398 | 13.33 | 84.602 |
| 2033 | 15.89 | 2.45 | 15.413 | 13.44 | 84.587 |
| Total | 152.62 | 23.42 | 15.347 | 129.19 | 84.653 |
| Average | 15.26 | 2.34 | 15.347 | 12.92 | 84.653 |

Note: Fatal and Injury Crashes and Property Damage Only Crashes do not necessarily sum up to Total Crashes because the distribution of these three crashes had been derived independently.

Table 4. Predicted Roundabout USA 42R Crash Severity

| Site No. | Fatal (K) <br> Crashes <br> (crashes) | Incapacitating Injury (A) <br> Crashes (crashes) | Non-Incapacitating Injury <br> (B) Crashes (crashes) | Possible Injury <br> (C) Crashes <br> (crashes) | No Injury (O) <br> Crashes <br> (crashes) |
| ---: | ---: | ---: | ---: | ---: | ---: |
| 1 | 0.1026 | 1.6417 | 6.8994 | 14.7781 | 129.1944 |
| Total | 0.1026 | 1.6417 | 6.8994 | 14.7781 | 129.1944 |

Table 5. Predicted Roundabout USA 42R Crash Type Distribution

| Element Type | Crash Type | FI <br> Crashes | Percent <br> FI (\%) | PDO <br> Crashes | Percent <br> PDO (\%) | Total <br> Crashes | Percent <br> Total (\%) |
| :--- | :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Intersection | Collision with Animal | 0.00 | 0.0 | 0.41 | 0.3 | 0.41 | 0.3 |
| Intersection | Collision with Fixed Object | 4.54 | 3.0 | 19.03 | 12.5 | 23.58 | 15.5 |
| Intersection | Collision with Other Object | 0.26 | 0.2 | 0.07 | 0.0 | 0.33 | 0.2 |
| Intersection | Other Single-vehicle Collision | 2.80 | 1.8 | 5.41 | 3.6 | 8.21 | 5.4 |
| Intersection | Collision with Parked Vehicle | 0.00 | 0.0 | 0.00 | 0.0 | 0.00 | 0.0 |
| Intersection | Total Single Vehicle Crashes | 7.60 | 5.0 | 24.92 | 16.4 | 32.52 | 21.4 |
| Intersection | Angle Collision | 3.58 | 2.4 | 23.48 | 15.4 | 27.07 | 17.8 |
| Intersection | Head-on Collision | 0.00 | 0.0 | 0.55 | 0.4 | 0.55 | 0.4 |
| Intersection | Other Multiple-vehicle Collision | 0.26 | 0.2 | 0.14 | 0.1 | 0.40 | 0.3 |
| Intersection | Rear-end Collision | 5.51 | 3.6 | 18.48 | 12.1 | 23.99 | 15.8 |
| Intersection | Sideswipe | 6.03 | 4.0 | 61.62 | 40.5 | 67.65 | 44.5 |
| Intersection | Total Multiple Vehicle Crashes | 15.38 | 10.1 | 104.27 | 68.5 | 119.65 | 78.6 |
| Intersection | Total Intersection Crashes | 22.98 | 15.1 | 129.19 | 84.9 | 152.18 | 100.0 |
|  | 22.98 | 15.1 | 129.19 | 84.9 | 152.18 | 100.0 |  |

Note: Fatal and Injury Crashes and Property Damage Only Crashes do not necessarily sum up to Total Crashes because the distribution of these three crashes had been derived independently.

# Interactive Highway Safety Design Model 

## Economic Analysis Report

February 2, 2023

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## Economic Analysis Report

Economic Analysis Report Overview

Report Generated: Feb 2, 2023 4:47 PM
Report Template: System: Single Page [System] (eam3, Nov 17, 2021 8:25 AM)

Evaluation Title: 2024-2033 Economic Analysis, WisDOT
Evaluation Comment: Created Thu Feb 02 16:47:04 CST 2023
Evaluation Date: Thu Feb 02 16:47:21 CST 2023

User Name: efrailing
Organization Name:
Phone:
E-Mail:

Project Title: Winneconne Ave at Commercial St
Project Comment: Created Tue Jan 31 15:54:42 CST 2023

## Configuration Summary

Crash Cost Configuration: WisDOTEconomics_v16-2
Configuration Comment: Updated with 2021 crash costs and '17-'21 crash proportions

Table 1. Economic Analysis Configuration

| Configuration Data |  |
| ---: | ---: |
| Crash Unit Cost Zero Year | $\mathbf{2 0 2 1}$ |
| Crash Cost Index | 0.00 |
| Discount Rate | 0.05 |
| KABCO Unit Costs | $\mathbf{1 3 , 0 2 1 , 4 8 9 . 0 0}$ |
| K Cost (\$/Crash) | $\mathbf{6 9 8 , 0 1 0 . 0 0}$ |
| A Cost (\$/Crash) | $\mathbf{2 2 0 , 7 1 7 . 0 0}$ |
| B Cost (\$/Crash) | $\mathbf{1 2 5 , 9 8 3 . 0 0}$ |
| C Cost (\$/Crash) | $\mathbf{1 6 , 0 3 4 . 0 0}$ |

Table 2. RTL Segment FI Proportion Data

| Segment Type | Fatal Crash (K) <br> Proportion of <br> FI (\%) | Incapacitating Injury <br> Crash (A) Proportion <br> of FI (\%) | Non-incapacitating <br> Injury Crash (B) <br> Proportion of FI (\%) | Possible Injury <br> Crash (C) <br> Proportion of <br> FI (\%) |
| :---: | :---: | :---: | :---: | :---: |
| RTL 2U Two-Lane Undivided | 3.916 | 12.980 |  | 47.819 |

Table 3. RTL Intersection FI Proportion Data

| Intersection Type | Fatal Crash (K) <br> Proportion of FI <br> $(\%)$ | Incapacitating Injury <br> Crash (A) Proportion of <br> FI (\%) | Non-incapacitating <br> Injury Crash (B) <br> Proportion of FI (\%) | Possible Injury <br> Crash (C) <br> Proportion of FI <br> $(\%)$ |
| ---: | ---: | ---: | ---: | ---: |
| RTL Three-Legged w/STOP control | 4.196 | 16.268 | 46.961 | 32.575 |
| RTL Four-Legged w/STOP control | 4.524 | 14.796 | 48.678 |  |
| RTL Four-Legged Signalized | 1.290 | 9.678 | 46.451 |  |

Table 4. RML Segment FI Proportion Data

| Segment Type | Fatal Crash (K) <br> Proportion of <br> FI (\%) | Incapacitating Injury <br> Crash (A) Proportion <br> of FI (\%) | Non-incapacitating <br> Injury Crash (B) <br> Proportion of FI (\%) | Possible Injury <br> Crash (C) <br> Proportion of <br> FI (\%) |
| ---: | ---: | ---: | ---: | ---: |
| RML Four-Lane Undivided | 3.916 | 12.980 | 47.819 | 35.286 |
| RML Four-Lane Divided | 3.916 | 12.980 | 47.819 | 35.286 |

Table 5. RML Intersection FI Proportion Data

| Intersection Type | Fatal Crash (K) <br> Proportion of FI <br> $(\%)$ | Incapacitating Injury <br> Crash (A) Proportion of <br> FI (\%) | Non-incapacitating <br> Injury Crash (B) <br> Proportion of FI (\%) | Possible Injury <br> Crash (C) <br> Proportion of FI <br> $(\%)$ |
| ---: | ---: | ---: | ---: | ---: |
| RML Three-Legged w/STOP control | 3.723 | 15.633 | 45.409 | 35.236 |
| RML Four-Legged w/STOP control | 4.307 | 16.285 | 47.779 | 31.628 |
| RML Four-Legged Signalized | 0.875 | 6.704 | 41.690 | 50.730 |

Table 6. USA Segment FI Proportion Data

| Segment Type | Fatal Crash (K) <br> Proportion of FI (\%) | Incapacitating Injury Crash (A) Proportion of FI (\%) | Non-incapacitating Injury Crash (B) Proportion of FI (\%) | Possible Injury Crash (C) <br> Proportion of FI (\%) |
| :---: | :---: | :---: | :---: | :---: |
| USA Two-Lane Undivided | 1.301 | 7.610 | 38.365 | 52.724 |
| USA Three-Lane w/Center TWLTL | 1.301 | 7.610 | 38.365 | 52.724 |
| USA Four-Lane Undivided | 1.301 | 7.610 | 38.365 | 52.724 |
| USA Four-Lane Divided | 1.301 | 7.610 | 38.365 | 52.724 |
| USA Five-Lane w/Center TWLTL | 1.301 | 7.610 | 38.365 | 52.724 |

Table 7. USA Intersection FI Proportion Data

| Intersection Type | Fatal Crash (K) <br> Proportion of FI <br> $(\%)$ | Incapacitating Injury <br> Crash (A) Proportion of <br> FI (\%) | Non-incapacitating <br> Injury Crash (B) <br> Proportion of FI (\%) | Possible Injury <br> Crash (C) <br> Proportion of FI <br> $(\%)$ |
| ---: | ---: | ---: | ---: | ---: |
| USA Three-Legged w/STOP control | 1.230 | 8.399 | 41.252 | 4. |
| USA Three-Legged Signalized | 0.623 | 4.506 | 35.042 | 49.120 |
| USA Four-Legged w/STOP control | 1.072 | 7.773 | 59.828 |  |
| USA Four-Legged Signalized | 0.706 | 5.399 | 42.745 |  |

## Analysis Output Summary

Analysis Type: Benefit/Cost

Table 8. Case Cost Summary

| Is <br> Base <br> Case | Title | Present Value <br> of Crash Cost <br> $\mathbf{( \$ )}$ | Present Value <br> of Other Cost <br> (\$) | Net Present <br> Value of <br> Benefits (B) (\$) | Net Present <br> Value of Costs <br> (C) (\$) | Present Value <br> of Net Benefit <br> (B-C) (\$) | Benefit Cost <br> Ratio (B/C) |
| :---: | :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Yes | Existing Traffic Signal | $1,827,075.56$ | 0.00 |  |  |  |  |
|  | Modified Traffic Signal | $1,688,556.94$ | $299,100.00$ | $138,518.62$ | $299,100.00$ | $-160,581.38$ | 0.4631 |
|  | 4-Leg Roundabout | $6,604,387.05$ | $1,932,600.00$ | $-4,777,311.49$ | $1,932,600.00$ | $-6,709,911.49$ | -2.4720 |

Table 9. Case Crash Summary

| Is <br> Base | Title | Fatal (K) <br> Crashes <br> (crashes) | Incapacitating <br> Injury (A) Crashes <br> (crashes) | Non-Incapacitating <br> Injury (B) Crashes <br> (crashes) | Possible <br> Injury (C) <br> Crashes <br> (crashes) | No Injury <br> (O) <br> Crashes <br> (crashes) | Total <br> Crashes <br> (crashes) |
| :--- | :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Yes | Existing Traffic Signal | 0.0509 | 0.3895 | 2.7063 | 4.0682 | 13.5512 | 20.7662 |
|  | Modified Traffic Signal | 0.0472 | 0.3606 | 2.5051 | 3.7658 | 12.3307 | 19.0093 |
|  | 4-Leg Roundabout | 0.1063 | 1.7010 |  | 7.1487 | 15.3122 | 133.3034 |

## Crash Cost Data

## Existing Traffic Signal Data

Case Title: Existing Traffic Signal
Is Base Case: true
Present Value of Crash Cost: $1,827,075.56$
Present Value of Other Cost: 0.00

## Table 10. Existing Traffic Signal Evaluation Cost

| Project or Interchange | Selected Facility | Selected Evaluation | Present Value of Crash Cost <br> $(\$)$ |
| :---: | :---: | :---: | :---: |
| Winneconne Ave at Commercial St | Existing Traffic Signal | $2022-2031$ Traffic Signal Analysis, WisDOT | $1,827,075.56$ |
| Total |  |  | $1,827,075.56$ |

Table 11. Existing Traffic Signal Evaluation Crashes

| Project or Interchange | Selected Facility | Selected Evaluation | Fatal (K) Crashes (crashes) | Incapacitating Injury (A) Crashes (crashes) | Non-Incapacitating Injury <br> (B) Crashes (crashes) | Possible Injury (C) Crashes (crashes) | No Injury (O) Crashes (crashes) | Total Crashes (crashes) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Winneconne Ave at Commercial St | Existing Traffic Signal | 2022-2031 Traffic Signal Analysis, WisDOT | 0.0509 | 0.3895 | 2.7063 | 4.0682 | 13.5512 | 20.7662 |
| Total |  |  | 0.0509 | 0.3895 | 2.7063 | 4.0682 | 13.5512 | 20.7662 |

Table 12. Existing Traffic Signal Facility Type Crashes

| Facility Type | Fatal (K) <br> Crashes <br> (crashes) | Incapacitating Injury (A) <br> Crashes (crashes) | Non-Incapacitating <br> Injury (B) Crashes <br> (crashes) | Possible <br> Injury (C) <br> Crashes <br> (crashes) | No Injury <br> (O) Crashes <br> (crashes) | Total <br> Crashes <br> (crashes) |
| :---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Urban/Suburban Arterial Intersection (5 Lanes or Fewer) | 0.0509 | 0.3895 | 2.7063 | 4.0682 | 13.5512 | 20.7662 |
| Total | 0.0509 | 0.3895 | 2.7063 | 4.0682 | 13.5512 | 20.7662 |

## Modified Traffic Signal Data

Case Title: Modified Traffic Signal
Is Base Case: false
Present Value of Crash Cost: $1,688,556.94$
Present Value of Other Cost: 299,100.00

## Table 13. Modified Traffic Signal Evaluation Cost

| Project or Interchange | Selected Facility | Selected Evaluation | Present Value of Crash <br> Cost (\$) |
| :---: | :---: | :--- | ---: |
| Winneconne Ave at Commercial St | Modified Traffic Signal | 2022-2031 Modified Traffic Signal Analysis, WisDOT |  |
| Total |  |  | $1,688,556.94$ |

Table 14. Modified Traffic Signal Evaluation Crashes

| Project or Interchange | Selected Facility | Selected Evaluation | Fatal (K) Crashes (crashes) | Incapacitating Injury (A) Crashes (crashes) | Non-Incapacitating Injury (B) Crashes (crashes) | Possible Injury (C) Crashes (crashes) | $\begin{aligned} & \text { No Injury (O) } \\ & \text { Crashes } \\ & \text { (crashes) } \end{aligned}$ | Total Crashes (crashes) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Winneconne Ave at Commercial St | Modified Traffic Signal | 2022-2031 Modified Traffic Signal Analysis, WisDot | 0.0472 | 0.3606 | 2.5051 | 3.7658 | 12.3307 | 19.0093 |
| Total |  |  | 0.0472 | 0.3606 | 2.5051 | 3.7658 | 12.3307 | 19.0093 |

Table 15. Modified Traffic Signal Facility Type Crashes

| Facility Type | Fatal (K) <br> Crashes <br> (crashes) | Incapacitating Injury (A) <br> Crashes (crashes) | Non-Incapacitating <br> Injury (B) Crashes <br> (crashes) | Possible <br> Injury (C) <br> Crashes <br> (crashes) | No Injury <br> (O) Crashes <br> (crashes) |
| :---: | ---: | ---: | ---: | ---: | ---: |
| Urban/Suburban Arterial Intersection (5 Lanes or Fewer) | 0.0472 | 0.3606 | Total <br> Crashes <br> (crashes) |  |  |
| Total | 0.0472 | 0.5051 | 3.7658 | 12.3307 | 19.0093 |
|  |  | 2.5051 | 3.7658 | 12.3307 | 19.0093 |

## 4-Leg Roundabout Data

Case Title: 4-Leg Roundabout
Is Base Case: false
Present Value of Crash Cost: 6,604,387.05
Present Value of Other Cost: $1,932,600.00$

Table 16. 4-Leg Roundabout Evaluation Cost

| Project or Interchange | Selected Facility | Selected Evaluation | Present Value of Crash <br> Cost (\$) |
| :---: | :--- | :--- | ---: |
| Winneconne Ave at Commercial St | 4-Leg Roundabout | 2022-2031 4-Leg Roundabout Analysis, WisDOT | $6,604,387.05$ |
| Total |  |  | $6,604,387.05$ |

Table 17. 4-Leg Roundabout Evaluation Crashes

| Project or Interchange | Selected Facility | Selected Evaluation | Fatal (K) Crashes (crashes) | Incapacitating Injury (A) Crashes (crashes) | Non-Incapacitating Injury <br> (B) Crashes (crashes) | Possible Injury <br> (C) Crashes (crashes) | $\begin{array}{\|c\|} \hline \text { No Injury (0) } \\ \text { Crashes } \\ \text { (crashes) } \\ \hline \end{array}$ | Total Crashes (crashes) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Winneconne Ave at Commercial St | 4-Leg Roundabout | 2022-2031 4-Leg Roundabout Analysis, WisDOT | 0.1063 | 1.7010 | 7.1487 | 15.3122 | 133.3034 | 157.5717 |
| Total |  |  | 0.1063 | 1.7010 | 7.1487 | 15.3122 | 133.3034 | 157.5717 |

Table 18. 4-Leg Roundabout Facility Type Crashes

| Facility Type | Fatal (K) <br> Crashes <br> (crashes) | Incapacitating Injury (A) <br> Crashes (crashes) | Non-Incapacitating Injury (B) <br> Crashes (crashes) | Possible Injury <br> (C) Crashes <br> (crashes) | No Injury (O) <br> Crashes (crashes) | Total Crashes <br> (crashes) |
| :---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Roundabout | 0.1063 | 1.7010 | 7.1487 | 15.3122 | 133.3034 | 157.5717 |
| Total | 0.1063 | 1.7010 | 7.1487 | 15.3122 | 133.3034 | 157.5717 |

## Evaluation Message

| Year |  | 114/Winneconne Ave at 114/Commercial St - AM Peak |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | SB |  |  | WB |  |  | NB |  |  | EB |  |  | Total |
|  |  | R | T | L | R | T | L | R | T | L | R | T | L |  |
| 2018 | Volume | 256 | 261 | 2 | 4 | 303 | 40 | 27 | 304 | 232 | 208 | 253 | 263 | 2153 |
| 2022 | Volume | 265 | 270 | 2 | 4 | 314 | 41 | 28 | 315 | 240 | 215 | 262 | 272 | 2228 |
| 2042 | Volume | 309 | 315 | 2 | 5 | 366 | 48 | 33 | 367 | 280 | 251 | 306 | 318 | 2600 |
|  |  |  | 4\% |  |  | 1\% |  |  | 3\% |  |  | 2\% |  |  |


| 114/Winneconne Ave at 114/ Commercial St - PM Peak |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Year |  | SB |  |  | WB |  |  | NB |  |  | EB |  |  | Total |
|  |  | R | T | L | R | T | L | R | T | L | R | T | L |  |
| 2018 | Volume | 385 | 334 | 12 | 7 | 293 | 51 | 35 | 368 | 136 | 212 | 239 | 279 | 2351 |
| 2022 | Volume | 398 | 346 | 12 | 7 | 303 | 53 | 36 | 381 | 141 | 219 | 247 | 289 | 2432 |
| 2042 | Volume | 465 | 404 | 15 | 8 | 354 | 62 | 42 | 445 | 164 | 256 | 289 | 337 | 2841 |
|  |  |  | 1\% |  |  | 1\% |  |  | 1\% |  |  | 1\% |  |  |



|  | 4 |  |  | 7 |  |  | $4$ | $\dagger$ | $p$ | ( | $\dagger$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ${ }^{*}$ | 4 | F | ${ }^{1}$ | $\hat{\beta}$ |  | ${ }^{1}$ | $\uparrow$ |  |  | * ${ }^{\text {d }}$ |  |
| Traffic Volume (vph) | 272 | 262 | 215 | 41 | 314 | 4 | 240 | 315 | 28 | 2 | 270 | 265 |
| Future Volume (vph) | 272 | 262 | 215 | 41 | 314 | 4 | 240 | 315 | 28 | 2 | 270 | 265 |
| Ideal Flow (vphpl) | 1785 | 1785 | 1750 | 1750 | 1750 | 1750 | 1750 | 1750 | 1750 | 1750 | 1750 | 1750 |
| Lane Width (ft) | 11 | 11 | 16 | 11 | 11 | 11 | 11 | 11 | 11 | 11 | 11 | 11 |
| Grade (\%) |  | 0\% |  |  | 0\% |  |  | 0\% |  |  | 0\% |  |
| Storage Length (ft) | 0 |  | 150 | 0 |  | 0 | 0 |  | 0 | 0 |  | 0 |
| Storage Lanes | 1 |  | 1 | 1 |  | 0 | 1 |  | 0 | 0 |  | 0 |
| Taper Length (ft) | 25 |  |  | 25 |  |  | 25 |  |  | 25 |  |  |
| Right Turn on Red |  |  | Yes |  |  | Yes |  |  | Yes |  |  | Yes |
| Link Speed (mph) |  | 30 |  |  | 25 |  |  | 30 |  |  | 25 |  |
| Link Distance (ft) |  | 548 |  |  | 403 |  |  | 539 |  |  | 1202 |  |
| Travel Time (s) |  | 12.5 |  |  | 11.0 |  |  | 12.3 |  |  | 32.8 |  |
| Confl. Peds. (\#/hr) |  |  |  |  |  |  |  |  |  |  |  |  |
| Confl. Bikes (\#/hr) |  |  |  |  |  |  |  |  |  |  |  |  |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Growth Factor | 100\% | 100\% | 62\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% |
| Heavy Vehicles (\%) | 1\% | 1\% | 1\% | 1\% | 1\% | 1\% | 1\% | 1\% | 1\% | 1\% | 1\% | 1\% |
| Bus Blockages (\#/hr) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Parking (\#/hr) |  |  |  |  |  |  |  |  |  |  |  |  |
| Mid-Block Traffic (\%) |  | 0\% |  |  | 0\% |  |  | 0\% |  |  | 0\% |  |
| Shared Lane Traffic (\%) |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Group Flow (vph) | 296 | 285 | 145 | 45 | 345 | 0 | 261 | 372 | 0 | 0 | 583 | 0 |
| Turn Type | pm+pt | NA | Perm | pm+pt | NA |  | pm+pt | NA |  | Perm | NA |  |
| Protected Phases | 3 | 8 |  | 7 | 4 |  | 1 | 6 |  |  | 2 |  |
| Permitted Phases | 8 |  | 8 | 4 |  |  | 6 |  |  | 2 |  |  |
| Detector Phase | 3 | 8 | 8 | 7 | 4 |  | 1 | 6 |  | 2 | 2 |  |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial (s) | 6.0 | 19.0 | 19.0 | 6.0 | 19.0 |  | 6.0 | 19.0 |  | 19.0 | 19.0 |  |
| Minimum Split (s) | 10.0 | 25.0 | 25.0 | 10.0 | 25.0 |  | 10.0 | 25.0 |  | 25.0 | 25.0 |  |
| Total Split (s) | 21.0 | 41.0 | 41.0 | 10.0 | 30.0 |  | 19.0 | 49.0 |  | 30.0 | 30.0 |  |
| Total Split (\%) | 21.0\% | 41.0\% | 41.0\% | 10.0\% | 30.0\% |  | 19.0\% | 49.0\% |  | 30.0\% | 30.0\% |  |
| Yellow Time (s) | 3.0 | 4.0 | 4.0 | 3.0 | 4.0 |  | 3.0 | 4.0 |  | 4.0 | 4.0 |  |
| All-Red Time (s) | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 |  | 1.0 | 1.0 |  | 1.0 | 1.0 |  |
| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  | 0.0 | 0.0 |  |  | 0.0 |  |
| Total Lost Time (s) | 4.0 | 5.0 | 5.0 | 4.0 | 5.0 |  | 4.0 | 5.0 |  |  | 5.0 |  |
| Lead/Lag | Lead | Lag | Lag | Lead | Lag |  | Lead |  |  | Lag | Lag |  |
| Lead-Lag Optimize? |  |  |  |  |  |  |  |  |  |  |  |  |
| Recall Mode | None | Min | Min | None | Max |  | None | C-Max |  | C-Max | C-Max |  |
| v/c Ratio | 0.75 | 0.42 | 0.19 | 0.12 | 0.76 |  | 0.79 | 0.51 |  |  | 0.64 |  |
| Control Delay | 29.9 | 25.2 | 4.5 | 16.5 | 47.0 |  | 37.1 | 22.9 |  |  | 28.4 |  |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  | 0.0 | 0.0 |  |  | 0.0 |  |
| Total Delay | 29.9 | 25.2 | 4.5 | 16.5 | 47.0 |  | 37.1 | 22.9 |  |  | 28.4 |  |
| Queue Length 50th (ft) | 118 | 138 | 0 | 15 | 206 |  | 106 | 164 |  |  | 127 |  |
| Queue Length 95th (ft) | 185 | 216 | 40 | 35 | \#355 |  | \#200 | 250 |  |  | 197 |  |
| Internal Link Dist (ft) |  | 468 |  |  | 323 |  |  | 459 |  |  | 1122 |  |
| Turn Bay Length (ft) |  |  | 150 |  |  |  |  |  |  |  |  |  |
| Base Capacity (vph) | 420 | 682 | 754 | 369 | 452 |  | 346 | 731 |  |  | 912 |  |
| Starvation Cap Reductn | 0 | 0 | 0 | 0 | 0 |  | 0 | 0 |  |  | 0 |  |


|  |  |  |  |  |  |  | 4 | $\dagger$ | 7 |  | $\ddagger$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Spillback Cap Reductn | 0 | 0 | 0 | 0 | 0 |  | 0 | 0 |  |  | 0 |  |
| Storage Cap Reductn | 0 | 0 | 0 | 0 | 0 |  | 0 | 0 |  |  | 0 |  |
| Reduced v/c Ratio | 0.70 | 0.42 | 0.19 | 0.12 | 0.76 |  | 0.75 | 0.51 |  |  | 0.64 |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| Area Type: OtherCycle Length: $100 \quad$ |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |
| Actuated Cycle Length: 100 |  |  |  |  |  |  |  |  |  |  |  |  |
| Offset: 0 (0\%), Referenced to phase 2:SBTL and 6:NBTL, Start of Green, Master Intersection |  |  |  |  |  |  |  |  |  |  |  |  |
| Natural Cycle: 75 |  |  |  |  |  |  |  |  |  |  |  |  |
| Control Type: Actuated-Coordinated |  |  |  |  |  |  |  |  |  |  |  |  |
| \# 95th percentile volume exceeds capacity, queue may be longer. |  |  |  |  |  |  |  |  |  |  |  |  |
| Queue shown is maximum after two cycles. |  |  |  |  |  |  |  |  |  |  |  |  |

Splits and Phases: 30: Commercial St \& Winneconne Ave


|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |


|  | 4 |  | $\checkmark$ | $\checkmark$ |  | 4 | 4 | $\dagger$ | $p$ | $1$ |  | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ${ }^{7}$ | 4 | F | ${ }^{7}$ | F |  | ${ }^{1}$ | F |  |  | ¢ $\uparrow$ |  |
| Traffic Volume (vph) | 289 | 247 | 219 | 53 | 303 | 7 | 141 | 381 | 36 | 12 | 346 | 398 |
| Future Volume (vph) | 289 | 247 | 219 | 53 | 303 | 7 | 141 | 381 | 36 | 12 | 346 | 398 |
| Ideal Flow (vphpl) | 1785 | 1785 | 1750 | 1750 | 1750 | 1750 | 1750 | 1750 | 1750 | 1750 | 1750 | 1750 |
| Lane Width (ft) | 11 | 11 | 16 | 11 | 11 | 11 | 11 | 11 | 11 | 11 | 11 | 11 |
| Grade (\%) |  | 0\% |  |  | 0\% |  |  | 0\% |  |  | 0\% |  |
| Storage Length (ft) | 0 |  | 150 | 0 |  | 0 | 0 |  | 0 | 0 |  | 0 |
| Storage Lanes | 1 |  | 1 | 1 |  | 0 | 1 |  | 0 | 0 |  | 0 |
| Taper Length (ft) | 25 |  |  | 25 |  |  | 25 |  |  | 25 |  |  |
| Right Turn on Red |  |  | Yes |  |  | Yes |  |  | Yes |  |  | Yes |
| Link Speed (mph) |  | 30 |  |  | 25 |  |  | 30 |  |  | 25 |  |
| Link Distance (ft) |  | 548 |  |  | 403 |  |  | 539 |  |  | 1202 |  |
| Travel Time (s) |  | 12.5 |  |  | 11.0 |  |  | 12.3 |  |  | 32.8 |  |
| Confl. Peds. (\#/hr) |  |  |  |  |  |  |  |  |  |  |  |  |
| Confl. Bikes (\#/hr) |  |  |  |  |  |  |  |  |  |  |  |  |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Growth Factor | 100\% | 100\% | 62\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% |
| Heavy Vehicles (\%) | 1\% | 1\% | 1\% | 1\% | 1\% | 1\% | 1\% | 1\% | 1\% | 1\% | 1\% | 1\% |
| Bus Blockages (\#/hr) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Parking (\#/hr) |  |  |  |  |  |  |  |  |  |  |  |  |
| Mid-Block Traffic (\%) |  | 0\% |  |  | 0\% |  |  | 0\% |  |  | 0\% |  |
| Shared Lane Traffic (\%) |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Group Flow (vph) | 314 | 268 | 148 | 58 | 337 | 0 | 153 | 453 | 0 | 0 | 822 | 0 |
| Turn Type | pm+pt | NA | Perm | pm+pt | NA |  | pm+pt | NA |  | Perm | NA |  |
| Protected Phases | 3 | 8 |  | 7 | 4 |  | 1 | 6 |  |  | 2 |  |
| Permitted Phases | 8 |  | 8 | 4 |  |  | 6 |  |  | 2 |  |  |
| Detector Phase | 3 | 8 | 8 | 7 | 4 |  | 1 | 6 |  | 2 | 2 |  |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial (s) | 6.0 | 19.0 | 19.0 | 6.0 | 19.0 |  | 6.0 | 19.0 |  | 19.0 | 19.0 |  |
| Minimum Split (s) | 10.0 | 25.0 | 25.0 | 10.0 | 25.0 |  | 10.0 | 25.0 |  | 25.0 | 25.0 |  |
| Total Split (s) | 21.0 | 42.0 | 42.0 | 10.0 | 31.0 |  | 19.0 | 48.0 |  | 29.0 | 29.0 |  |
| Total Split (\%) | 21.0\% | 42.0\% | 42.0\% | 10.0\% | 31.0\% |  | 19.0\% | 48.0\% |  | 29.0\% | 29.0\% |  |
| Yellow Time (s) | 3.0 | 4.0 | 4.0 | 3.0 | 4.0 |  | 3.0 | 4.0 |  | 4.0 | 4.0 |  |
| All-Red Time (s) | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 |  | 1.0 | 1.0 |  | 1.0 | 1.0 |  |
| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  | 0.0 | 0.0 |  |  | 0.0 |  |
| Total Lost Time (s) | 4.0 | 5.0 | 5.0 | 4.0 | 5.0 |  | 4.0 | 5.0 |  |  | 5.0 |  |
| Lead/Lag | Lead | Lag | Lag | Lead | Lag |  | Lead |  |  | Lag | Lag |  |
| Lead-Lag Optimize? |  |  |  |  |  |  |  |  |  |  |  |  |
| Recall Mode | None | Min | Min | None | Max |  | None | C-Max |  | C-Max | C-Max |  |
| v/c Ratio | 0.76 | 0.40 | 0.20 | 0.15 | 0.73 |  | 0.65 | 0.63 |  |  | 0.84 |  |
| Control Delay | 30.4 | 25.2 | 4.3 | 16.3 | 44.2 |  | 31.9 | 27.0 |  |  | 36.5 |  |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  | 0.0 | 0.0 |  |  | 0.0 |  |
| Total Delay | 30.4 | 25.2 | 4.3 | 16.3 | 44.2 |  | 31.9 | 27.0 |  |  | 36.5 |  |
| Queue Length 50th (ft) | 124 | 126 | 0 | 19 | 199 |  | 59 | 218 |  |  | 222 |  |
| Queue Length 95th (ft) | \#201 | 198 | 39 | 41 | \#332 |  | 111 | 327 |  |  | \#336 |  |
| Internal Link Dist (ft) |  | 468 |  |  | 323 |  |  | 459 |  |  | 1122 |  |
| Turn Bay Length (ft) |  |  | 150 |  |  |  |  |  |  |  |  |  |
| Base Capacity (vph) | 430 | 665 | 740 | 380 | 462 |  | 299 | 714 |  |  | 982 |  |
| Starvation Cap Reductn | 0 | 0 | 0 | 0 | 0 |  | 0 | 0 |  |  | 0 |  |

2022 Base Year Background
Existing Transportation System
MSA-EF 11/21/2022

|  |  |  |  |  |  |  | 4 | $\dagger$ | 7 |  | $\ddagger$ | 4 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Spillback Cap Reductn | 0 | 0 | 0 | 0 | 0 |  | 0 | 0 |  |  | 0 |  |
| Storage Cap Reductn | 0 | 0 | 0 | 0 | 0 |  | 0 | 0 |  |  | 0 |  |
| Reduced v/c Ratio | 0.73 | 0.40 | 0.20 | 0.15 | 0.73 |  | 0.51 | 0.63 |  |  | 0.84 |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| Area Type: | Other |  |  |  |  |  |  |  |  |  |  |  |
| Cycle Length: 100 |  |  |  |  |  |  |  |  |  |  |  |  |
| Actuated Cycle Length: 100 |  |  |  |  |  |  |  |  |  |  |  |  |
| Offset: 0 (0\%), Referenced to phase 2:SBTL and 6:NBTL, Start of Green, Master Intersection |  |  |  |  |  |  |  |  |  |  |  |  |
| Natural Cycle: 70 |  |  |  |  |  |  |  |  |  |  |  |  |
| Control Type: Actuated-Coordinated |  |  |  |  |  |  |  |  |  |  |  |  |
| \# 95th percentile volume exceeds capacity, queue may be longer. |  |  |  |  |  |  |  |  |  |  |  |  |
| Queue shown is maximum after two cycles. |  |  |  |  |  |  |  |  |  |  |  |  |

Splits and Phases: 30: Commercial St \& Winneconne Ave


|  | 4 |  | $\checkmark$ | 7 |  |  | 4 | 4 | \% |  | $\downarrow$ | $\pm$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ${ }^{7}$ | 4 | F' | ${ }^{7}$ | $\uparrow$ |  | ${ }^{7}$ | $\uparrow$ |  |  | * ${ }^{\text {F }}$ |  |
| Traffic Volume (veh/h) | 289 | 247 | 219 | 53 | 303 | 7 | 141 | 381 | 36 | 12 | 346 | 398 |
| Future Volume (veh/h) | 289 | 247 | 219 | 53 | 303 | 7 | 141 | 381 | 36 | 12 | 346 | 398 |
| Initial Q (Qb), veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Work Zone On Approach |  | No |  |  | No |  |  | No |  |  | No |  |
| Adj Sat Flow, veh/h/ln | 1771 | 1771 | 1806 | 1736 | 1736 | 1736 | 1736 | 1736 | 1736 | 1736 | 1736 | 1736 |
| Adj Flow Rate, veh/h | 314 | 268 | 148 | 58 | 329 | 8 | 153 | 414 | 39 | 13 | 376 | 433 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Percent Heavy Veh, \% | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 |
| Cap, veh/h | 416 | 646 | 558 | 397 | 439 | 11 | 207 | 699 | 66 | 45 | 554 | 438 |
| Arrive On Green | 0.15 | 0.36 | 0.36 | 0.05 | 0.26 | 0.26 | 0.08 | 0.45 | 0.45 | 0.11 | 0.11 | 0.11 |
| Sat Flow, veh/h | 1687 | 1771 | 1530 | 1654 | 1688 | 41 | 1654 | 1563 | 147 | 23 | 1694 | 1339 |
| Grp Volume(v), veh/h | 314 | 268 | 148 | 58 | 0 | 337 | 153 | 0 | 453 | 389 | 0 | 433 |
| Grp Sat Flow(s),veh/h/ln | 1687 | 1771 | 1530 | 1654 | 0 | 1729 | 1654 | 0 | 1710 | 1717 | 0 | 1339 |
| Q Serve(g_s), s | 13.0 | 11.3 | 6.8 | 2.5 | 0.0 | 17.9 | 5.8 | 0.0 | 19.9 | 2.3 | 0.0 | 32.3 |
| Cycle Q Clear(g_c), s | 13.0 | 11.3 | 6.8 | 2.5 | 0.0 | 17.9 | 5.8 | 0.0 | 19.9 | 21.6 | 0.0 | 32.3 |
| Prop In Lane | 1.00 |  | 1.00 | 1.00 |  | 0.02 | 1.00 |  | 0.09 | 0.03 |  | 1.00 |
| Lane Grp Cap(c), veh/h | 416 | 646 | 558 | 397 | 0 | 450 | 207 | 0 | 765 | 599 | 0 | 438 |
| V/C Ratio(X) | 0.75 | 0.41 | 0.27 | 0.15 | 0.00 | 0.75 | 0.74 | 0.00 | 0.59 | 0.65 | 0.00 | 0.99 |
| Avail Cap(c_a), veh/h | 445 | 655 | 566 | 417 | 0 | 450 | 323 | 0 | 765 | 599 | 0 | 438 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.33 | 0.33 | 0.33 |
| Upstream Filter(l) | 1.00 | 1.00 | 1.00 | 1.00 | 0.00 | 1.00 | 1.00 | 0.00 | 1.00 | 0.93 | 0.00 | 0.93 |
| Uniform Delay (d), s/veh | 22.6 | 23.8 | 22.3 | 24.8 | 0.0 | 34.0 | 24.1 | 0.0 | 20.8 | 39.6 | 0.0 | 44.4 |
| Incr Delay (d2), s/veh | 6.7 | 0.4 | 0.3 | 0.2 | 0.0 | 10.9 | 5.1 | 0.0 | 3.4 | 5.0 | 0.0 | 38.7 |
| Initial Q Delay(d3),s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| \%ile BackOfQ(95\%),veh/ln | 9.7 | 8.3 | 4.4 | 1.8 | 0.0 | 13.7 | 4.5 | 0.0 | 13.1 | 16.1 | 0.0 | 22.7 |
| Unsig. Movement Delay, s/veh |  |  |  |  |  |  |  |  |  |  |  |  |
| LnGrp Delay(d),s/veh | 29.3 | 24.2 | 22.6 | 25.0 | 0.0 | 44.9 | 29.2 | 0.0 | 24.1 | 44.7 | 0.0 | 83.2 |
| LnGrp LOS | C | C | C | C | A | D | C | A | C | D | A | F |
| Approach Vol, veh/h |  | 730 |  |  | 395 |  |  | 606 |  |  | 822 |  |
| Approach Delay, s/veh |  | 26.1 |  |  | 42.0 |  |  | 25.4 |  |  | 64.9 |  |
| Approach LOS |  | C |  |  | D |  |  | C |  |  | E |  |
| Timer - Assigned Phs | 1 | 2 | 3 | 4 |  | 6 | 7 | 8 |  |  |  |  |
| Phs Duration ( $G+Y+R c$ ), $s$ | 12.0 | 37.7 | 19.3 | 31.0 |  | 49.7 | 8.8 | 41.5 |  |  |  |  |
| Change Period ( $\mathrm{Y}+\mathrm{Rc}$ ), s | 4.0 | 5.0 | 4.0 | 5.0 |  | 5.0 | 4.0 | 5.0 |  |  |  |  |
| Max Green Setting (Gmax), s | 15.0 | 24.0 | 17.0 | 26.0 |  | 43.0 | 6.0 | 37.0 |  |  |  |  |
| Max Q Clear Time ( $\mathrm{g}_{\sim} \mathrm{c}+11$ ), s | 7.8 | 0.0 | 15.0 | 0.0 |  | 0.0 | 4.5 | 0.0 |  |  |  |  |
| Green Ext Time (p_c), s | 0.3 | 0.0 | 0.3 | 0.0 |  | 0.0 | 0.0 | 0.0 |  |  |  |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| HCM 6th Ctrl Delay 40.9 |  |  |  |  |  |  |  |  |  |  |  |  |
| HCM 6th LOS |  |  | D |  |  |  |  |  |  |  |  |  |


|  | 4 |  |  | 7 |  |  | $4$ | $\dagger$ | $p$ | ( | $\dagger$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ${ }^{7}$ | 4 | F | ${ }^{1}$ | $\hat{\beta}$ |  | ${ }^{1}$ | $\uparrow$ |  |  | * ${ }^{\text {d }}$ |  |
| Traffic Volume (vph) | 318 | 306 | 251 | 48 | 366 | 5 | 280 | 367 | 33 | 2 | 315 | 309 |
| Future Volume (vph) | 318 | 306 | 251 | 48 | 366 | 5 | 280 | 367 | 33 | 2 | 315 | 309 |
| Ideal Flow (vphpl) | 1785 | 1785 | 1750 | 1750 | 1750 | 1750 | 1750 | 1750 | 1750 | 1750 | 1750 | 1750 |
| Lane Width (ft) | 11 | 11 | 16 | 11 | 11 | 11 | 11 | 11 | 11 | 11 | 11 | 11 |
| Grade (\%) |  | 0\% |  |  | 0\% |  |  | 0\% |  |  | 0\% |  |
| Storage Length (ft) | 0 |  | 150 | 0 |  | 0 | 0 |  | 0 | 0 |  | 0 |
| Storage Lanes | 1 |  | 1 | 1 |  | 0 | 1 |  | 0 | 0 |  | 0 |
| Taper Length (ft) | 25 |  |  | 25 |  |  | 25 |  |  | 25 |  |  |
| Right Turn on Red |  |  | Yes |  |  | Yes |  |  | Yes |  |  | Yes |
| Link Speed (mph) |  | 30 |  |  | 25 |  |  | 30 |  |  | 25 |  |
| Link Distance (ft) |  | 548 |  |  | 403 |  |  | 539 |  |  | 1202 |  |
| Travel Time (s) |  | 12.5 |  |  | 11.0 |  |  | 12.3 |  |  | 32.8 |  |
| Confl. Peds. (\#/hr) |  |  |  |  |  |  |  |  |  |  |  |  |
| Confl. Bikes (\#/hr) |  |  |  |  |  |  |  |  |  |  |  |  |
| Peak Hour Factor | 0.83 | 0.83 | 0.83 | 0.83 | 0.83 | 0.83 | 0.83 | 0.83 | 0.83 | 0.83 | 0.83 | 0.83 |
| Growth Factor | 100\% | 100\% | 62\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% |
| Heavy Vehicles (\%) | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% | 3\% | 3\% | 3\% | 4\% | 4\% | 4\% |
| Bus Blockages (\#/hr) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Parking (\#/hr) |  |  |  |  |  |  |  |  |  |  |  |  |
| Mid-Block Traffic (\%) |  | 0\% |  |  | 0\% |  |  | 0\% |  |  | 0\% |  |
| Shared Lane Traffic (\%) |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Group Flow (vph) | 383 | 369 | 187 | 58 | 447 | 0 | 337 | 482 | 0 | 0 | 754 | 0 |
| Turn Type | pm+pt | NA | Perm | pm+pt | NA |  | pm+pt | NA |  | Perm | NA |  |
| Protected Phases | 3 | 8 |  | 7 | 4 |  | 1 | 6 |  |  | 2 |  |
| Permitted Phases | 8 |  | 8 | 4 |  |  | 6 |  |  | 2 |  |  |
| Detector Phase | 3 | 8 | 8 | 7 | 4 |  | 1 | 6 |  | 2 | 2 |  |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial (s) | 6.0 | 19.0 | 19.0 | 6.0 | 19.0 |  | 6.0 | 19.0 |  | 19.0 | 19.0 |  |
| Minimum Split (s) | 10.0 | 25.0 | 25.0 | 10.0 | 25.0 |  | 10.0 | 25.0 |  | 25.0 | 25.0 |  |
| Total Split (s) | 22.0 | 42.0 | 42.0 | 10.0 | 30.0 |  | 20.0 | 48.0 |  | 28.0 | 28.0 |  |
| Total Split (\%) | 22.0\% | 42.0\% | 42.0\% | 10.0\% | 30.0\% |  | 20.0\% | 48.0\% |  | 28.0\% | 28.0\% |  |
| Yellow Time (s) | 3.0 | 4.0 | 4.0 | 3.0 | 4.0 |  | 3.0 | 4.0 |  | 4.0 | 4.0 |  |
| All-Red Time (s) | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 |  | 1.0 | 1.0 |  | 1.0 | 1.0 |  |
| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  | 0.0 | 0.0 |  |  | 0.0 |  |
| Total Lost Time (s) | 4.0 | 5.0 | 5.0 | 4.0 | 5.0 |  | 4.0 | 5.0 |  |  | 5.0 |  |
| Lead/Lag | Lead | Lag | Lag | Lead | Lag |  | Lead |  |  | Lag | Lag |  |
| Lead-Lag Optimize? |  | Yes | Yes | Yes |  |  |  |  |  |  |  |  |
| Recall Mode | None | Max | Max | None | Min |  | None | C-Max |  | C-Max | C-Max |  |
| v/c Ratio | 1.07 | 0.56 | 0.25 | 0.18 | 1.08 |  | 1.06 | 0.69 |  |  | 0.94 |  |
| Control Delay | 96.3 | 28.7 | 4.1 | 16.9 | 104.4 |  | 93.2 | 29.0 |  |  | 44.5 |  |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  | 0.0 | 0.0 |  |  | 0.0 |  |
| Total Delay | 96.3 | 28.7 | 4.1 | 16.9 | 104.4 |  | 93.2 | 29.0 |  |  | 44.5 |  |
| Queue Length 50th (ft) | ~226 | 187 | 0 | 19 | ~320 |  | ~188 | 239 |  |  | 195 |  |
| Queue Length 95th (ft) | \#355 | 253 | 33 | 38 | \#452 |  | \#315 | 316 |  |  | \#257 |  |
| Internal Link Dist (ft) |  | 468 |  |  | 323 |  |  | 459 |  |  | 1122 |  |
| Turn Bay Length (ft) |  |  | 150 |  |  |  |  |  |  |  |  |  |
| Base Capacity (vph) | 357 | 660 | 758 | 328 | 414 |  | 319 | 701 |  |  | 804 |  |
| Starvation Cap Reductn | 0 | 0 | 0 | 0 | 0 |  | 0 | 0 |  |  | 0 |  |


|  | 4 | $\rightarrow$ | $\checkmark$ | 7 |  |  | 4 | $\dagger$ | \% | $\pm$ | $\dagger$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Spillback Cap Reductn | 0 | 0 | 0 | 0 | 0 |  | 0 | 0 |  |  | 0 |  |
| Storage Cap Reductn | 0 | 0 | 0 | 0 | 0 |  | 0 | 0 |  |  | 0 |  |
| Reduced v/c Ratio | 1.07 | 0.56 | 0.25 | 0.18 | 1.08 |  | 1.06 | 0.69 |  |  | 0.94 |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| Area Type: |  |  |  |  |  |  |  |  |  |  |  |  |

Cycle Length: 100
Actuated Cycle Length: 100
Offset: $0(0 \%)$, Referenced to phase 2:SBTL and 6:NBTL, Start of Green, Master Intersection
Natural Cycle: 90
Control Type: Actuated-Coordinated
~ Volume exceeds capacity, queue is theoretically infinite.
Queue shown is maximum after two cycles.
\# 95th percentile volume exceeds capacity, queue may be longer.
Queue shown is maximum after two cycles.
Splits and Phases: 30: Commercial St \& Winneconne Ave


|  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |


|  | 4 |  |  | 7 |  |  | $4$ | $\dagger$ | $p$ | ( | $\dagger$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ${ }^{*}$ | 4 | F | ${ }^{1}$ | $\uparrow$ |  | ${ }^{1}$ | $\uparrow$ |  |  | * ${ }^{\text {W }}$ |  |
| Traffic Volume (vph) | 337 | 289 | 256 | 62 | 354 | 8 | 164 | 445 | 42 | 15 | 404 | 465 |
| Future Volume (vph) | 337 | 289 | 256 | 62 | 354 | 8 | 164 | 445 | 42 | 15 | 404 | 465 |
| Ideal Flow (vphpl) | 1785 | 1785 | 1750 | 1750 | 1750 | 1750 | 1750 | 1750 | 1750 | 1750 | 1750 | 1750 |
| Lane Width (ft) | 11 | 11 | 16 | 11 | 11 | 11 | 11 | 11 | 11 | 11 | 11 | 11 |
| Grade (\%) |  | 0\% |  |  | 0\% |  |  | 0\% |  |  | 0\% |  |
| Storage Length (ft) | 0 |  | 150 | 0 |  | 0 | 0 |  | 0 | 0 |  | 0 |
| Storage Lanes | 1 |  | 1 | 1 |  | 0 | 1 |  | 0 | 0 |  | 0 |
| Taper Length (ft) | 25 |  |  | 25 |  |  | 25 |  |  | 25 |  |  |
| Right Turn on Red |  |  | Yes |  |  | Yes |  |  | Yes |  |  | Yes |
| Link Speed (mph) |  | 30 |  |  | 25 |  |  | 30 |  |  | 25 |  |
| Link Distance (ft) |  | 548 |  |  | 403 |  |  | 539 |  |  | 1202 |  |
| Travel Time (s) |  | 12.5 |  |  | 11.0 |  |  | 12.3 |  |  | 32.8 |  |
| Confl. Peds. (\#/hr) |  |  |  |  |  |  |  |  |  |  |  |  |
| Confl. Bikes (\#/hr) |  |  |  |  |  |  |  |  |  |  |  |  |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Growth Factor | 100\% | 100\% | 62\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% |
| Heavy Vehicles (\%) | 1\% | 1\% | 1\% | 1\% | 1\% | 1\% | 1\% | 1\% | 1\% | 1\% | 1\% | 1\% |
| Bus Blockages (\#/hr) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Parking (\#/hr) |  |  |  |  |  |  |  |  |  |  |  |  |
| Mid-Block Traffic (\%) |  | 0\% |  |  | 0\% |  |  | 0\% |  |  | 0\% |  |
| Shared Lane Traffic (\%) |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Group Flow (vph) | 366 | 314 | 173 | 67 | 394 | 0 | 178 | 530 | 0 | 0 | 960 | 0 |
| Turn Type | pm+pt | NA | Perm | pm+pt | NA |  | pm+pt | NA |  | Perm | NA |  |
| Protected Phases | 3 | 8 |  | 7 | 4 |  | 1 | 6 |  |  | 2 |  |
| Permitted Phases | 8 |  | 8 | 4 |  |  | 6 |  |  | 2 |  |  |
| Detector Phase | 3 | 8 | 8 | 7 | 4 |  | 1 | 6 |  | 2 | 2 |  |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial (s) | 6.0 | 19.0 | 19.0 | 6.0 | 19.0 |  | 6.0 | 19.0 |  | 19.0 | 19.0 |  |
| Minimum Split (s) | 10.0 | 25.0 | 25.0 | 10.0 | 25.0 |  | 10.0 | 25.0 |  | 25.0 | 25.0 |  |
| Total Split (s) | 21.0 | 42.0 | 42.0 | 10.0 | 31.0 |  | 19.0 | 48.0 |  | 29.0 | 29.0 |  |
| Total Split (\%) | 21.0\% | 42.0\% | 42.0\% | 10.0\% | 31.0\% |  | 19.0\% | 48.0\% |  | 29.0\% | 29.0\% |  |
| Yellow Time (s) | 3.0 | 4.0 | 4.0 | 3.0 | 4.0 |  | 3.0 | 4.0 |  | 4.0 | 4.0 |  |
| All-Red Time (s) | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 |  | 1.0 | 1.0 |  | 1.0 | 1.0 |  |
| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  | 0.0 | 0.0 |  |  | 0.0 |  |
| Total Lost Time (s) | 4.0 | 5.0 | 5.0 | 4.0 | 5.0 |  | 4.0 | 5.0 |  |  | 5.0 |  |
| Lead/Lag | Lead | Lag | Lag | Lead | Lag |  | Lead |  |  | Lag | Lag |  |
| Lead-Lag Optimize? |  |  |  |  |  |  |  |  |  |  |  |  |
| Recall Mode | None | Min | Min | None | Max |  | None | C-Max |  | C-Max | C-Max |  |
| v/c Ratio | 0.97 | 0.47 | 0.23 | 0.19 | 0.91 |  | 0.71 | 0.74 |  |  | 1.00 |  |
| Control Delay | 62.2 | 26.6 | 4.2 | 16.8 | 62.5 |  | 36.1 | 31.3 |  |  | 61.3 |  |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  | 0.0 | 0.0 |  |  | 0.0 |  |
| Total Delay | 62.2 | 26.6 | 4.2 | 16.8 | 62.5 |  | 36.1 | 31.3 |  |  | 61.3 |  |
| Queue Length 50th (ft) | 161 | 152 | 0 | 22 | 243 |  | 70 | 273 |  |  | ~282 |  |
| Queue Length 95th (ft) | \#347 | 235 | 42 | 46 | \#420 |  | 133 | 406 |  |  | \#442 |  |
| Internal Link Dist (ft) |  | 468 |  |  | 323 |  |  | 459 |  |  | 1122 |  |
| Turn Bay Length (ft) |  |  | 150 |  |  |  |  |  |  |  |  |  |
| Base Capacity (vph) | 378 | 665 | 756 | 353 | 434 |  | 301 | 714 |  |  | 956 |  |
| Starvation Cap Reductn | 0 | 0 | 0 | 0 | 0 |  | 0 | 0 |  |  | 0 |  |


|  |  |  |  |  |  |  |  | 4 | \% | $\pm$ | $\frac{1}{1}$ | 4 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Spillback Cap Reductn | 0 | 0 | 0 | 0 | 0 |  | 0 | 0 |  |  | 0 |  |
| Storage Cap Reductn | 0 | 0 | 0 | 0 | 0 |  | 0 | 0 |  |  | 0 |  |
| Reduced v/c Ratio | 0.97 | 0.47 | 0.23 | 0.19 | 0.91 |  | 0.59 | 0.74 |  |  | 1.00 |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| Area Type: <br> Other | Other |  |  |  |  |  |  |  |  |  |  |  |
| Cycle Length: 100 |  |  |  |  |  |  |  |  |  |  |  |  |
| Actuated Cycle Length: 100 |  |  |  |  |  |  |  |  |  |  |  |  |
| Offset: 0 (0\%), Referenced to phase 2:SBTL and 6:NBTL, Start of Green, Master Intersection |  |  |  |  |  |  |  |  |  |  |  |  |
| Natural Cycle: 75 |  |  |  |  |  |  |  |  |  |  |  |  |
| Control Type: Actuated-Coordinated |  |  |  |  |  |  |  |  |  |  |  |  |
| ~ Volume exceeds capacity, queue is theoretically infinite. |  |  |  |  |  |  |  |  |  |  |  |  |
| Queue shown is maximum after two cycles. |  |  |  |  |  |  |  |  |  |  |  |  |
| \# 95th percentile volume exceeds capacity, queue may be longer. |  |  |  |  |  |  |  |  |  |  |  |  |
| Queue shown is maximum after two cycles. |  |  |  |  |  |  |  |  |  |  |  |  |

Splits and Phases: 30: Commercial St \& Winneconne Ave


|  | 4 |  | $\checkmark$ | 7 |  |  | 4 | 4 | \% |  | $\pm$ | $\pm$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ${ }^{*}$ | 4 | 7 | ${ }^{7}$ | $\uparrow$ |  | ${ }^{7}$ | $\uparrow$ |  |  | $\uparrow \uparrow$ |  |
| Traffic Volume (veh/h) | 337 | 289 | 256 | 62 | 354 | 8 | 164 | 445 | 42 | 15 | 404 | 465 |
| Future Volume (veh/h) | 337 | 289 | 256 | 62 | 354 | 8 | 164 | 445 | 42 | 15 | 404 | 465 |
| Initial Q (Qb), veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Work Zone On Approach |  | No |  |  | No |  |  | No |  |  | No |  |
| Adj Sat Flow, veh/h/ln | 1771 | 1771 | 1806 | 1736 | 1736 | 1736 | 1736 | 1736 | 1736 | 1736 | 1736 | 1736 |
| Adj Flow Rate, veh/h | 366 | 314 | 173 | 67 | 385 | 9 | 178 | 484 | 46 | 16 | 439 | 505 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Percent Heavy Veh, \% | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 |
| Cap, veh/h | 401 | 672 | 581 | 381 | 439 | 10 | 227 | 671 | 64 | 45 | 499 | 397 |
| Arrive On Green | 0.17 | 0.38 | 0.38 | 0.05 | 0.26 | 0.26 | 0.09 | 0.43 | 0.43 | 0.10 | 0.10 | 0.10 |
| Sat Flow, veh/h | 1687 | 1771 | 1530 | 1654 | 1690 | 40 | 1654 | 1561 | 148 | 27 | 1683 | 1339 |
| Grp Volume(v), veh/h | 366 | 314 | 173 | 67 | 0 | 394 | 178 | 0 | 530 | 455 | 0 | 505 |
| Grp Sat Flow(s), veh/h/ln | 1687 | 1771 | 1530 | 1654 | 0 | 1729 | 1654 | 0 | 1710 | 1710 | 0 | 1339 |
| Q Serve(g_s), s | 15.2 | 13.4 | 7.9 | 2.9 | 0.0 | 21.8 | 7.1 | 0.0 | 25.6 | 10.1 | 0.0 | 29.6 |
| Cycle Q Clear(g_c), s | 15.2 | 13.4 | 7.9 | 2.9 | 0.0 | 21.8 | 7.1 | 0.0 | 25.6 | 26.2 | 0.0 | 29.6 |
| Prop In Lane | 1.00 |  | 1.00 | 1.00 |  | 0.02 | 1.00 |  | 0.09 | 0.04 |  | 1.00 |
| Lane Grp Cap(c), veh/h | 401 | 672 | 581 | 381 | 0 | 450 | 227 | 0 | 735 | 544 | 0 | 397 |
| V/C Ratio(X) | 0.91 | 0.47 | 0.30 | 0.18 | 0.00 | 0.88 | 0.78 | 0.00 | 0.72 | 0.84 | 0.00 | 1.27 |
| Avail Cap(c_a), veh/h | 401 | 672 | 581 | 396 | 0 | 450 | 320 | 0 | 735 | 544 | 0 | 397 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.33 | 0.33 | 0.33 |
| Upstream Filter(l) | 1.00 | 1.00 | 1.00 | 1.00 | 0.00 | 1.00 | 1.00 | 0.00 | 1.00 | 0.93 | 0.00 | 0.93 |
| Uniform Delay (d), s/veh | 23.0 | 23.4 | 21.7 | 24.8 | 0.0 | 35.5 | 24.5 | 0.0 | 23.5 | 43.5 | 0.0 | 45.1 |
| Incr Delay (d2), s/veh | 24.8 | 0.5 | 0.3 | 0.2 | 0.0 | 20.7 | 8.1 | 0.0 | 6.0 | 13.3 | 0.0 | 139.9 |
| Initial Q Delay(d3),s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| \%ile BackOfQ(95\%),veh/ln | 13.3 | 9.4 | 5.1 | 2.1 | 0.0 | 17.3 | 5.8 | 0.0 | 16.7 | 20.0 | 0.0 | 39.1 |
| Unsig. Movement Delay, s/veh |  |  |  |  |  |  |  |  |  |  |  |  |
| LnGrp Delay(d),s/veh | 47.8 | 23.9 | 22.0 | 25.0 | 0.0 | 56.1 | 32.6 | 0.0 | 29.6 | 56.8 | 0.0 | 185.0 |
| LnGrp LOS | D | C | C | C | A | E | C | A | C | E | A | F |
| Approach Vol, veh/h |  | 853 |  |  | 461 |  |  | 708 |  |  | 960 |  |
| Approach Delay, s/veh |  | 33.8 |  |  | 51.6 |  |  | 30.3 |  |  | 124.2 |  |
| Approach LOS |  | C |  |  | D |  |  | C |  |  | F |  |
| Timer - Assigned Phs | 1 | 2 | 3 | 4 |  | 6 | 7 | 8 |  |  |  |  |
| Phs Duration ( $G+Y+R c$ ), $s$ | 13.4 | 34.6 | 21.0 | 31.0 |  | 48.0 | 9.1 | 42.9 |  |  |  |  |
| Change Period ( $\mathrm{Y}+\mathrm{Rc}$ ), s | 4.0 | 5.0 | 4.0 | 5.0 |  | 5.0 | 4.0 | 5.0 |  |  |  |  |
| Max Green Setting (Gmax), s | 15.0 | 24.0 | 17.0 | 26.0 |  | 43.0 | 6.0 | 37.0 |  |  |  |  |
| Max Q Clear Time ( $\mathrm{g}_{\sim} \mathrm{c}+11$ ), s | 9.1 | 0.0 | 17.2 | 0.0 |  | 0.0 | 4.9 | 0.0 |  |  |  |  |
| Green Ext Time (p_c), s | 0.3 | 0.0 | 0.0 | 0.0 |  | 0.0 | 0.0 | 0.0 |  |  |  |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| HCM 6th Ctrl Delay 64.8 |  |  |  |  |  |  |  |  |  |  |  |  |
| HCM 6th LOS |  |  | E |  |  |  |  |  |  |  |  |  |


|  | 4 |  |  | 7 |  |  | $4$ | $\dagger$ | $p$ | ( | $\frac{1}{\dagger}$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ${ }^{7 \%}$ | 4 | F | ${ }^{1}$ | $\uparrow$ |  | ${ }^{1}$ | $\uparrow$ |  |  | *个 | 7 |
| Traffic Volume (vph) | 272 | 262 | 215 | 41 | 314 | 4 | 240 | 315 | 28 | 2 | 270 | 265 |
| Future Volume (vph) | 272 | 262 | 215 | 41 | 314 | 4 | 240 | 315 | 28 | 2 | 270 | 265 |
| Ideal Flow (vphpl) | 1805 | 1805 | 1750 | 1750 | 1750 | 1750 | 1750 | 1750 | 1750 | 1750 | 1750 | 1750 |
| Lane Width (ft) | 11 | 11 | 16 | 11 | 11 | 11 | 11 | 11 | 11 | 11 | 11 | 11 |
| Grade (\%) |  | 0\% |  |  | 0\% |  |  | 0\% |  |  | 0\% |  |
| Storage Length (ft) | 0 |  | 150 | 0 |  | 0 | 0 |  | 0 | 0 |  | 0 |
| Storage Lanes | 2 |  | 1 | 1 |  | 0 | 1 |  | 0 | 0 |  | 1 |
| Taper Length (ft) | 25 |  |  | 25 |  |  | 25 |  |  | 25 |  |  |
| Right Turn on Red |  |  | Yes |  |  | Yes |  |  | Yes |  |  | Yes |
| Link Speed (mph) |  | 30 |  |  | 25 |  |  | 30 |  |  | 25 |  |
| Link Distance (ft) |  | 542 |  |  | 403 |  |  | 539 |  |  | 1202 |  |
| Travel Time (s) |  | 12.3 |  |  | 11.0 |  |  | 12.3 |  |  | 32.8 |  |
| Confl. Peds. (\#/hr) |  |  |  |  |  |  |  |  |  |  |  |  |
| Confl. Bikes (\#/hr) |  |  |  |  |  |  |  |  |  |  |  |  |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Growth Factor | 100\% | 100\% | 62\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 62\% |
| Heavy Vehicles (\%) | 1\% | 1\% | 1\% | 1\% | 1\% | 1\% | 1\% | 1\% | 1\% | 1\% | 1\% | 1\% |
| Bus Blockages (\#/hr) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Parking (\#/hr) |  |  |  |  |  |  |  |  |  |  |  |  |
| Mid-Block Traffic (\%) |  | 0\% |  |  | 0\% |  |  | 0\% |  |  | 0\% |  |
| Shared Lane Traffic (\%) |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Group Flow (vph) | 296 | 285 | 145 | 45 | 345 | 0 | 261 | 372 | 0 | 0 | 295 | 179 |
| Turn Type | Prot | NA | Perm | pm+pt | NA |  | pm+pt | NA |  | Perm | NA | $\mathrm{pm}+0 \mathrm{~V}$ |
| Protected Phases | 3 | 8 |  | 7 | 4 |  | 1 | 6 |  |  | 2 | 3 |
| Permitted Phases |  |  | 8 | 4 |  |  | 6 |  |  | 2 |  | 2 |
| Detector Phase | 3 | 8 | 8 | 7 | 4 |  | 1 | 6 |  | 2 | 2 | 3 |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial (s) | 8.0 | 19.0 | 19.0 | 6.0 | 19.0 |  | 6.0 | 19.0 |  | 19.0 | 19.0 | 8.0 |
| Minimum Split (s) | 13.5 | 25.0 | 25.0 | 10.0 | 25.0 |  | 10.0 | 25.0 |  | 25.0 | 25.0 | 13.5 |
| Total Split (s) | 20.0 | 44.0 | 44.0 | 10.0 | 34.0 |  | 18.0 | 46.0 |  | 28.0 | 28.0 | 20.0 |
| Total Split (\%) | 20.0\% | 44.0\% | 44.0\% | 10.0\% | 34.0\% |  | 18.0\% | 46.0\% |  | 28.0\% | 28.0\% | 20.0\% |
| Yellow Time (s) | 3.5 | 4.0 | 4.0 | 3.0 | 4.0 |  | 3.0 | 4.0 |  | 4.0 | 4.0 | 3.5 |
| All-Red Time (s) | 2.0 | 1.0 | 1.0 | 1.0 | 1.0 |  | 1.0 | 1.0 |  | 1.0 | 1.0 | 2.0 |
| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  | 0.0 | 0.0 |  |  | 0.0 | 0.0 |
| Total Lost Time (s) | 5.5 | 5.0 | 5.0 | 4.0 | 5.0 |  | 4.0 | 5.0 |  |  | 5.0 | 5.5 |
| Lead/Lag | Lead | Lag | Lag | Lead | Lag |  | Lead |  |  | Lag | Lag | Lead |
| Lead-Lag Optimize? |  |  |  |  |  |  |  |  |  |  |  |  |
| Recall Mode | None | Min | Min | None | Max |  | None | C-Max |  | C-Max | C-Max | None |
| v/c Ratio | 0.73 | 0.38 | 0.18 | 0.11 | 0.67 |  | 0.63 | 0.55 |  |  | 0.40 | 0.26 |
| Control Delay | 52.6 | 22.6 | 4.0 | 14.6 | 38.4 |  | 27.8 | 25.8 |  |  | 36.8 | 14.5 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  | 0.0 | 0.0 |  |  | 0.0 | 0.0 |
| Total Delay | 52.6 | 22.6 | 4.0 | 14.6 | 38.4 |  | 27.8 | 25.8 |  |  | 36.8 | 14.5 |
| Queue Length 50th (ft) | 93 | 130 | 0 | 14 | 193 |  | 113 | 174 |  |  | 92 | 36 |
| Queue Length 95th (ft) | 137 | 203 | 38 | 33 | 299 |  | 179 | 266 |  |  | 142 | 99 |
| Internal Link Dist (ft) |  | 462 |  |  | 323 |  |  | 459 |  |  | 1122 |  |
| Turn Bay Length (ft) |  |  | 150 |  |  |  |  |  |  |  |  |  |
| Base Capacity (vph) | 461 | 742 | 800 | 406 | 514 |  | 426 | 681 |  |  | 729 | 721 |
| Starvation Cap Reductn | 0 | 0 | 0 | 0 | 0 |  | 0 | 0 |  |  | 0 | 0 |

2022 Base Year Background

|  | 4 | $\rightarrow$ | \% | 7 |  | 4 | 4 | $\dagger$ | $p$ | $\pm$ | $\dagger$ | $\checkmark$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Spillback Cap Reductn | 0 | 0 | 0 | 0 | 0 |  | 0 | 0 |  |  | 0 | 0 |
| Storage Cap Reductn | 0 | 0 | 0 | 0 | 0 |  | 0 | 0 |  |  | 0 | 0 |
| Reduced v/c Ratio | 0.64 | 0.38 | 0.18 | 0.11 | 0.67 |  | 0.61 | 0.55 |  |  | 0.40 | 0.25 |

## Intersection Summary

```
Area Type: Other
```

Cycle Length: 100
Actuated Cycle Length: 100
Offset: $0(0 \%)$, Referenced to phase 2:SBTL and 6:NBTL, Start of Green, Master Intersection
Natural Cycle: 75
Control Type: Actuated-Coordinated
Splits and Phases: 30: Commercial St \& Winneconne Ave


|  | 4 | $\rightarrow$ |  | $\checkmark$ |  |  | 4 | 4 | $p$ |  | $\downarrow$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | \% ${ }^{1 / 4}$ | 4 | 「 | ${ }_{1}$ | $\uparrow$ |  | ${ }^{4}$ | $\hat{\beta}$ |  |  | $\uparrow \uparrow$ | F |
| Traffic Volume (veh/h) | 272 | 262 | 215 | 41 | 314 |  | 240 | 315 | 28 | 2 | 270 | 265 |
| Future Volume (veh/h) | 272 | 262 | 215 | 41 | 314 | 4 | 240 | 315 | 28 | 2 | 270 | 265 |
| Initial $\mathrm{Q}(\mathrm{Qb})$, veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Work Zone On Approach |  | No |  |  | No |  |  | No |  |  | No |  |
| Adj Sat Flow, veh/h/ln | 1791 | 1791 | 1806 | 1736 | 1736 | 1736 | 1736 | 1736 | 1736 | 1736 | 1736 | 1736 |
| Adj Flow Rate, veh/h | 296 | 285 | 145 | 45 | 341 | 4 | 261 | 342 | 30 | 2 | 293 | 179 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Percent Heavy Veh, \% | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 |
| Cap, veh/h | 372 | 671 | 573 | 390 | 497 | 6 | 460 | 696 | 61 | 38 | 883 | 567 |
| Arrive On Green | 0.11 | 0.37 | 0.37 | 0.04 | 0.29 | 0.29 | 0.13 | 0.44 | 0.44 | 0.09 | 0.09 | 0.09 |
| Sat Flow, veh/h | 3309 | 1791 | 1530 | 1654 | 1713 | 20 | 1654 | 1573 | 138 | 4 | 3231 | 1471 |
| Grp Volume(v), veh/h | 296 | 285 | 145 | 45 | 0 | 345 | 261 | 0 | 372 | 158 | 137 | 179 |
| Grp Sat Flow(s),veh/h/ln | 1654 | 1791 | 1530 | 1654 | 0 | 1733 | 1654 | 0 | 1712 | 1734 | 1501 | 1471 |
| Q Serve(g_s), s | 8.7 | 11.8 | 6.5 | 1.9 | 0.0 | 17.7 | 10.8 | 0.0 | 15.5 | 0.0 | 8.5 | 9.7 |
| Cycle Q Clear(g_c), s | 8.7 | 11.8 | 6.5 | 1.9 | 0.0 | 17.7 | 10.8 | 0.0 | 15.5 | 8.5 | 8.5 | 9.7 |
| Prop In Lane | 1.00 |  | 1.00 | 1.00 |  | 0.01 | 1.00 |  | 0.08 | 0.01 |  | 1.00 |
| Lane Grp Cap(c), veh/h | 372 | 671 | 573 | 390 | 0 | 502 | 460 | 0 | 758 | 510 | 410 | 567 |
| V/C Ratio(X) | 0.80 | 0.42 | 0.25 | 0.12 | 0.00 | 0.69 | 0.57 | 0.00 | 0.49 | 0.31 | 0.33 | 0.32 |
| Avail Cap(c_a), veh/h | 480 | 698 | 597 | 419 | 0 | 502 | 478 | 0 | 758 | 510 | 410 | 567 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.33 | 0.33 | 0.33 |
| Upstream Filter(l) | 1.00 | 1.00 | 1.00 | 1.00 | 0.00 | 1.00 | 1.00 | 0.00 | 1.00 | 0.93 | 0.93 | 0.93 |
| Uniform Delay (d), s/veh | 43.3 | 23.3 | 21.6 | 22.9 | 0.0 | 31.5 | 20.6 | 0.0 | 19.8 | 37.0 | 37.0 | 27.4 |
| Incr Delay (d2), s/veh | 7.0 | 0.4 | 0.2 | 0.1 | 0.0 | 7.5 | 1.5 | 0.0 | 2.3 | 1.5 | 2.0 | 1.4 |
| Initial Q Delay(d3),s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| \%ile BackOfQ(95\%),veh/ln | 7.0 | 8.7 | 4.2 | 1.3 | 0.0 | 13.1 | 7.6 | 0.0 | 10.6 | 7.3 | 6.5 | 7.1 |
| Unsig. Movement Delay, s/veh |  |  |  |  |  |  |  |  |  |  |  |  |
| LnGrp Delay(d),s/veh | 50.3 | 23.7 | 21.8 | 23.1 | 0.0 | 38.9 | 22.0 | 0.0 | 22.1 | 38.4 | 39.0 | 28.7 |
| LnGrp LOS | D | C | C | C | A | D | C | A | C | D | D | C |
| Approach Vol, veh/h |  | 726 |  |  | 390 |  |  | 633 |  |  | 474 |  |
| Approach Delay, s/veh |  | 34.2 |  |  | 37.1 |  |  | 22.1 |  |  | 34.9 |  |
| Approach LOS |  | C |  |  | D |  |  | C |  |  | C |  |
| Timer - Assigned Phs | 1 | 2 | 3 | 4 |  | 6 | 7 | 8 |  |  |  |  |
| Phs Duration ( $G+Y+R \mathrm{C})$, s | 16.9 | 32.3 | 16.7 | 34.0 |  | 49.3 | 8.3 | 42.5 |  |  |  |  |
| Change Period ( $\mathrm{Y}+\mathrm{Rc}$ ), s | 4.0 | 5.0 | 5.5 | 5.0 |  | 5.0 | 4.0 | 5.0 |  |  |  |  |
| Max Green Setting (Gmax), s | 14.0 | 23.0 | 14.5 | 29.0 |  | 41.0 | 6.0 | 39.0 |  |  |  |  |
| Max Q Clear Time ( $\left.\mathrm{g}_{-} \mathrm{c}+11\right)$, s | 12.8 | 11.7 | 10.7 | 0.0 |  | 0.0 | 3.9 | 0.0 |  |  |  |  |
| Green Ext Time (p_c), s | 0.1 | 0.1 | 0.5 | 0.0 |  | 0.0 | 0.0 | 0.0 |  |  |  |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| HCM 6th Ctrl Delay |  |  | 31.4 |  |  |  |  |  |  |  |  |  |
| HCM 6th LOS |  |  | C |  |  |  |  |  |  |  |  |  |


|  | 4 |  |  | $\checkmark$ |  |  | $4$ | $\dagger$ | $p$ | $\downarrow$ | $\dagger$ | $\pm$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ${ }^{17}$ | 4 | 7 | ${ }^{7}$ | $\uparrow$ |  | ${ }^{*}$ | $\uparrow$ |  |  | * $\uparrow$ ¢ | 「 |
| Traffic Volume (vph) | 289 | 247 | 219 | 53 | 303 | 7 | 141 | 381 | 36 | 12 | 346 | 398 |
| Future Volume (vph) | 289 | 247 | 219 | 53 | 303 | 7 | 141 | 381 | 36 | 12 | 346 | 398 |
| Ideal Flow (vphpl) | 1805 | 1805 | 1750 | 1750 | 1750 | 1750 | 1750 | 1750 | 1750 | 1750 | 1750 | 1750 |
| Lane Width (ft) | 11 | 11 | 16 | 11 | 11 | 11 | 11 | 11 | 11 | 11 | 11 | 11 |
| Grade (\%) |  | 0\% |  |  | 0\% |  |  | 0\% |  |  | 0\% |  |
| Storage Length (ft) | 0 |  | 150 | 0 |  | 0 | 0 |  | 0 | 0 |  | 0 |
| Storage Lanes | 2 |  | 1 | 1 |  | 0 | 1 |  | 0 | 0 |  | 1 |
| Taper Length (ft) | 25 |  |  | 25 |  |  | 25 |  |  | 25 |  |  |
| Right Turn on Red |  |  | Yes |  |  | Yes |  |  | Yes |  |  | Yes |
| Link Speed (mph) |  | 30 |  |  | 25 |  |  | 30 |  |  | 25 |  |
| Link Distance (ft) |  | 542 |  |  | 403 |  |  | 539 |  |  | 1202 |  |
| Travel Time (s) |  | 12.3 |  |  | 11.0 |  |  | 12.3 |  |  | 32.8 |  |
| Confl. Peds. (\#/hr) |  |  |  |  |  |  |  |  |  |  |  |  |
| Confl. Bikes (\#/hr) |  |  |  |  |  |  |  |  |  |  |  |  |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Growth Factor | 100\% | 100\% | 62\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 62\% |
| Heavy Vehicles (\%) | 1\% | 1\% | 1\% | 1\% | 1\% | 1\% | 1\% | 1\% | 1\% | 1\% | 1\% | 1\% |
| Bus Blockages (\#/hr) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Parking (\#/hr) |  |  |  |  |  |  |  |  |  |  |  |  |
| Mid-Block Traffic (\%) |  | 0\% |  |  | 0\% |  |  | 0\% |  |  | 0\% |  |
| Shared Lane Traffic (\%) |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Group Flow (vph) | 314 | 268 | 148 | 58 | 337 | 0 | 153 | 453 | 0 | 0 | 389 | 268 |
| Turn Type | Prot | NA | Perm | pm+pt | NA |  | pm+pt | NA |  | Perm | NA | $\mathrm{pm}+\mathrm{ov}$ |
| Protected Phases | 3 | 8 |  | 7 | 4 |  | 1 | 6 |  |  | 2 | 3 |
| Permitted Phases |  |  | 8 | 4 |  |  | 6 |  |  | 2 |  | 2 |
| Detector Phase | 3 | 8 | 8 | 7 | 4 |  | 1 | 6 |  | 2 | 2 | 3 |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial (s) | 8.0 | 19.0 | 19.0 | 6.0 | 19.0 |  | 6.0 | 19.0 |  | 19.0 | 19.0 | 8.0 |
| Minimum Split (s) | 13.5 | 25.0 | 25.0 | 10.0 | 25.0 |  | 10.0 | 25.0 |  | 25.0 | 25.0 | 13.5 |
| Total Split (s) | 21.0 | 44.0 | 44.0 | 10.0 | 33.0 |  | 11.0 | 46.0 |  | 35.0 | 35.0 | 21.0 |
| Total Split (\%) | 21.0\% | 44.0\% | 44.0\% | 10.0\% | 33.0\% |  | 11.0\% | 46.0\% |  | 35.0\% | 35.0\% | 21.0\% |
| Yellow Time (s) | 3.5 | 4.0 | 4.0 | 3.0 | 4.0 |  | 3.0 | 4.0 |  | 4.0 | 4.0 | 3.5 |
| All-Red Time (s) | 2.0 | 1.0 | 1.0 | 1.0 | 1.0 |  | 1.0 | 1.0 |  | 1.0 | 1.0 | 2.0 |
| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  | 0.0 | 0.0 |  |  | 0.0 | 0.0 |
| Total Lost Time (s) | 5.5 | 5.0 | 5.0 | 4.0 | 5.0 |  | 4.0 | 5.0 |  |  | 5.0 | 5.5 |
| Lead/Lag | Lead | Lag | Lag | Lead | Lag |  | Lead |  |  | Lag | Lag | Lead |
| Lead-Lag Optimize? |  |  |  |  |  |  |  |  |  |  |  |  |
| Recall Mode | None | Min | Min | None | Max |  | None | C-Max |  | C-Max | C-Max | None |
| v/c Ratio | 0.73 | 0.38 | 0.19 | 0.14 | 0.67 |  | 0.45 | 0.67 |  |  | 0.43 | 0.32 |
| Control Delay | 51.9 | 23.4 | 4.1 | 15.1 | 39.1 |  | 23.5 | 29.4 |  |  | 35.5 | 14.0 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  | 0.0 | 0.0 |  |  | 0.0 | 0.0 |
| Total Delay | 51.9 | 23.4 | 4.1 | 15.1 | 39.1 |  | 23.5 | 29.4 |  |  | 35.5 | 14.0 |
| Queue Length 50th (ft) | 99 | 121 | 0 | 18 | 189 |  | 61 | 226 |  |  | 123 | 55 |
| Queue Length 95th (ft) | 143 | 191 | 38 | 40 | 296 |  | 106 | 340 |  |  | 179 | 143 |
| Internal Link Dist (ft) |  | 462 |  |  | 323 |  |  | 459 |  |  | 1122 |  |
| Turn Bay Length (ft) |  |  | 150 |  |  |  |  |  |  |  |  |  |
| Base Capacity (vph) | 493 | 708 | 771 | 403 | 501 |  | 343 | 681 |  |  | 896 | 852 |
| Starvation Cap Reductn | 0 | 0 | 0 | 0 | 0 |  | 0 | 0 |  |  | 0 | 0 |

2022 Base Year Background

|  | 4 | - | 7 | 7 | $\leftarrow$ | 4 | + | $\dagger$ | 7 | - | $\frac{1}{7}$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Spillback Cap Reductn | 0 | 0 | 0 | 0 | 0 |  | 0 | 0 |  |  | 0 | 0 |
| Storage Cap Reductn | 0 | 0 | 0 | 0 | 0 |  | 0 | 0 |  |  | 0 | 0 |
| Reduced v/c Ratio | 0.64 | 0.38 | 0.19 | 0.14 | 0.67 |  | 0.45 | 0.67 |  |  | 0.43 | 0.31 |

## Intersection Summary

```
Area Type: Other
```

Cycle Length: 100
Actuated Cycle Length: 100
Offset: 0 ( $0 \%$ ), Referenced to phase 2:SBTL and 6:NBTL, Start of Green, Master Intersection
Natural Cycle: 75
Control Type: Actuated-Coordinated
Splits and Phases: $\quad 30$ : Commercial St \& Winneconne Ave


|  | 4 | $\rightarrow$ | \％ | 7 |  |  | 4 | $\dagger$ | $p$ |  | $\dagger$ | 4 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ${ }^{1 *}$ | 4 | 「 | ${ }^{7}$ | $\uparrow$ |  | ${ }^{1}$ | 个 |  |  | ＋4 | 「 |
| Traffic Volume（veh／h） | 289 | 247 | 219 | 53 | 303 | 7 | 141 | 381 | 36 | 12 | 346 | 398 |
| Future Volume（veh／h） | 289 | 247 | 219 | 53 | 303 | 7 | 141 | 381 | 36 | 12 | 346 | 398 |
| Initial Q（Qb），veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped－Bike Adj（A＿pbT） | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 |
| Parking Bus，Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Work Zone On Approach |  | No |  |  | No |  |  | No |  |  | No |  |
| Adj Sat Flow，veh／h／ln | 1791 | 1791 | 1806 | 1736 | 1736 | 1736 | 1736 | 1736 | 1736 | 1736 | 1736 | 1736 |
| Adj Flow Rate，veh／h | 314 | 268 | 148 | 58 | 329 | 8 | 153 | 414 | 39 | 13 | 376 | 268 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Percent Heavy Veh，\％ | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 |
| Cap，veh／h | 392 | 655 | 559 | 400 | 473 | 11 | 365 | 698 | 66 | 53 | 1063 | 670 |
| Arrive On Green | 0.12 | 0.37 | 0.37 | 0.05 | 0.28 | 0.28 | 0.07 | 0.45 | 0.45 | 0.11 | 0.11 | 0.11 |
| Sat Flow，veh／h | 3309 | 1791 | 1530 | 1654 | 1688 | 41 | 1654 | 1563 | 147 | 42 | 3159 | 1471 |
| Grp Volume（v），veh／h | 314 | 268 | 148 | 58 | 0 | 337 | 153 | 0 | 453 | 207 | 182 | 268 |
| Grp Sat Flow（s），veh／h／ln | 1654 | 1791 | 1530 | 1654 | 0 | 1729 | 1654 | 0 | 1710 | 1701 | 1501 | 1471 |
| Q Serve（g＿s），s | 9.2 | 11.2 | 6.8 | 2.4 | 0.0 | 17.4 | 5.8 | 0.0 | 20.0 | 0.0 | 11.2 | 14.1 |
| Cycle Q Clear（g＿c），s | 9.2 | 11.2 | 6.8 | 2.4 | 0.0 | 17.4 | 5.8 | 0.0 | 20.0 | 11.0 | 11.2 | 14.1 |
| Prop In Lane | 1.00 |  | 1.00 | 1.00 |  | 0.02 | 1.00 |  | 0.09 | 0.06 |  | 1.00 |
| Lane Grp Cap（c），veh／h | 392 | 655 | 559 | 400 | 0 | 484 | 365 | 0 | 763 | 610 | 505 | 670 |
| V／C Ratio（X） | 0.80 | 0.41 | 0.26 | 0.15 | 0.00 | 0.70 | 0.42 | 0.00 | 0.59 | 0.34 | 0.36 | 0.40 |
| Avail Cap（c＿a），veh／h | 513 | 698 | 597 | 420 | 0 | 484 | 365 | 0 | 763 | 610 | 505 | 670 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.33 | 0.33 | 0.33 |
| Upstream Filter（I） | 1.00 | 1.00 | 1.00 | 1.00 | 0.00 | 1.00 | 1.00 | 0.00 | 1.00 | 0.93 | 0.93 | 0.93 |
| Uniform Delay（d），s／veh | 42.9 | 23.7 | 22.3 | 23.4 | 0.0 | 32.2 | 19.2 | 0.0 | 20.8 | 34.4 | 34.5 | 25.1 |
| Incr Delay（d2），s／veh | 6.7 | 0.4 | 0.2 | 0.2 | 0.0 | 8.0 | 0.8 | 0.0 | 3.4 | 1.4 | 1.9 | 1.7 |
| Initial Q Delay（d3），s／veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| \％ile BackOfQ（95\％），veh／In | 7.4 | 8.3 | 4.4 | 1.8 | 0.0 | 13.1 | 4.1 | 0.0 | 13.2 | 9.0 | 8.2 | 9.6 |
| Unsig．Movement Delay，s／veh |  |  |  |  |  |  |  |  |  |  |  |  |
| LnGrp Delay（d），s／veh | 49.6 | 24.1 | 22.5 | 23.6 | 0.0 | 40.2 | 20.0 | 0.0 | 24.2 | 35.8 | 36.3 | 26.7 |
| LnGrp LOS | D | C | C | C | A | D | B | A | C | D | D | C |
| Approach Vol，veh／h |  | 730 |  |  | 395 |  |  | 606 |  |  | 657 |  |
| Approach Delay，s／veh |  | 34.8 |  |  | 37.8 |  |  | 23.2 |  |  | 32.2 |  |
| Approach LOS |  | C |  |  | D |  |  | C |  |  | C |  |
| Timer－Assigned Phs | 1 | 2 | 3 | 4 |  | 6 | 7 | 8 |  |  |  |  |
| Phs Duration（ $G+Y+R \mathrm{c}$ ），$s$ | 11.0 | 38.6 | 17.4 | 33.0 |  | 49.6 | 8.8 | 41.6 |  |  |  |  |
| Change Period（ $\mathrm{Y}+\mathrm{Rc}$ ），s | 4.0 | 5.0 | 5.5 | 5.0 |  | 5.0 | 4.0 | 5.0 |  |  |  |  |
| Max Green Setting（Gmax），s | 7.0 | 30.0 | 15.5 | 28.0 |  | 41.0 | 6.0 | 39.0 |  |  |  |  |
| Max Q Clear Time（g＿c＋l1），s | 7.8 | 16.1 | 11.2 | 0.0 |  | 0.0 | 4.4 | 0.0 |  |  |  |  |
| Green Ext Time（p＿c），s | 0.0 | 0.2 | 0.6 | 0.0 |  | 0.0 | 0.0 | 0.0 |  |  |  |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| HCM 6th Ctrl Delay |  |  | 31.6 |  |  |  |  |  |  |  |  |  |
| HCM 6th LOS |  |  | C |  |  |  |  |  |  |  |  |  |


|  | 4 |  |  | $\checkmark$ |  |  | $4$ | $\dagger$ | $p$ | $V$ | $\dagger$ | $\pm$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ${ }^{7 \%}$ | 4 | F | ${ }^{*}$ | $\uparrow$ |  | ${ }^{7}$ | $\uparrow$ |  |  | * $\uparrow$ ¢ | 「 |
| Traffic Volume (vph) | 318 | 306 | 251 | 48 | 366 | 5 | 280 | 367 | 33 | 2 | 315 | 309 |
| Future Volume (vph) | 318 | 306 | 251 | 48 | 366 | 5 | 280 | 367 | 33 | 2 | 315 | 309 |
| Ideal Flow (vphpl) | 1805 | 1805 | 1750 | 1750 | 1750 | 1750 | 1750 | 1750 | 1750 | 1750 | 1750 | 1750 |
| Lane Width (ft) | 11 | 11 | 16 | 11 | 11 | 11 | 11 | 11 | 11 | 11 | 11 | 11 |
| Grade (\%) |  | 0\% |  |  | 0\% |  |  | 0\% |  |  | 0\% |  |
| Storage Length (ft) | 0 |  | 150 | 0 |  | 0 | 0 |  | 0 | 0 |  | 0 |
| Storage Lanes | 2 |  | 1 | 1 |  | 0 | 1 |  | 0 | 0 |  | 1 |
| Taper Length (ft) | 25 |  |  | 25 |  |  | 25 |  |  | 25 |  |  |
| Right Turn on Red |  |  | Yes |  |  | Yes |  |  | Yes |  |  | Yes |
| Link Speed (mph) |  | 30 |  |  | 25 |  |  | 30 |  |  | 25 |  |
| Link Distance (ft) |  | 542 |  |  | 403 |  |  | 539 |  |  | 1202 |  |
| Travel Time (s) |  | 12.3 |  |  | 11.0 |  |  | 12.3 |  |  | 32.8 |  |
| Confl. Peds. (\#/hr) |  |  |  |  |  |  |  |  |  |  |  |  |
| Confl. Bikes (\#/hr) |  |  |  |  |  |  |  |  |  |  |  |  |
| Peak Hour Factor | 0.83 | 0.83 | 0.83 | 0.83 | 0.83 | 0.83 | 0.83 | 0.83 | 0.83 | 0.83 | 0.83 | 0.83 |
| Growth Factor | 100\% | 100\% | 62\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% |
| Heavy Vehicles (\%) | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% | 3\% | 3\% | 3\% | 4\% | 4\% | 4\% |
| Bus Blockages (\#/hr) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Parking (\#/hr) |  |  |  |  |  |  |  |  |  |  |  |  |
| Mid-Block Traffic (\%) |  | 0\% |  |  | 0\% |  |  | 0\% |  |  | 0\% |  |
| Shared Lane Traffic (\%) |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Group Flow (vph) | 383 | 369 | 187 | 58 | 447 | 0 | 337 | 482 | 0 | 0 | 382 | 372 |
| Turn Type | Prot | NA | Perm | pm+pt | NA |  | pm+pt | NA |  | Perm | NA | $\mathrm{pm}+\mathrm{ov}$ |
| Protected Phases | 3 | 8 |  | 7 | 4 |  | 1 | 6 |  |  | 2 | 3 |
| Permitted Phases |  |  | 8 | 4 |  |  | 6 |  |  | 2 |  | 2 |
| Detector Phase | 3 | 8 | 8 | 7 | 4 |  | 1 | 6 |  | 2 | 2 | 3 |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial (s) | 8.0 | 19.0 | 19.0 | 6.0 | 19.0 |  | 6.0 | 19.0 |  | 19.0 | 19.0 | 8.0 |
| Minimum Split (s) | 13.5 | 25.0 | 25.0 | 10.0 | 25.0 |  | 10.0 | 25.0 |  | 25.0 | 25.0 | 13.5 |
| Total Split (s) | 21.0 | 44.0 | 44.0 | 12.0 | 35.0 |  | 17.0 | 44.0 |  | 27.0 | 27.0 | 21.0 |
| Total Split (\%) | 21.0\% | 44.0\% | 44.0\% | 12.0\% | 35.0\% |  | 17.0\% | 44.0\% |  | 27.0\% | 27.0\% | 21.0\% |
| Yellow Time (s) | 3.5 | 4.0 | 4.0 | 3.0 | 4.0 |  | 3.0 | 4.0 |  | 4.0 | 4.0 | 3.5 |
| All-Red Time (s) | 2.0 | 1.0 | 1.0 | 1.0 | 1.0 |  | 1.0 | 1.0 |  | 1.0 | 1.0 | 2.0 |
| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  | 0.0 | 0.0 |  |  | 0.0 | 0.0 |
| Total Lost Time (s) | 5.5 | 5.0 | 5.0 | 4.0 | 5.0 |  | 4.0 | 5.0 |  |  | 5.0 | 5.5 |
| Lead/Lag | Lead | Lag | Lag | Lead | Lag |  | Lead |  |  | Lag | Lag | Lead |
| Lead-Lag Optimize? |  |  |  |  |  |  |  |  |  |  |  |  |
| Recall Mode | None | Min | Min | None | Max |  | None | C-Max |  | C-Max | C-Max | None |
| v/c Ratio | 0.83 | 0.51 | 0.23 | 0.15 | 0.87 |  | 0.95 | 0.76 |  |  | 0.59 | 0.56 |
| Control Delay | 57.6 | 25.5 | 3.8 | 14.0 | 52.9 |  | 64.9 | 35.3 |  |  | 41.4 | 29.0 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  | 0.0 | 0.0 |  |  | 0.0 | 0.0 |
| Total Delay | 57.6 | 25.5 | 3.8 | 14.0 | 52.9 |  | 64.9 | 35.3 |  |  | 41.4 | 29.0 |
| Queue Length 50th (ft) | 122 | 176 | 0 | 18 | 272 |  | 161 | 259 |  |  | 131 | 168 |
| Queue Length 95th (ft) | 158 | 243 | 32 | 35 | \#395 |  | \#289 | 342 |  |  | 166 | 236 |
| Internal Link Dist (ft) |  | 462 |  |  | 323 |  |  | 459 |  |  | 1122 |  |
| Turn Bay Length (ft) |  |  | 150 |  |  |  |  |  |  |  |  |  |
| Base Capacity (vph) | 488 | 721 | 805 | 412 | 511 |  | 353 | 636 |  |  | 647 | 678 |
| Starvation Cap Reductn | 0 | 0 | 0 | 0 | 0 |  | 0 | 0 |  |  | 0 | 0 |

2042 Horizon Year Background


Splits and Phases: 30: Commercial St \& Winneconne Ave


|  | 4 | $\rightarrow$ |  | 7 |  |  | 4 | 4 | $p$ |  | $\downarrow$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ${ }^{7 *}$ | 4 | $\overline{7}$ | ${ }^{4}$ | $\uparrow$ |  | ${ }^{1}$ | $\hat{+}$ |  |  | $\uparrow_{\text {¢ }}$ ¢ | 「 |
| Traffic Volume (veh/h) | 318 | 306 | 251 | 48 | 366 | 5 | 280 | 367 | 33 | 2 | 315 | 309 |
| Future Volume (veh/h) | 318 | 306 | 251 | 48 | 366 | 5 | 280 | 367 | 33 | 2 | 315 | 309 |
| Initial $\mathrm{Q}(\mathrm{Qb})$, veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Work Zone On Approach |  | No |  |  | No |  |  | No |  |  | No |  |
| Adj Sat Flow, veh/h/ln | 1777 | 1777 | 1792 | 1723 | 1723 | 1723 | 1709 | 1709 | 1709 | 1695 | 1695 | 1695 |
| Adj Flow Rate, veh/h | 383 | 369 | 187 | 58 | 441 | 6 | 337 | 442 | 40 | 2 | 380 | 372 |
| Peak Hour Factor | 0.83 | 0.83 | 0.83 | 0.83 | 0.83 | 0.83 | 0.83 | 0.83 | 0.83 | 0.83 | 0.83 | 0.83 |
| Percent Heavy Veh, \% | 2 | 2 | 2 | 2 | 2 | 2 | 3 | 3 | 3 | 4 | 4 | 4 |
| Cap, veh/h | 454 | 720 | 615 | 363 | 509 | 7 | 369 | 628 | 57 | 37 | 747 | 539 |
| Arrive On Green | 0.14 | 0.41 | 0.41 | 0.05 | 0.30 | 0.30 | 0.13 | 0.41 | 0.41 | 0.08 | 0.08 | 0.08 |
| Sat Flow, veh/h | 3283 | 1777 | 1518 | 1641 | 1695 | 23 | 1628 | 1544 | 140 | 3 | 3155 | 1437 |
| Grp Volume(v), veh/h | 383 | 369 | 187 | 58 | 0 | 447 | 337 | 0 | 482 | 205 | 177 | 372 |
| Grp Sat Flow(s),veh/h/ln | 1641 | 1777 | 1518 | 1641 | 0 | 1719 | 1628 | 0 | 1684 | 1693 | 1466 | 1437 |
| Q Serve(g_s), s | 11.4 | 15.6 | 8.4 | 2.4 | 0.0 | 24.6 | 13.0 | 0.0 | 23.8 | 0.0 | 11.6 | 21.4 |
| Cycle Q Clear(g_c), s | 11.4 | 15.6 | 8.4 | 2.4 | 0.0 | 24.6 | 13.0 | 0.0 | 23.8 | 11.6 | 11.6 | 21.4 |
| Prop In Lane | 1.00 |  | 1.00 | 1.00 |  | 0.01 | 1.00 |  | 0.08 | 0.01 |  | 1.00 |
| Lane Grp Cap(c), veh/h | 454 | 720 | 615 | 363 | 0 | 516 | 369 | 0 | 685 | 437 | 347 | 539 |
| V/C Ratio(X) | 0.84 | 0.51 | 0.30 | 0.16 | 0.00 | 0.87 | 0.91 | 0.00 | 0.70 | 0.47 | 0.51 | 0.69 |
| Avail Cap(c_a), veh/h | 509 | 720 | 615 | 416 | 0 | 516 | 369 | 0 | 685 | 437 | 347 | 539 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.33 | 0.33 | 0.33 |
| Upstream Filter(l) | 1.00 | 1.00 | 1.00 | 1.00 | 0.00 | 1.00 | 1.00 | 0.00 | 1.00 | 0.96 | 0.96 | 0.96 |
| Uniform Delay (d), s/veh | 42.0 | 22.3 | 20.2 | 22.2 | 0.0 | 33.1 | 28.3 | 0.0 | 24.6 | 40.5 | 40.5 | 31.7 |
| Incr Delay (d2), s/veh | 11.3 | 0.6 | 0.3 | 0.2 | 0.0 | 17.6 | 26.6 | 0.0 | 6.0 | 3.4 | 5.1 | 6.8 |
| Initial Q Delay(d3),s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| \%ile BackOfQ(95\%),veh/ln | 9.0 | 10.6 | 5.3 | 1.7 | 0.0 | 18.5 | 9.0 | 0.0 | 15.6 | 9.5 | 8.7 | 14.0 |
| Unsig. Movement Delay, s/veh |  |  |  |  |  |  |  |  |  |  |  |  |
| LnGrp Delay(d),s/veh | 53.4 | 22.9 | 20.5 | 22.4 | 0.0 | 50.7 | 54.9 | 0.0 | 30.6 | 44.0 | 45.6 | 38.5 |
| LnGrp LOS | D | C | C | C | A | D | D | A | C | D | D | D |
| Approach Vol, veh/h |  | 939 |  |  | 505 |  |  | 819 |  |  | 754 |  |
| Approach Delay, s/veh |  | 34.9 |  |  | 47.4 |  |  | 40.6 |  |  | 41.6 |  |
| Approach LOS |  | C |  |  | D |  |  | D |  |  | D |  |
| Timer - Assigned Phs | 1 | 2 | 3 | 4 |  | 6 | 7 | 8 |  |  |  |  |
| Phs Duration ( $G+Y+R \mathrm{C})$, s | 17.0 | 28.7 | 19.3 | 35.0 |  | 45.7 | 8.8 | 45.5 |  |  |  |  |
| Change Period ( $\mathrm{Y}+\mathrm{Rc}$ ), s | 4.0 | 5.0 | 5.5 | 5.0 |  | 5.0 | 4.0 | 5.0 |  |  |  |  |
| Max Green Setting (Gmax), s | 13.0 | 22.0 | 15.5 | 30.0 |  | 39.0 | 8.0 | 39.0 |  |  |  |  |
| Max Q Clear Time ( $\left.\mathrm{g}_{-} \mathrm{c}+11\right)$, s | 15.0 | 23.4 | 13.4 | 0.0 |  | 0.0 | 4.4 | 0.0 |  |  |  |  |
| Green Ext Time (p_c), s | 0.0 | 0.0 | 0.4 | 0.0 |  | 0.0 | 0.0 | 0.0 |  |  |  |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| HCM 6th Ctrl DelayHCM 6th LOS |  |  | 40.2 |  |  |  |  |  |  |  |  |  |
|  |  |  | D |  |  |  |  |  |  |  |  |  |


|  | 4 | $\rightarrow$ | $\checkmark$ | $\checkmark$ |  | 4 | 4 | $\dagger$ | $p$ | $1$ |  | 4 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ** | 4 | 7 | ${ }^{7}$ | 个 |  | ${ }^{1}$ | 个 |  |  | ¢4 | 7 |
| Traffic Volume (vph) | 337 | 289 | 256 | 62 | 354 | 8 | 164 | 445 | 42 | 15 | 404 | 465 |
| Future Volume (vph) | 337 | 289 | 256 | 62 | 354 | 8 | 164 | 445 | 42 | 15 | 404 | 465 |
| Ideal Flow (vphpl) | 1805 | 1805 | 1750 | 1750 | 1750 | 1750 | 1750 | 1750 | 1750 | 1750 | 1750 | 1750 |
| Lane Width (ft) | 11 | 11 | 16 | 11 | 11 | 11 | 11 | 11 | 11 | 11 | 11 | 11 |
| Grade (\%) |  | 0\% |  |  | 0\% |  |  | 0\% |  |  | 0\% |  |
| Storage Length (ft) | 0 |  | 150 | 0 |  | 0 | 0 |  | 0 | 0 |  | 0 |
| Storage Lanes | 2 |  | 1 | 1 |  | 0 | 1 |  | 0 | 0 |  | 1 |
| Taper Length (ft) | 25 |  |  | 25 |  |  | 25 |  |  | 25 |  |  |
| Right Turn on Red |  |  | Yes |  |  | Yes |  |  | Yes |  |  | Yes |
| Link Speed (mph) |  | 30 |  |  | 25 |  |  | 30 |  |  | 25 |  |
| Link Distance (ft) |  | 542 |  |  | 403 |  |  | 539 |  |  | 1202 |  |
| Travel Time (s) |  | 12.3 |  |  | 11.0 |  |  | 12.3 |  |  | 32.8 |  |
| Confl. Peds. (\#/hr) |  |  |  |  |  |  |  |  |  |  |  |  |
| Confl. Bikes (\#/hr) |  |  |  |  |  |  |  |  |  |  |  |  |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Growth Factor | 100\% | 100\% | 62\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 100\% | 62\% |
| Heavy Vehicles (\%) | 1\% | 1\% | 1\% | 1\% | 1\% | 1\% | 1\% | 1\% | 1\% | 1\% | 1\% | 1\% |
| Bus Blockages (\#/hr) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Parking (\#/hr) |  |  |  |  |  |  |  |  |  |  |  |  |
| Mid-Block Traffic (\%) |  | 0\% |  |  | 0\% |  |  | 0\% |  |  | 0\% |  |
| Shared Lane Traffic (\%) |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Group Flow (vph) | 366 | 314 | 173 | 67 | 394 | 0 | 178 | 530 | 0 | 0 | 455 | 313 |
| Turn Type | Prot | NA | Perm | pm+pt | NA |  | pm+pt | NA |  | Perm | NA | pm+ov |
| Protected Phases | 3 | 8 |  | 7 | 4 |  | 1 | 6 |  |  | 2 | 3 |
| Permitted Phases |  |  | 8 | 4 |  |  | 6 |  |  | 2 |  | 2 |
| Detector Phase | 3 | 8 | 8 | 7 | 4 |  | 1 | 6 |  | 2 | 2 | 3 |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial (s) | 8.0 | 19.0 | 19.0 | 6.0 | 19.0 |  | 6.0 | 19.0 |  | 19.0 | 19.0 | 8.0 |
| Minimum Split (s) | 13.5 | 25.0 | 25.0 | 10.0 | 25.0 |  | 10.0 | 25.0 |  | 25.0 | 25.0 | 13.5 |
| Total Split (s) | 21.0 | 44.0 | 44.0 | 10.0 | 33.0 |  | 13.0 | 46.0 |  | 33.0 | 33.0 | 21.0 |
| Total Split (\%) | 21.0\% | 44.0\% | 44.0\% | 10.0\% | 33.0\% |  | 13.0\% | 46.0\% |  | 33.0\% | 33.0\% | 21.0\% |
| Yellow Time (s) | 3.5 | 4.0 | 4.0 | 3.0 | 4.0 |  | 3.0 | 4.0 |  | 4.0 | 4.0 | 3.5 |
| All-Red Time (s) | 2.0 | 1.0 | 1.0 | 1.0 | 1.0 |  | 1.0 | 1.0 |  | 1.0 | 1.0 | 2.0 |
| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  | 0.0 | 0.0 |  |  | 0.0 | 0.0 |
| Total Lost Time (s) | 5.5 | 5.0 | 5.0 | 4.0 | 5.0 |  | 4.0 | 5.0 |  |  | 5.0 | 5.5 |
| Lead/Lag | Lead | Lag | Lag | Lead | Lag |  | Lead |  |  | Lag | Lag | Lead |
| Lead-Lag Optimize? |  |  |  |  |  |  |  |  |  |  |  |  |
| Recall Mode | None | Min | Min | None | Max |  | None | C-Max |  | C-Max | C-Max | None |
| v/c Ratio | 0.80 | 0.44 | 0.22 | 0.17 | 0.81 |  | 0.55 | 0.78 |  |  | 0.54 | 0.39 |
| Control Delay | 55.3 | 24.6 | 3.9 | 15.5 | 48.0 |  | 26.3 | 34.8 |  |  | 39.2 | 19.2 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  | 0.0 | 0.0 |  |  | 0.0 | 0.0 |
| Total Delay | 55.3 | 24.6 | 3.9 | 15.5 | 48.0 |  | 26.3 | 34.8 |  |  | 39.2 | 19.2 |
| Queue Length 50th (ft) | 115 | 147 | 0 | 21 | 236 |  | 72 | 284 |  |  | 156 | 87 |
| Queue Length 95th (ft) | \#169 | 226 | 41 | 44 | \#397 |  | 122 | 422 |  |  | 208 | 197 |
| Internal Link Dist (ft) |  | 462 |  |  | 323 |  |  | 459 |  |  | 1122 |  |
| Turn Bay Length (ft) |  |  | 150 |  |  |  |  |  |  |  |  |  |
| Base Capacity (vph) | 493 | 708 | 786 | 383 | 487 |  | 327 | 681 |  |  | 837 | 809 |
| Starvation Cap Reductn | 0 | 0 | 0 | 0 | 0 |  | 0 | 0 |  |  | 0 | 0 |

2042 Horizon Year Background
Synchro 11 Report
MSA-EF 11/21/2022

|  | 4 | $\rightarrow$ | $\checkmark$ | $\%$ |  | 4 | 4 | $\dagger$ | $p$ | - | $\frac{1}{1}$ | 4 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Spillback Cap Reductn | 0 | 0 | 0 | 0 | 0 |  | 0 | 0 |  |  | 0 | 0 |
| Storage Cap Reductn | 0 | 0 | 0 | 0 | 0 |  | 0 | 0 |  |  | 0 | 0 |
| Reduced v/c Ratio | 0.74 | 0.44 | 0.22 | 0.17 | 0.81 |  | 0.54 | 0.78 |  |  | 0.54 | 0.39 |

```
Intersection Summary
```

```
Area Type: Other
```

```
Area Type: Other
```

Cycle Length: 100
Actuated Cycle Length: 100
Offset: $0(0 \%)$, Referenced to phase 2:SBTL and 6:NBTL, Start of Green, Master Intersection
Natural Cycle: 80
Control Type: Actuated-Coordinated
\# 95th percentile volume exceeds capacity, queue may be longer.
Queue shown is maximum after two cycles.

Splits and Phases: 30: Commercial St \& Winneconne Ave


|  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |

## SITE LAYOUT

$\forall$ Site: 1 [Commercial \& Winneconne 4-leg 2022 AM Peak (Site
Folder: 4-leg Alternative)]
Site Category: (None)
Roundabout

Layout pictures are schematic functional drawings reflecting input data. They are not design drawings.


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## INPUT VOLUMES

Vehicles and pedestrians per 60 minutes
© Site: 1 [Commercial \& Winneconne 4-leg 2022 AM Peak (Site
Folder: 4-leg Alternative)]

Site Category: (None)
Roundabout

Volume Display Method: Total and \%

|  | R2 | T1 | L2 |
| :--- | ---: | ---: | ---: |
| Tot | 265 | 270 | 2 |
| LV | $96 \%$ | $96 \%$ | $98 \%$ |
| HV | $4 \%$ | $4 \%$ | $4 \%$ |



|  | All MCs | Light Vehicles (LV) | Heavy Vehicles (HV) |
| :--- | :---: | :---: | :---: |
| S: NB Commercial | 583 | 566 | 17 |
| E: WB Winneconne | 359 | 355 | 4 |
| N: SB Commercial | 537 | 516 | 21 |
| W: EB Winneconne | 749 | 734 | 15 |
| Total | 2228 | 2170 | 58 |

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Organisation: MSA PROFESSIONAL SERVICES | Licence: PLUS / 1PC | Created: Wednesday, November 23, 2022 10:49:37 AM
Project: <br>msa-ps.com\fs\Projectl07\07578\07578063\Traffic\SIDRA\Commercial-Winneconne RAB Analysis.sip9

## LANE SUMMARY

## $\nabla$ Site: 1 [Commercial \& Winneconne 4-leg 2022 AM Peak (Site Folder: 4-leg Alternative)]

Site Category: (None)
Roundabout

| Lane Use and Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | $\begin{aligned} & \text { ND } \\ & \text { NS } \\ & \text { HV ] } \\ & \% \end{aligned}$ | Cap. <br> veh/h | Deg. Satn v/c | Lane Util. \% | Aver. Delay sec | Level of Service | 95\% <br> [ Veh | $\begin{aligned} & \mathrm{K} \text { OF } \\ & \mathrm{JE} \\ & \text { Dist ] } \\ & \mathrm{ft} \end{aligned}$ | Lane Config | Lane Length ft | Cap. Adj. \% | Prob. Block. \% |
| South: NB Commercial |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane 1 | 341 | 3.0 | 735 | 0.465 | 100 | 11.4 | LOS B | 2.7 | 68.9 | Full | 1600 | 0.0 | 0.0 |
| Lane $2^{\text {d }}$ | 361 | 3.0 | 777 | 0.465 | 100 | 10.9 | LOS B | 2.6 | 66.5 | Full | 1600 | 0.0 | 0.0 |
| Approach | 702 | 3.0 |  | 0.465 |  | 11.2 | LOS B | 2.7 | 68.9 |  |  |  |  |
| East: WB Winneconne |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane 1 | 207 | 1.0 | 537 | 0.386 | 100 | 12.8 | LOS B | 1.7 | 43.7 | Full | 1600 | 0.0 | 0.0 |
| Lane $2^{\text {d }}$ | 226 | 1.0 | 585 | 0.386 | 100 | 11.9 | LOS B | 1.7 | 42.3 | Full | 1600 | 0.0 | 0.0 |
| Approach | 433 | 1.0 |  | 0.386 |  | 12.3 | LOS B | 1.7 | 43.7 |  |  |  |  |
| North: SB Commercial |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane 1 | 314 | 4.0 | 682 | 0.460 | 100 | 12.0 | LOS B | 2.5 | 65.3 | Full | 1600 | 0.0 | 0.0 |
| Lane $2^{\text {d }}$ | 333 | 4.0 | 725 | 0.460 | 100 | 11.4 | LOS B | 2.4 | 63.1 | Full | 1600 | 0.0 | 0.0 |
| Approach | 647 | 4.0 |  | 0.460 |  | 11.7 | LOS B | 2.5 | 65.3 |  |  |  |  |
| West: EB Winneconne |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane 1 | 444 | 2.0 | 949 | 0.468 | 100 | 9.4 | LOS A | 2.9 | 73.2 | Full | 1600 | 0.0 | 0.0 |
| Lane $2^{\text {d }}$ | 459 | 2.0 | 981 | 0.468 | 100 | 9.2 | LOS A | 2.7 | 69.4 | Full | 1600 | 0.0 | 0.0 |
| Approach | 902 | 2.0 |  | 0.468 |  | 9.3 | LOS A | 2.9 | 73.2 |  |  |  |  |
| Intersection | 2684 | 2.6 |  | 0.468 |  | 10.9 | LOS B | 2.9 | 73.2 |  |  |  |  |

Site Level of Service (LOS) Method: Delay \& v/c (HCM 6). Site LOS Method is specified in the Parameter Settings dialog (Site tab).
Roundabout LOS Method: Same as Sign Control.
Lane LOS values are based on average delay and v/c ratio (degree of saturation) per lane.
LOS F will result if v/c > 1 irrespective of lane delay value (does not apply for approaches and intersection).
Intersection and Approach LOS values are based on average delay for all lanes ( $\mathrm{v} / \mathrm{c}$ not used as specified in HCM 6).
Roundabout Capacity Model: US HCM 6.
Delay Model: HCM Delay Formula (Geometric Delay is not included).
Queue Model: HCM Queue Formula.
Gap-Acceptance Capacity: Traditional M1.
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.
d Dominant lane on roundabout approach

| Approach Lane Flows (veh/h) |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| South: NB Commercial |  |  |  |  |  |  |  |  |  |  |
| Mov. <br> From S To Exit: | L2 W | T1 N | R2 E | Total | \%HV | Cap. veh/h | Deg. Satn v/c | Lane Util. \% | Prob. SL Ov. \% | $\begin{gathered} \text { Ov. } \\ \text { Lane } \\ \text { No. } \end{gathered}$ |
| Lane 1 | 289 | 52 | - | 341 | 3.0 | 735 | 0.465 | 100 | NA | NA |
| Lane 2 | - | 327 | 34 | 361 | 3.0 | 777 | 0.465 | 100 | NA | NA |
| Approach | 289 | 380 | 34 | 702 | 3.0 |  | 0.465 |  |  |  |
| East: WB Winneconne |  |  |  |  |  |  |  |  |  |  |


| Mov. <br> From E To Exit: | L2 S | T1 W | R2 N | Total | \%HV | Cap. veh/h | Deg. <br> Satn v/c | Lane Util. \% | Prob. SL Ov. \% | Ov. Lane No. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane 1 | 49 | 158 | - | 207 | 1.0 | 537 | 0.386 | 100 | NA | NA |
| Lane 2 | - | 221 | 5 | 226 | 1.0 | 585 | 0.386 | 100 | NA | NA |
| Approach | 49 | 378 | 5 | 433 | 1.0 |  | 0.386 |  |  |  |
| North: SB Commercial |  |  |  |  |  |  |  |  |  |  |
| Mov. From N To Exit: | L2 E | T1 S | R2 W | Total | \%HV | Cap. veh/h | Deg. Satn v/c | Lane Util. \% | Prob. SL Ov. \% | Ov Lane No. |
| Lane 1 | 2 | 311 | - | 314 | 4.0 | 682 | 0.460 | 100 | NA | NA |
| Lane 2 | - | 14 | 319 | 333 | 4.0 | 725 | 0.460 | 100 | NA | NA |
| Approach | 2 | 325 | 319 | 647 | 4.0 |  | 0.460 |  |  |  |
| West: EB Winneconne |  |  |  |  |  |  |  |  |  |  |
| Mov. <br> From W To Exit: | L2 N | T1 E | R2 S | Total | \%HV | Cap. veh/h | Deg. Satn v/c | Lane Util. \% | Prob SL Ov. \% | Ov Lane No. |
| Lane 1 | 328 | 116 | - | 444 | 2.0 | 949 | 0.468 | 100 | NA | NA |
| Lane 2 | - | 200 | 259 | 459 | 2.0 | 981 | 0.468 | 100 | NA | NA |
| Approach | 328 | 316 | 259 | 902 | 2.0 |  | 0.468 |  |  |  |
| Total \%HV Deg.Satn (v/c) |  |  |  |  |  |  |  |  |  |  |
| Intersection | 2684 | 2.6 |  | 0.468 |  |  |  |  |  |  |

Lane flow rates given in this report are based on the arrival flow rates subject to upstream capacity constraint where applicable.

| Merge Analysis |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{array}{r} \text { Exit } \\ \text { Lane } \\ \text { Number } \end{array}$ | Short Percent Opposing Lane Opng in Flow Rate Length Lane $\mathrm{ft} \quad \%$ veh/h pcu/h | Critical Gap sec | Follow-up Headway <br> sec | Lane Flow Rate veh/h | apacity <br> veh/h | Deg. Satn v/c |  | Merge Delay <br> sec |
| South Exit: NB Commercial Merge Type: Not Applied |  |  |  |  |  |  |  |  |
| Full Length Lane 1 <br> Full Length Lane 2 | Merge Analysis not applied. Merge Analysis not applied. |  |  |  |  |  |  |  |
| East Exit: WB Winneconne Merge Type: Not Applied |  |  |  |  |  |  |  |  |
| Full Length Lane 1 <br> Full Length Lane 2 | Merge Analysis not applied. Merge Analysis not applied. |  |  |  |  |  |  |  |
| North Exit: SB Commercial Merge Type: Not Applied |  |  |  |  |  |  |  |  |
| Full Length Lane 1 <br> Full Length Lane 2 | Merge Analysis not applied. Merge Analysis not applied. |  |  |  |  |  |  |  |
| West Exit: EB Winneconne Merge Type: Not Applied |  |  |  |  |  |  |  |  |
| Full Length Lane 1 <br> Full Length Lane 2 | Merge Analysis not applied. Merge Analysis not applied. |  |  |  |  |  |  |  |

[^6]
## ROUNDABOUT ANALYSIS

## $\nabla$ Site: 1 [Commercial \& Winneconne 4-leg 2022 AM Peak (Site Folder: 4-leg Alternative)]

Site Category: (None)
Roundabout

| Roundabout Basic Parameters |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Location | Name | Central Island Diam | Circ Width | Insc Diam | Entry Radius | Entry Angle | Circ Lanes | Entry Lanes | Av.Entry Lane Width | App. Dist | Prop Queued Upstr Signal | Extra Bunching |
|  |  | ft | ft | ft | ft |  |  |  | ft | ft |  | \% |
| South |  | 100.00 * | 30.00 * | $160.0{ }^{*}$ | $85.0{ }^{*}$ | $20.0{ }^{*}$ | 2 | 2 | 13.00 * | 1600.0 | $N A^{5}$ | 0.0 |
| East | Commercial WB | $100.0{ }^{*}$ | $30.00{ }^{*}$ | $160.0{ }^{*}$ | $85.0{ }^{*}$ | $20.0{ }^{*}$ | 2 | 2 | $13.00{ }^{*}$ | 1600.0 | $N A^{5}$ | 0.0 |
| North | Winneconne SB | $100.00{ }^{*}$ | $30.00{ }^{*}$ | $160.0{ }^{*}$ | $85.0{ }^{*}$ | $20.0{ }^{*}$ | 2 | 2 | $13.00{ }^{*}$ | 1600.0 | $N A^{5}$ | 0.0 |
| West | Commercial EB | $100.00^{*}$ | 30.00 * | $160.0 *$ | $85.0{ }^{*}$ | $20.0{ }^{*}$ | 2 | 2 | 13.00 * | 1600.0 | $N A^{5}$ | 0.0 |

Roundabout Capacity Model: US HCM 6
5 Not Applicable (single Site analysis or unconnected Site in Network analysis).

* These parameters do not affect estimated capacity values in the HCM 6 Capacity Model.

| Roundabout Entry and Circulating / Exiting Stream Parameters |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| To Approach | Turn | Lane <br> No | Lane Type | Opng Flow veh/h | Opng Flow pcu/h | Bunch Hdwy sec | Prop. Bunched | Cap Const Effect | Priority Sharing | $\begin{gathered} \text { OD } \\ \text { Factor } \end{gathered}$ | HVE for Entry | Critical [ Hdwy <br> sec | Gap Dist ] ft | Follow- <br> up Hdwy sec |
| South: NB Commercial Model Calibration Factor (HCM 6): 1.00 Entry/Circ Flow Adj (HCM 6): None |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| West | L2 | 1 | Subdom. | 646 | 659 | 0.00 | 0.000 | No | No | - | 1.03 | 4.60 | 135.6 | 2.60 |
| North | T1 | 1 | Subdom. | 646 | 659 | 0.00 | 0.000 | No | No | - | 1.03 | 4.60 | 135.6 | 2.60 |
| North | T1 | 2 | Dominant | 646 | 659 | 0.00 | 0.000 | No | No | - | 1.03 | 4.30 | 126.7 | 2.60 |
| East | R2 | 2 | Dominant | 646 | 659 | 0.00 | 0.000 | No | No | - | 1.03 | 4.30 | 126.7 | 2.60 |
| East: WB Winneconne <br> Model Calibration Factor (HCM 6): 1.00 Entry/Circ Flow Adj (HCM 6): None |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| South | L2 | 1 | Subdom. | 996 | 1023 | 0.00 | 0.000 | No | No | - | 1.01 | 4.60 | 129.4 | 2.60 |
| West | T1 | 1 | Subdom. | 996 | 1023 | 0.00 | 0.000 | No | No | - | 1.01 | 4.60 | 129.4 | 2.60 |
| West | T1 | 2 | Dominant | 996 | 1023 | 0.00 | 0.000 | No | No | - | 1.01 | 4.30 | 120.9 | 2.60 |
| North | R2 | 2 | Dominant | 996 | 1023 | 0.00 | 0.000 | No | No | - | 1.01 | 4.30 | 120.9 | 2.60 |
| North: SB Commercial <br> Model Calibration Factor (HCM 6): 1.00 <br> Entry/Circ Flow Adj (HCM 6): None |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| East | L2 | 1 | Subdom. | 717 | 730 | 0.00 | 0.000 | No | No | - | 1.04 | 4.60 | 137.8 | 2.60 |
| South | T1 | 1 | Subdom. | 717 | 730 | 0.00 | 0.000 | No | No | - | 1.04 | 4.60 | 137.8 | 2.60 |
| South | T1 | 2 | Dominant | 717 | 730 | 0.00 | 0.000 | No | No | - | 1.04 | 4.30 | 128.8 | 2.60 |
| West | R2 | 2 | Dominant | 717 | 730 | 0.00 | 0.000 | No | No | - | 1.04 | 4.30 | 128.8 | 2.60 |
| West: EB Winneconne <br> Model Calibration Factor (HCM 6): 1.00 <br> Entry/Circ Flow Adj (HCM 6): None |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| North | L2 | 1 | Subdom. | 377 | 391 | 0.00 | 0.000 | No | No | - | 1.02 | 4.60 | 156.9 | 2.60 |
| East | T1 | 1 | Subdom. | 377 | 391 | 0.00 | 0.000 | No | No | - | 1.02 | 4.60 | 156.9 | 2.60 |
| East | T1 | 2 | Dominant | 377 | 391 | 0.00 | 0.000 | No | No | - | 1.02 | 4.30 | 146.6 | 2.60 |
| South | R2 | 2 | Dominant | 377 | 391 | 0.00 | 0.000 | No | No | - | 1.02 | 4.30 | 146.6 | 2.60 |

## Roundabout Capacity Model: US HCM 6

| Circulating Lane Flow Rates |  |  |  |
| :--- | ---: | ---: | ---: |
| Circ. | Circulating Flow Rate |  |  |
| Lane |  |  |  |
| No | veh/h | pcu/h | Percent |
| South: NB Commercial |  |  |  |
| Lane 1 | 446 | 455 | 69.1 |
| Lane 2 | 200 | 204 | 30.9 |
| Approach | 646 | 659 |  |
| East: WB Winneconne |  |  |  |
| Lane 1 | 669 | 686 | 67.1 |
| Lane 2 | 327 | 337 | 32.9 |
| Approach | 996 | 1023 |  |
| North: SB Commercial |  |  |  |
| Lane 1 | 496 | 507 | 69.5 |
| Lane 2 | 221 | 223 | 30.5 |
| Approach | 717 | 730 |  |
| West: EB Winneconne |  |  |  |
| Lane 1 | 363 | 376 | 96.2 |
| Lane 2 | 14 | 15 | 3.8 |
| Approach | 377 | 391 |  |

Roundabout Capacity Model: The US HCM 6 roundabout capacity model option is in use.
This model considers only the total circulating flow and not the flow rates in individual circulating lanes.
To model the effects of flow distribution in circulating lanes on the entry capacity results, you should use the SIDRA Standard roundabout capacity model.

## Gap Acceptance Cycle Parameters (Lanes)

| Opposed Lane | Cycle <br> Time <br> sec | Blocked Time sec | Unblocked Time sec | Unblocked Time Ratio | Minimum Delay sec |
| :---: | :---: | :---: | :---: | :---: | :---: |
| South: NB Commercial |  |  |  |  |  |
| 1 | 12.38 | 5.61 | 6.76 | 0.547 | 4.9 |
| 2 | 11.71 | 4.95 | 6.76 | 0.578 | 4.6 |
| East: WB Winneconne |  |  |  |  |  |
| 1 | 12.31 | 7.49 | 4.82 | 0.391 | 6.7 |
| 2 | 11.30 | 6.48 | 4.82 | 0.426 | 6.2 |
| North: SB Commercial |  |  |  |  |  |
| 1 | 12.17 | 5.94 | 6.23 | 0.512 | 5.3 |
| 2 | 11.45 | 5.21 | 6.23 | 0.544 | 5.0 |
| West: EB Winneconne |  |  |  |  |  |
| 1 | 15.04 | 4.53 | 10.51 | 0.699 | 3.8 |
| 2 | 14.56 | 4.04 | 10.51 | 0.722 | 3.7 |

Roundabout Capacity Model: US HCM 6

Gap Acceptance Cycle Parameters (Movements)


| North | T1 | 1 | 12.38 | 5.61 | 6.76 | 0.547 | 4.9 |
| :--- | :--- | ---: | :--- | :--- | :--- | :--- | :--- |
| North | T1 | 2 | 11.71 | 4.95 | 6.76 | 0.578 | 4.6 |
| East | R2 | 2 | 11.71 | 4.95 | 6.76 | 0.578 | 4.6 |
| East: WB Winneconne |  |  |  |  |  |  |  |
| South | L2 | 1 | 12.31 | 7.49 | 4.82 | 0.391 | 6.7 |
| West | T1 | 1 | 12.31 | 7.49 | 4.82 | 0.391 | 6.7 |
| West | T1 | 2 | 11.30 | 6.48 | 4.82 | 0.426 | 6.2 |
| North | R2 | 2 | 11.30 | 6.48 | 4.82 | 0.426 | 6.2 |
| North: | SB Commercial |  |  |  |  |  |  |
| East | L2 | 1 | 12.17 | 5.94 | 6.23 | 0.512 | 5.3 |
| South | T1 | 1 | 12.17 | 5.94 | 6.23 | 0.512 | 5.3 |
| South | T1 | 2 | 11.45 | 5.21 | 6.23 | 0.544 | 5.0 |
| West | R2 | 2 | 11.45 | 5.21 | 6.23 | 0.544 | 5.0 |
| West: EB Winneconne |  |  |  |  |  |  |  |
| North | L2 | 1 | 15.04 | 4.53 | 10.51 | 0.699 | 3.8 |
| East | T1 | 1 | 15.04 | 4.53 | 10.51 | 0.699 | 3.8 |
| East | T1 | 2 | 14.56 | 4.04 | 10.51 | 0.722 | 3.7 |
| South | R2 | 2 | 14.56 | 4.04 | 10.51 | 0.722 | 3.7 |

Roundabout Capacity Model: US HCM 6

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## SITE LAYOUT

$\forall$ Site: 1 [Commercial \& Winneconne 4-leg 2022 PM Peak (Site
Folder: 4-leg Alternative)]
Site Category: (None)
Roundabout

Layout pictures are schematic functional drawings reflecting input data. They are not design drawings.


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## INPUT VOLUMES

Vehicles and pedestrians per 60 minutes
© Site: 1 [Commercial \& Winneconne 4-leg 2022 PM Peak (Site
Folder: 4-leg Alternative)]

Site Category: (None)
Roundabout

Volume Display Method: Total and \%

|  | R2 | T1 | L2 |
| :--- | ---: | ---: | ---: |
| Tot | 398 | 346 | 12 |
| LV | $99 \%$ | $99 \%$ | $99 \%$ |
| HV | $1 \%$ | $1 \%$ | $1 \%$ |



|  | All MCs | Light Vehicles (LV) | Heavy Vehicles (HV) |
| :--- | :---: | :---: | :---: |
| S: NB Commercial | 558 | 552 | 6 |
| E: WB Winneconne | 363 | 359 | 4 |
| N: SB Commercial | 756 | 748 | 8 |
| W: EB Winneconne | 755 | 747 | 8 |
| Total | 2432 | 2408 | 24 |

## LANE SUMMARY

## $\nabla$ Site: 1 [Commercial \& Winneconne 4-leg 2022 PM Peak (Site Folder: 4-leg Alternative)]

Site Category: (None)
Roundabout

| Lane Use and Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | $\begin{aligned} & \text { ND } \\ & \text { NS } \\ & \text { HV ] } \\ & \% \end{aligned}$ | Cap. <br> veh/h | Deg. Satn v/c | Lane Util. \% | Aver. Delay <br> sec | Level of Service | $\begin{gathered} 95 \% \text { \| } \\ \text { Q } \end{gathered}$ | $\begin{gathered} \mathrm{K} \text { OF } \\ \mathrm{JE} \\ \text { Dist ] } \\ \mathrm{ft} \end{gathered}$ | Lane Config | Lane Length | Cap. Adj. \% | Prob. <br> Block. <br> \% |
| South: NB Commercial |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane 1 | 296 | 1.0 | 790 | 0.374 | 100 | 9.1 | LOS A | 1.8 | 45.7 | Full | 1600 | 0.0 | 0.0 |
| Lane $2^{\text {d }}$ | 311 | 1.0 | 831 | 0.374 | 100 | 8.8 | LOS A | 1.7 | 43.4 | Full | 1600 | 0.0 | 0.0 |
| Approach | 607 | 1.0 |  | 0.374 |  | 8.9 | LOS A | 1.8 | 45.7 |  |  |  |  |
| East: WB Winneconne |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane 1 | 190 | 1.0 | 606 | 0.313 | 100 | 10.2 | LOS B | 1.3 | 32.6 | Full | 1600 | 0.0 | 0.0 |
| Lane $2^{\text {d }}$ | 205 | 1.0 | 653 | 0.313 | 100 | 9.6 | LOS A | 1.2 | 31.1 | Full | 1600 | 0.0 | 0.0 |
| Approach | 395 | 1.0 |  | 0.313 |  | 9.9 | LOS A | 1.3 | 32.6 |  |  |  |  |
| North: SB Commercial |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane 1 | 389 | 1.0 | 831 | 0.468 | $94^{5}$ | 10.4 | LOS B | 2.9 | 73.6 | Full | 1600 | 0.0 | 0.0 |
| Lane $2^{\text {d }}$ | 433 | 1.0 | 870 | 0.497 | 100 | 10.6 | LOS B | 3.2 | 81.2 | Full | 1600 | 0.0 | 0.0 |
| Approach | 822 | 1.0 |  | 0.497 |  | 10.5 | LOS B | 3.2 | 81.2 |  |  |  |  |
| West: EB Winneconne |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane 1 | 403 | 1.0 | 907 | 0.444 | 100 | 9.3 | LOS A | 2.6 | 65.7 | Full | 1600 | 0.0 | 0.0 |
| Lane $2^{\text {d }}$ | 418 | 1.0 | 942 | 0.444 | 100 | 9.1 | LOS A | 2.5 | 62.5 | Full | 1600 | 0.0 | 0.0 |
| Approach | 821 | 1.0 |  | 0.444 |  | 9.2 | LOS A | 2.6 | 65.7 |  |  |  |  |
| Intersection | 2643 | 1.0 |  | 0.497 |  | 9.7 | LOS A | 3.2 | 81.2 |  |  |  |  |

Site Level of Service (LOS) Method: Delay \& v/c (HCM 6). Site LOS Method is specified in the Parameter Settings dialog (Site tab).
Roundabout LOS Method: Same as Sign Control.
Lane LOS values are based on average delay and v/c ratio (degree of saturation) per lane.
LOS F will result if v/c > 1 irrespective of lane delay value (does not apply for approaches and intersection).
Intersection and Approach LOS values are based on average delay for all lanes ( $\mathrm{v} / \mathrm{c}$ not used as specified in HCM 6).
Roundabout Capacity Model: US HCM 6.
Delay Model: HCM Delay Formula (Geometric Delay is not included).
Queue Model: HCM Queue Formula.
Gap-Acceptance Capacity: Traditional M1.
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.
5 Lane under-utilisation found by the program
d Dominant lane on roundabout approach

Approach Lane Flows (veh/h)
South: NB Commercial

| Mov. <br> From S To Exit: | L2 W | T1 N | R2 E | Total | \%HV | Cap. veh/h | Deg. Satn v/c | Lane Util. \% | Prob. SL Ov. \% | $\begin{array}{r} \text { Ov. } \\ \text { Lane } \\ \text { No. } \end{array}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane 1 | 153 | 142 | - | 296 | 1.0 | 790 | 0.374 | 100 | NA | NA |
| Lane 2 | - | 272 | 39 | 311 | 1.0 | 831 | 0.374 | 100 | NA | NA |
| Approach | 153 | 414 | 39 | 607 | 1.0 |  | 0.374 |  |  |  |


| East: WB Winneconne |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov. <br> From E To Exit: | L2 S | T1 <br> W | R2 N | Total | \%HV | Cap. veh/h | Deg. Satn v/c | Lane Util. \% | Prob. SL Ov. \% | Ov Lane No. |
| Lane 1 | 58 | 132 | - | 190 | 1.0 | 606 | 0.313 | 100 | NA | NA |
| Lane 2 | - | 197 | 8 | 205 | 1.0 | 653 | 0.313 | 100 | NA | NA |
| Approach | 58 | 329 | 8 | 395 | 1.0 |  | 0.313 |  |  |  |
| North: SB Commercial |  |  |  |  |  |  |  |  |  |  |
| Mov. From N To Exit: | L2 E | T1 S | R2 W | Total | \%HV | Cap. veh/h | Deg. Satn v/c | Lane Util. \% | Prob. SL Ov. \% | Ov. Lane No. |
| Lane 1 | 13 | 376 | - | 389 | 1.0 | 831 | 0.468 | $94^{5}$ | NA | NA |
| Lane 2 | - | - | 433 | 433 | 1.0 | 870 | 0.497 | 100 | NA | NA |
| Approach | 13 | 376 | 433 | 822 | 1.0 |  | 0.497 |  |  |  |
| West: EB Winneconne |  |  |  |  |  |  |  |  |  |  |
| Mov. From W To Exit: | L2 N | T1 E | R2 S | Total | \%HV | Cap. veh/h | Deg. Satn v/c | Lane Util. \% | Prob. SL Ov. \% | $\begin{gathered} \text { Ov. } \\ \text { Lane } \\ \text { No. } \end{gathered}$ |
| Lane 1 | 314 | 88 | - | 403 | 1.0 | 907 | 0.444 | 100 | NA | NA |
| Lane 2 | - | 180 | 238 | 418 | 1.0 | 942 | 0.444 | 100 | NA | NA |
| Approach | 314 | 268 | 238 | 821 | 1.0 |  | 0.444 |  |  |  |
| Total \%HV Deg.Satn (v/c) |  |  |  |  |  |  |  |  |  |  |
| Intersection | 2643 | 1.0 |  | 0.497 |  |  |  |  |  |  |

Lane flow rates given in this report are based on the arrival flow rates subject to upstream capacity constraint where applicable.
5 Lane under-utilisation found by the program

| Merge Analysis |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Exit Lane Number | Short Percent Opposing Lane Opng in Flow Rate Length Lane $\mathrm{ft} \quad \%$ veh/h pcu/h | Critical Gap sec | Follow-up Lane Headway Flow Rate sec veh/h | Capacity <br> veh/h | Deg. Satn v/c |  | Merge Delay sec |
| South Exit: NB Commercial Merge Type: Not Applied |  |  |  |  |  |  |  |
| Full Length Lane 1 <br> Full Length Lane 2 | Merge Analysis not applied. Merge Analysis not applied. |  |  |  |  |  |  |
| East Exit: WB Winneconne Merge Type: Not Applied |  |  |  |  |  |  |  |
| Full Length Lane 1 <br> Full Length Lane 2 | Merge Analysis not applied. Merge Analysis not applied. |  |  |  |  |  |  |
| North Exit: SB Commercial Merge Type: Not Applied |  |  |  |  |  |  |  |
| Full Length Lane 1 <br> Full Length Lane 2 | Merge Analysis not applied. <br> Merge Analysis not applied. |  |  |  |  |  |  |
| West Exit: EB Winneconne Merge Type: Not Applied |  |  |  |  |  |  |  |
| Full Length Lane 1 <br> Full Length Lane 2 | Merge Analysis not applied. <br> Merge Analysis not applied. |  |  |  |  |  |  |

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## ROUNDABOUT ANALYSIS

## $\nabla$ Site: 1 [Commercial \& Winneconne 4-leg 2022 PM Peak (Site Folder: 4-leg Alternative)]

Site Category: (None)
Roundabout

| Roundabout Basic Parameters |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Location | Name | Central Island Diam | Circ Width | Insc Diam | Entry Radius | Entry Angle | Circ Lanes | Entry Lanes | Av.Entry Lane Width | App. Dist | Prop Queued Upstr Signal | Extra Bunching |
|  |  | ft | ft | ft | ft |  |  |  | ft | ft |  | \% |
| South | NB | 100.00 * | $30.00{ }^{*}$ | $160.0{ }^{*}$ | $85.0{ }^{*}$ | $20.0{ }^{*}$ | 2 | 2 | $13.00{ }^{*}$ | 1600.0 | $N A^{5}$ | 0.0 |
| East | Commercial WB | $100.00{ }^{*}$ | $30.00{ }^{*}$ | $160.0{ }^{*}$ | $85.0{ }^{*}$ | $20.0{ }^{*}$ | 2 | 2 | $13.00{ }^{*}$ | 1600.0 | $N A^{5}$ | 0.0 |
| North | Winneconne SB | $100.00{ }^{*}$ | $30.00{ }^{*}$ | $160.0{ }^{*}$ | $85.0{ }^{*}$ | $20.0{ }^{*}$ | 2 | 2 | $13.00{ }^{*}$ | 1600.0 | $N A^{5}$ | 0.0 |
| West | Commercial | $100.00^{*}$ | $30.00 *$ | 160.0 * | $85.0{ }^{*}$ | $20.0{ }^{*}$ | 2 | 2 | $13.00{ }^{*}$ | 1600.0 | $N A^{5}$ | 0.0 |

Roundabout Capacity Model: US HCM 6
5 Not Applicable (single Site analysis or unconnected Site in Network analysis).

* These parameters do not affect estimated capacity values in the HCM 6 Capacity Model.

| Roundabout Entry and Circulating / Exiting Stream Parameters |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| To Approach | Turn | Lane <br> No | Lane Type | Opng Flow veh/h | Opng Flow <br> pcu/h | In- <br> Bunch Hdwy sec | Prop. | Cap Const Effect | Priority Sharing | $\begin{gathered} \text { OD } \\ \text { Factor } \end{gathered}$ | HVE for Entry | Critical [ Hdwy <br> sec | Gap Dist ] ft | Followup <br> Hdwy sec |
| South: NB Commercial <br> Model Calibration Factor (HCM 6): 1.00 <br> Entry/Circ Flow Adj (HCM 6): None |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| West | L2 | 1 | Subdom. | 596 | 602 | 0.00 | 0.000 | No | No | - | 1.01 | 4.60 | 133.4 | 2.60 |
| North | T1 | 1 | Subdom. | 596 | 602 | 0.00 | 0.000 | No | No | - | 1.01 | 4.60 | 133.4 | 2.60 |
| North | T1 | 2 | Dominant | 596 | 602 | 0.00 | 0.000 | No | No | - | 1.01 | 4.30 | 124.7 | 2.60 |
| East | R2 | 2 | Dominant | 596 | 602 | 0.00 | 0.000 | No | No | - | 1.01 | 4.30 | 124.7 | 2.60 |
| East: WB Winneconne <br> Model Calibration Factor (HCM 6): 1.00 <br> Entry/Circ Flow Adj (HCM 6): None |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| South | L2 | 1 | Subdom. | 882 | 890 | 0.00 | 0.000 | No | No | - | 1.01 | 4.60 | 134.5 | 2.60 |
| West | T1 | 1 | Subdom. | 882 | 890 | 0.00 | 0.000 | No | No | - | 1.01 | 4.60 | 134.5 | 2.60 |
| West | T1 | 2 | Dominant | 882 | 890 | 0.00 | 0.000 | No | No | - | 1.01 | 4.30 | 125.7 | 2.60 |
| North | R2 | 2 | Dominant | 882 | 890 | 0.00 | 0.000 | No | No | - | 1.01 | 4.30 | 125.7 | 2.60 |
| North: SB Commercial <br> Model Calibration Factor (HCM 6): 1.00 <br> Entry/Circ Flow Adj (HCM 6): None |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| East | L2 | 1 | Subdom. | 540 | 546 | 0.00 | 0.000 | No | No | - | 1.01 | 4.60 | 142.5 | 2.60 |
| South | T1 | 1 | Subdom. | 540 | 546 | 0.00 | 0.000 | No | No | - | 1.01 | 4.60 | 142.5 | 2.60 |
| West | R2 | 2 | Dominant | 540 | 546 | 0.00 | 0.000 | No | No | - | 1.01 | 4.30 | 133.1 | 2.60 |
| West: EB Winneconne <br> Model Calibration Factor (HCM 6): 1.00 <br> Entry/Circ Flow Adj (HCM 6): None |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| North | L2 | 1 | Subdom. | 447 | 451 | 0.00 | 0.000 | No | No | - | 1.01 | 4.60 | 155.8 | 2.60 |
| East | T1 | 1 | Subdom. | 447 | 451 | 0.00 | 0.000 | No | No | - | 1.01 | 4.60 | 155.8 | 2.60 |
| East | T1 | 2 | Dominant | 447 | 451 | 0.00 | 0.000 | No | No | - | 1.01 | 4.30 | 145.5 | 2.60 |
| South | R2 | 2 | Dominant | 447 | 451 | 0.00 | 0.000 | No | No | - | 1.01 | 4.30 | 145.5 | 2.60 |

Roundabout Capacity Model: US HCM 6

| Circulating Lane Flow Rates |  |  |  |
| :--- | ---: | ---: | ---: |
| Circ. |  |  |  |
| Lane |  |  |  |
| No |  |  |  |
|  | veh/h | pculh | Percent |
| South: NB Commercial |  |  |  |
| Lane 1 | 416 | 420 | 69.8 |
| Lane 2 | 180 | 182 | 30.2 |
| Approach | 596 | 602 |  |
| East: WB Winneconne |  |  |  |
| Lane 1 | 610 | 616 | 69.2 |
| Lane 2 | 272 | 275 | 30.8 |
| Approach | 882 | 890 |  |
| North: SB Commercial |  |  |  |
| Lane 1 | 343 | 347 | 63.5 |
| Lane 2 | 197 | 199 | 36.5 |
| Approach | 540 | 546 |  |
| West: EB Winneconne |  |  |  |
| Lane 1 | 447 | 0 | 451 |
| Lane 2 | 447 | 451 | 100.0 |
| Approach |  | 0.0 |  |

Roundabout Capacity Model: The US HCM 6 roundabout capacity model option is in use.
This model considers only the total circulating flow and not the flow rates in individual circulating lanes.
To model the effects of flow distribution in circulating lanes on the entry capacity results, you should use the SIDRA Standard roundabout capacity model.

| Gap Acceptance Cycle Parameters (Lanes) |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Opposed Lane | Cycle <br> Time sec | Blocked Time sec | Unblocked Time sec | Unblocked Time Ratio | Minimum Delay sec |
| South: NB Commercial |  |  |  |  |  |
| 1 | 12.65 | 5.36 | 7.28 | 0.576 | 4.6 |
| 2 | 12.02 | 4.74 | 7.28 | 0.606 | 4.3 |
| East: WB Winneconne |  |  |  |  |  |
| 1 | 12.09 | 6.75 | 5.34 | 0.442 | 5.9 |
| 2 | 11.22 | 5.87 | 5.34 | 0.476 | 5.5 |
| North: SB Commercial |  |  |  |  |  |
| 1 | 13.03 | 5.13 | 7.90 | 0.606 | 4.3 |
| 2 | 12.44 | 4.54 | 7.90 | 0.635 | 4.1 |
| West: EB Winneconne |  |  |  |  |  |
| 1 | 14.03 | 4.75 | 9.28 | 0.661 | 4.0 |
| 2 | 13.51 | 4.23 | 9.28 | 0.687 | 3.8 |

Roundabout Capacity Model: US HCM 6

| Gap Acceptance Cycle Parameters (Movements) |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| To <br> Approach | Turn | Opsd | Cycle | Blocked | Unblocked | Unblocked | Minimum |
|  |  | Lane No | Time | Time | Time | Time Ratio | Delay |
|  |  |  | sec | sec | sec |  | sec |
| South: NB Commercial |  |  |  |  |  |  |  |
| West | L2 | 1 | 12.65 | 5.36 | 7.28 | 0.576 | 4.6 |
| North | T1 | 1 | 12.65 | 5.36 | 7.28 | 0.576 | 4.6 |
| North | T1 | 2 | 12.02 | 4.74 | 7.28 | 0.606 | 4.3 |


| East | R2 | 2 | 12.02 | 4.74 | 7.28 | 0.606 | 4.3 |
| :--- | ---: | ---: | :--- | :--- | :--- | :--- | :--- |
| East: WB Winneconne |  |  |  |  |  |  |  |
| South | L2 | 1 | 12.09 | 6.75 | 5.34 | 0.442 | 5.9 |
| West | T1 | 1 | 12.09 | 6.75 | 5.34 | 0.442 | 5.9 |
| West | T1 | 2 | 11.22 | 5.87 | 5.34 | 0.476 | 5.5 |
| North | R2 | 2 | 11.22 | 5.87 | 5.34 | 0.476 | 5.5 |
| North: | SB Commercial |  |  |  |  |  |  |
| East | L2 | 1 | 13.03 | 5.13 | 7.90 | 0.606 | 4.3 |
| South | T1 | 1 | 13.03 | 5.13 | 7.90 | 0.606 | 4.3 |
| West | R2 | 2 | 12.44 | 4.54 | 7.90 | 0.635 | 4.1 |
| West: EB Winneconne |  |  |  |  |  |  |  |
| North | L2 | 1 | 14.03 | 4.75 | 9.28 | 0.661 | 4.0 |
| East | T1 | 1 | 14.03 | 4.75 | 9.28 | 0.661 | 4.0 |
| East | T1 | 2 | 13.51 | 4.23 | 9.28 | 0.687 | 3.8 |
| South | R2 | 2 | 13.51 | 4.23 | 9.28 | 0.687 | 3.8 |

Roundabout Capacity Model: US HCM 6

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## SITE LAYOUT

$\forall$ Site: 1 [Commercial \& Winneconne 4-leg 2042 AM Peak (Site
Folder: 4-leg Alternative)]
Site Category: (None)
Roundabout

Layout pictures are schematic functional drawings reflecting input data. They are not design drawings.


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## INPUT VOLUMES

Vehicles and pedestrians per 60 minutes
( Site: 1 [Commercial \& Winneconne 4-leg 2042 AM Peak (Site
Folder: 4-leg Alternative)]

Site Category: (None)
Roundabout

Volume Display Method: Total and \%

|  | R2 | T1 | L2 |
| :--- | ---: | ---: | ---: |
| Tot | 309 | 315 | 2 |
| LV | $96 \%$ | $96 \%$ | $98 \%$ |
| HV | $4 \%$ | $4 \%$ | $4 \%$ |



|  | All MCs | Light Vehicles (LV) | Heavy Vehicles (HV) |
| :--- | :---: | :---: | :---: |
| S: NB Commercial | 680 | 660 | 20 |
| E: WB Winneconne | 419 | 415 | 4 |
| N: SB Commercial | 626 | 601 | 25 |
| W: EB Winneconne | 875 | 858 | 18 |
| Total | 2600 | 2533 | 67 |

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## LANE SUMMARY

## $\nabla$ Site: 1 [Commercial \& Winneconne 4-leg 2042 AM Peak (Site Folder: 4-leg Alternative)]

Site Category: (None)
Roundabout

| Lane Use and Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | DEMAND FLOWS |  | Cap. <br> veh/h | Deg. Satn v/c | Lane Util. \% | Aver. Delay <br> sec | Level of Service | 95\% BACK OF QUEUE |  | Lane Config | Lane Length ft | Cap. Adj. \% | Prob. Block. $\qquad$ |
| South: NB Commercial |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane 1 | 396 | 3.0 | 664 | 0.597 | 100 | 16.1 | LOS C | 4.2 | 108.4 | Full | 1600 | 0.0 | 0.0 |
| Lane $2^{\text {d }}$ | 423 | 3.0 | 708 | 0.597 | 100 | 15.3 | LOS C | 4.2 | 106.6 | Full | 1600 | 0.0 | 0.0 |
| Approach | 819 | 3.0 |  | 0.597 |  | 15.7 | LOS C | 4.2 | 108.4 |  |  |  |  |
| East: WB Winneconne |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane 1 | 240 | 1.0 | 459 | 0.522 | 100 | 18.7 | LOS C | 2.6 | 66.5 | Full | 1600 | 0.0 | 0.0 |
| Lane $2^{\text {d }}$ | 265 | 1.0 | 507 | 0.522 | 100 | 17.2 | LOS C | 2.6 | 65.5 | Full | 1600 | 0.0 | 0.0 |
| Approach | 505 | 1.0 |  | 0.522 |  | 17.9 | LOS C | 2.6 | 66.5 |  |  |  |  |
| North: SB Commercial |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane 1 | 364 | 4.0 | 610 | 0.596 | 100 | 17.2 | LOS C | 3.9 | 101.8 | Full | 1600 | 0.0 | 0.0 |
| Lane $2^{\text {d }}$ | 391 | 4.0 | 655 | 0.596 | 100 | 16.2 | LOS C | 3.9 | 100.3 | Full | 1600 | 0.0 | 0.0 |
| Approach | 754 | 4.0 |  | 0.596 |  | 16.7 | LOS C | 3.9 | 101.8 |  |  |  |  |
| West: EB Winneconne |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane 1 | 517 | 2.0 | 894 | 0.578 | 100 | 12.3 | LOS B | 5.0 | 128.1 | Full | 1600 | 0.0 | 0.0 |
| Lane $2^{\text {d }}$ | 537 | 2.0 | 929 | 0.578 | 100 | 11.9 | LOS B | 4.9 | 124.4 | Full | 1600 | 0.0 | 0.0 |
| Approach | 1054 | 2.0 |  | 0.578 |  | 12.1 | LOS B | 5.0 | 128.1 |  |  |  |  |
| Intersection | 3133 | 2.6 |  | 0.597 |  | 15.1 | LOS C | 5.0 | 128.1 |  |  |  |  |

Site Level of Service (LOS) Method: Delay \& v/c (HCM 6). Site LOS Method is specified in the Parameter Settings dialog (Site tab).
Roundabout LOS Method: Same as Sign Control.
Lane LOS values are based on average delay and v/c ratio (degree of saturation) per lane.
LOS F will result if v/c > 1 irrespective of lane delay value (does not apply for approaches and intersection).
Intersection and Approach LOS values are based on average delay for all lanes ( $\mathrm{v} / \mathrm{c}$ not used as specified in HCM 6).
Roundabout Capacity Model: US HCM 6.
Delay Model: HCM Delay Formula (Geometric Delay is not included).
Queue Model: HCM Queue Formula.
Gap-Acceptance Capacity: Traditional M1.
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.
d Dominant lane on roundabout approach

| Approach Lane Flows (veh/h) |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| South: NB Commercial |  |  |  |  |  |  |  |  |  |  |
| Mov. <br> From S To Exit: | L2 W | T1 N | R2 E | Total | \%HV | Cap. veh/h | Deg. Satn v/c | Lane Util. \% | Prob. SL Ov. \% | $\begin{gathered} \text { Ov. } \\ \text { Lane } \\ \text { No. } \end{gathered}$ |
| Lane 1 | 337 | 59 | - | 396 | 3.0 | 664 | 0.597 | 100 | NA | NA |
| Lane 2 | - | 383 | 40 | 423 | 3.0 | 708 | 0.597 | 100 | NA | NA |
| Approach | 337 | 442 | 40 | 819 | 3.0 |  | 0.597 |  |  |  |
| East: WB Winneconne |  |  |  |  |  |  |  |  |  |  |


| Mov. <br> From E To Exit: | L2 S | T1 W | R2 N | Total | \%HV | Cap. veh/h | Deg. Satn v/c | Lane Util. \% | Prob. SL Ov. \% | $\begin{gathered} \text { Ov. } \\ \text { Lane } \\ \text { No. } \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane 1 | 58 | 182 | - | 240 | 1.0 | 459 | 0.522 | 100 | NA | NA |
| Lane 2 | - | 259 | 6 | 265 | 1.0 | 507 | 0.522 | 100 | NA | NA |
| Approach | 58 | 441 | 6 | 505 | 1.0 |  | 0.522 |  |  |  |
| North: SB Commercial |  |  |  |  |  |  |  |  |  |  |
| Mov. From N To Exit: | L2 E | T1 S | R2 W | Total | \%HV | Cap. veh/h | Deg. Satn v/c | Lane Util. \% | Prob. SL Ov. \% | $\begin{gathered} \text { Ov. } \\ \text { Lane } \\ \text { No. } \end{gathered}$ |
| Lane 1 | 2 | 361 | - | 364 | 4.0 | 610 | 0.596 | 100 | NA | NA |
| Lane 2 | - | 18 | 372 | 391 | 4.0 | 655 | 0.596 | 100 | NA | NA |
| Approach | 2 | 380 | 372 | 754 | 4.0 |  | 0.596 |  |  |  |
| West: EB Winneconne |  |  |  |  |  |  |  |  |  |  |
| Mov. <br> From W To Exit: | L2 N | T1 E | R2 S | Total | \%HV | Cap. veh/h | Deg. Satn v/c | Lane Util. \% | Prob. SL Ov. \% | $\begin{gathered} \text { Ov. } \\ \text { Lane } \\ \text { No. } \end{gathered}$ |
| Lane 1 | 383 | 134 | - | 517 | 2.0 | 894 | 0.578 | 100 | NA | NA |
| Lane 2 | - | 235 | 302 | 537 | 2.0 | 929 | 0.578 | 100 | NA | NA |
| Approach | 383 | 369 | 302 | 1054 | 2.0 |  | 0.578 |  |  |  |
| Total \%HV Deg.Satn (v/c) |  |  |  |  |  |  |  |  |  |  |
| Intersection | 3133 | 2.6 |  | 0.597 |  |  |  |  |  |  |

Lane flow rates given in this report are based on the arrival flow rates subject to upstream capacity constraint where applicable.

| Merge Analysis |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Exit Lane Number | Short Percent Opposing <br> Lane Opng in Flow Rate <br> Length Lane <br> ft $\%$ veh/h pcu/h | Critical Gap sec | Follow-up Lane Headway Flow Rate sec veh/h | Capacity <br> veh/h | Deg. Satn v/c | Min. celay sec | Merge Delay <br> sec |
| South Exit: NB Commercial Merge Type: Not Applied |  |  |  |  |  |  |  |
| Full Length Lane 1 <br> Full Length Lane 2 | Merge Analysis not applied. <br> Merge Analysis not applied. |  |  |  |  |  |  |
| East Exit: WB Winneconne Merge Type: Not Applied |  |  |  |  |  |  |  |
| Full Length Lane 1 <br> Full Length Lane 2 | Merge Analysis not applied. <br> Merge Analysis not applied. |  |  |  |  |  |  |
| North Exit: SB Commercial Merge Type: Not Applied |  |  |  |  |  |  |  |
| Full Length Lane 1 <br> Full Length Lane 2 | Merge Analysis not applied. <br> Merge Analysis not applied. |  |  |  |  |  |  |
| West Exit: EB Winneconne Merge Type: Not Applied |  |  |  |  |  |  |  |
| Full Length Lane 1 <br> Full Length Lane 2 | Merge Analysis not applied. <br> Merge Analysis not applied. |  |  |  |  |  |  |

[^7]
## ROUNDABOUT ANALYSIS

## $\forall$ Site: 1 [Commercial \& Winneconne 4-leg 2042 AM Peak (Site Folder: 4-leg Alternative)]

Site Category: (None)
Roundabout

| Roundabout Basic Parameters |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Location | Name | Central Island Diam | Circ Width | Insc Diam | Entry Radius | Entry Angle | Circ Lanes | Entry Lanes | Av.Entry Lane Width | App. Dist | Prop Queued Upstr Signal | Extra Bunching |
|  |  | ft | ft | ft | ft |  |  |  | ft | ft |  | \% |
| South |  | 100.00 * | 30.00 * | $160.0{ }^{*}$ | $85.0{ }^{*}$ | $20.0{ }^{*}$ | 2 | 2 | 13.00 * | 1600.0 | $N A^{5}$ | 0.0 |
| East | Commercial WB | $100.0{ }^{*}$ | $30.00{ }^{*}$ | $160.0{ }^{*}$ | $85.0{ }^{*}$ | $20.0{ }^{*}$ | 2 | 2 | $13.00{ }^{*}$ | 1600.0 | $N A^{5}$ | 0.0 |
| North | Winneconne SB | $100.00{ }^{*}$ | $30.00{ }^{*}$ | $160.0{ }^{*}$ | $85.0{ }^{*}$ | $20.0{ }^{*}$ | 2 | 2 | $13.00{ }^{*}$ | 1600.0 | $N A^{5}$ | 0.0 |
| West | Commercial EB | $100.00^{*}$ | 30.00 * | $160.0 *$ | $85.0{ }^{*}$ | $20.0{ }^{*}$ | 2 | 2 | 13.00 * | 1600.0 | $N A^{5}$ | 0.0 |

Roundabout Capacity Model: US HCM 6
5 Not Applicable (single Site analysis or unconnected Site in Network analysis).

* These parameters do not affect estimated capacity values in the HCM 6 Capacity Model.

| Roundabout Entry and Circulating / Exiting Stream Parameters |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| To Approach | Turn | Lane <br> No | Lane Type | Opng Flow veh/h | Opng Flow pcu/h | Bunch Hdwy sec | Prop. | Cap Const Effect | Priority Sharing | $\begin{gathered} \text { OD } \\ \text { Factor } \end{gathered}$ | HVE for Entry | Critical [ Hdwy <br> sec | Gap Dist ] ft | Follow- <br> up Hdwy sec |
| South: NB Commercial <br> Model Calibration Factor (HCM 6): 1.00 <br> Entry/Circ Flow Adj (HCM 6): None |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| West | L2 | 1 | Subdom. | 754 | 769 | 0.00 | 0.000 | No | No | - | 1.03 | 4.60 | 135.6 | 2.60 |
| North | T1 | 1 | Subdom. | 754 | 769 | 0.00 | 0.000 | No | No | - | 1.03 | 4.60 | 135.6 | 2.60 |
| North | T1 | 2 | Dominant | 754 | 769 | 0.00 | 0.000 | No | No | - | 1.03 | 4.30 | 126.7 | 2.60 |
| East | R2 | 2 | Dominant | 754 | 769 | 0.00 | 0.000 | No | No | - | 1.03 | 4.30 | 126.7 | 2.60 |
| East: WB Winneconne <br> Model Calibration Factor (HCM 6): 1.00 Entry/Circ Flow Adj (HCM 6): None |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| South | L2 | 1 | Subdom. | 1163 | 1194 | 0.00 | 0.000 | No | No | - | 1.01 | 4.60 | 129.4 | 2.60 |
| West | T1 | 1 | Subdom. | 1163 | 1194 | 0.00 | 0.000 | No | No | - | 1.01 | 4.60 | 129.4 | 2.60 |
| West | T1 | 2 | Dominant | 1163 | 1194 | 0.00 | 0.000 | No | No | - | 1.01 | 4.30 | 120.9 | 2.60 |
| North | R2 | 2 | Dominant | 1163 | 1194 | 0.00 | 0.000 | No | No | - | 1.01 | 4.30 | 120.9 | 2.60 |
| North: SB Commercial <br> Model Calibration Factor (HCM 6): 1.00 <br> Entry/Circ Flow Adj (HCM 6): None |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| East | L2 | 1 | Subdom. | 836 | 851 | 0.00 | 0.000 | No | No | - | 1.04 | 4.60 | 137.8 | 2.60 |
| South | T1 | 1 | Subdom. | 836 | 851 | 0.00 | 0.000 | No | No | - | 1.04 | 4.60 | 137.8 | 2.60 |
| South | T1 | 2 | Dominant | 836 | 851 | 0.00 | 0.000 | No | No | - | 1.04 | 4.30 | 128.7 | 2.60 |
| West | R2 | 2 | Dominant | 836 | 851 | 0.00 | 0.000 | No | No | - | 1.04 | 4.30 | 128.7 | 2.60 |
| West: EB Winneconne <br> Model Calibration Factor (HCM 6): 1.00 <br> Entry/Circ Flow Adj (HCM 6): None |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| North | L2 | 1 | Subdom. | 440 | 456 | 0.00 | 0.000 | No | No | - | 1.02 | 4.60 | 157.0 | 2.60 |
| East | T1 | 1 | Subdom. | 440 | 456 | 0.00 | 0.000 | No | No | - | 1.02 | 4.60 | 157.0 | 2.60 |
| East | T1 | 2 | Dominant | 440 | 456 | 0.00 | 0.000 | No | No | - | 1.02 | 4.30 | 146.6 | 2.60 |
| South | R2 | 2 | Dominant | 440 | 456 | 0.00 | 0.000 | No | No | - | 1.02 | 4.30 | 146.6 | 2.60 |

## Roundabout Capacity Model: US HCM 6

| Circulating Lane Flow Rates |  |  |  |
| :--- | ---: | ---: | ---: |
| Circ. <br> Lane | Circulating Flow Rate |  |  |
| No |  |  |  |
|  | veh/h | pcu/h | Percent |
| South: NB Commercial |  |  |  |
| Lane 1 | 519 | 530 | 68.9 |
| Lane 2 | 235 | 239 | 31.1 |
| Approach | 754 | 769 |  |
| East: WB Winneconne |  |  |  |
| Lane 1 | 780 | 799 | 66.9 |
| Lane 2 | 383 | 395 | 33.1 |
| Approach | 1163 | 1194 |  |
| North: SB Commercial |  |  |  |
| Lane 1 | 577 | 590 | 69.3 |
| Lane 2 | 259 | 262 | 30.7 |
| Approach | 836 | 851 |  |
| West: EB Winneconne |  |  |  |
| Lane 1 | 421 | 437 | 95.8 |
| Lane 2 | 18 | 19 | 4.2 |
| Approach | 440 | 456 |  |

Roundabout Capacity Model: The US HCM 6 roundabout capacity model option is in use.
This model considers only the total circulating flow and not the flow rates in individual circulating lanes.
To model the effects of flow distribution in circulating lanes on the entry capacity results, you should use the SIDRA Standard roundabout capacity model.

## Gap Acceptance Cycle Parameters (Lanes)

| Opposed <br> Lane | Cycle <br> Time <br> sec | Blocked <br> Time <br> sec | Unblocked <br> Time <br> sec | Unblocked <br> Time Ratio | Minimum <br> Delay <br> sec |
| :--- | ---: | ---: | ---: | ---: | ---: |
| South: NB Commercial | 12.11 | 6.13 | 5.98 | 0.494 | 5.4 |
| 1 | 11.35 | 5.37 | 5.98 | 0.527 | 5.1 |
| 2 | 12.89 | 8.58 | 4.32 | 0.335 | 7.8 |
| East: WB Winneconne | 11.66 | 7.35 | 4.32 | 0.370 | 7.1 |
| 1 | 12.07 | 6.54 | 5.53 | 0.458 | 5.9 |
| 2 | 11.24 | 5.71 | 5.53 | 0.492 | 5.5 |
| North: SB Commercial |  |  |  |  |  |
| 1 | 13.97 | 4.77 | 9.20 | 0.658 | 4.0 |
| 2 | 13.45 | 4.25 | 9.20 | 0.684 | 3.9 |
| West: EB Winneconne |  |  |  |  |  |
| 1 |  |  |  |  |  |

Roundabout Capacity Model: US HCM 6

Gap Acceptance Cycle Parameters (Movements)


| North | T1 | 1 | 12.11 | 6.13 | 5.98 | 0.494 | 5.4 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| North | T1 | 2 | 11.35 | 5.37 | 5.98 | 0.527 | 5.1 |
| East | R2 | 2 | 11.35 | 5.37 | 5.98 | 0.527 | 5.1 |
| East: WB Winneconne |  |  |  |  |  |  |  |
| South | L2 | 1 | 12.89 | 8.58 | 4.32 | 0.335 | 7.8 |
| West | T1 | 1 | 12.89 | 8.58 | 4.32 | 0.335 | 7.8 |
| West | T1 | 2 | 11.66 | 7.35 | 4.32 | 0.370 | 7.1 |
| North | R2 | 2 | 11.66 | 7.35 | 4.32 | 0.370 | 7.1 |
| North: | CB Commercial |  |  |  |  |  |  |
| East | L2 | 1 | 12.07 | 6.54 | 5.53 | 0.458 | 5.9 |
| South | T1 | 1 | 12.07 | 6.54 | 5.53 | 0.458 | 5.9 |
| South | T1 | 2 | 11.24 | 5.71 | 5.53 | 0.492 | 5.5 |
| West | R2 | 2 | 11.24 | 5.71 | 5.53 | 0.492 | 5.5 |
| West: EB Winneconne |  |  |  |  |  |  |  |
| North | L2 | 1 | 13.97 | 4.77 | 9.20 | 0.658 | 4.0 |
| East | T1 | 1 | 13.97 | 4.77 | 9.20 | 0.658 | 4.0 |
| East | T1 | 2 | 13.45 | 4.25 | 9.20 | 0.684 | 3.9 |
| South | R2 | 2 | 13.45 | 4.25 | 9.20 | 0.684 | 3.9 |

Roundabout Capacity Model: US HCM 6

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## ROUNDABOUT ANALYSIS

## $\nabla$ Site: 1 [Commercial \& Winneconne 4-leg 2042 PM Peak (Site Folder: 4-leg Alternative)]

Site Category: (None)
Roundabout

| Roundabout Basic Parameters |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Location | Name | Central Island Diam | Circ Width | Insc Diam | Entry Radius | Entry Angle | Circ Lanes | Entry Lanes | Av.Entry Lane Width | App. Dist | Prop Queued Upstr Signal | Extra Bunching |
|  |  | ft | ft | ft | ft |  |  |  | ft | ft |  | \% |
| South | NB | 100.00 * | $30.00{ }^{*}$ | $160.0{ }^{*}$ | $85.0{ }^{*}$ | $20.0{ }^{*}$ | 2 | 2 | $13.00{ }^{*}$ | 1600.0 | $N A^{5}$ | 0.0 |
| East | Commercial WB | $100.00{ }^{*}$ | $30.00{ }^{*}$ | $160.0{ }^{*}$ | $85.0{ }^{*}$ | $20.0{ }^{*}$ | 2 | 2 | $13.00{ }^{*}$ | 1600.0 | $N A^{5}$ | 0.0 |
| North | Winneconne SB | $100.00{ }^{*}$ | $30.00{ }^{*}$ | $160.0{ }^{*}$ | $85.0{ }^{*}$ | $20.0{ }^{*}$ | 2 | 2 | $13.00{ }^{*}$ | 1600.0 | $N A^{5}$ | 0.0 |
| West | Commercial | $100.00^{*}$ | $30.00 *$ | 160.0 * | $85.0{ }^{*}$ | $20.0{ }^{*}$ | 2 | 2 | $13.00{ }^{*}$ | 1600.0 | $N A^{5}$ | 0.0 |

Roundabout Capacity Model: US HCM 6
5 Not Applicable (single Site analysis or unconnected Site in Network analysis).

* These parameters do not affect estimated capacity values in the HCM 6 Capacity Model.

| Roundabout Entry and Circulating / Exiting Stream Parameters |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| To Approach | Turn | Lane <br> No | Lane Type | Opng Flow veh/h | Opng Flow <br> pcu/h | In- <br> Bunch Hdwy sec | Prop. | Cap Const Effect | Priority Sharing | $\begin{gathered} \text { OD } \\ \text { Factor } \end{gathered}$ | HVE for Entry | Critical [ Hdwy <br> sec | Gap Dist ] ft | Followup <br> Hdwy sec |
| South: NB Commercial <br> Model Calibration Factor (HCM 6): 1.00 <br> Entry/Circ Flow Adj (HCM 6): None |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| West | L2 | 1 | Subdom. | 697 | 704 | 0.00 | 0.000 | No | No | - | 1.01 | 4.60 | 133.4 | 2.60 |
| North | T1 | 1 | Subdom. | 697 | 704 | 0.00 | 0.000 | No | No | - | 1.01 | 4.60 | 133.4 | 2.60 |
| North | T1 | 2 | Dominant | 697 | 704 | 0.00 | 0.000 | No | No | - | 1.01 | 4.30 | 124.7 | 2.60 |
| East | R2 | 2 | Dominant | 697 | 704 | 0.00 | 0.000 | No | No | - | 1.01 | 4.30 | 124.7 | 2.60 |
| East: WB Winneconne <br> Model Calibration Factor (HCM 6): 1.00 <br> Entry/Circ Flow Adj (HCM 6): None |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| South | L2 | 1 | Subdom. | 1028 | 1039 | 0.00 | 0.000 | No | No | - | 1.01 | 4.60 | 134.6 | 2.60 |
| West | T1 | 1 | Subdom. | 1028 | 1039 | 0.00 | 0.000 | No | No | - | 1.01 | 4.60 | 134.6 | 2.60 |
| West | T1 | 2 | Dominant | 1028 | 1039 | 0.00 | 0.000 | No | No | - | 1.01 | 4.30 | 125.7 | 2.60 |
| North | R2 | 2 | Dominant | 1028 | 1039 | 0.00 | 0.000 | No | No | - | 1.01 | 4.30 | 125.7 | 2.60 |
| North: SB Commercial <br> Model Calibration Factor (HCM 6): 1.00 <br> Entry/Circ Flow Adj (HCM 6): None |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| East | L2 | 1 | Subdom. | 630 | 637 | 0.00 | 0.000 | No | No | - | 1.01 | 4.60 | 142.5 | 2.60 |
| South | T1 | 1 | Subdom. | 630 | 637 | 0.00 | 0.000 | No | No | - | 1.01 | 4.60 | 142.5 | 2.60 |
| West | R2 | 2 | Dominant | 630 | 637 | 0.00 | 0.000 | No | No | - | 1.01 | 4.30 | 133.2 | 2.60 |
| West: EB Winneconne <br> Model Calibration Factor (HCM 6): 1.00 <br> Entry/Circ Flow Adj (HCM 6): None |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| North | L2 | 1 | Subdom. | 523 | 528 | 0.00 | 0.000 | No | No | - | 1.01 | 4.60 | 155.6 | 2.60 |
| East | T1 | 1 | Subdom. | 523 | 528 | 0.00 | 0.000 | No | No | - | 1.01 | 4.60 | 155.6 | 2.60 |
| East | T1 | 2 | Dominant | 523 | 528 | 0.00 | 0.000 | No | No | - | 1.01 | 4.30 | 145.4 | 2.60 |
| South | R2 | 2 | Dominant | 523 | 528 | 0.00 | 0.000 | No | No | - | 1.01 | 4.30 | 145.4 | 2.60 |

Roundabout Capacity Model: US HCM 6

| Circulating Lane Flow Rates |  |  |  |
| :---: | :---: | :---: | :---: |
| Circ. <br> Lane <br> No | Circulating Flow Rate |  |  |
|  | veh/h | pcu/h | Percent |
| South: NB Commercial |  |  |  |
| Lane 1 | 485 | 490 | 69.6 |
| Lane 2 | 212 | 214 | 30.4 |
| Approach | 697 | 704 |  |
| East: WB Winneconne |  |  |  |
| Lane 1 | 710 | 717 | 69.0 |
| Lane 2 | 319 | 322 | 31.0 |
| Approach | 1028 | 1039 |  |
| North: SB Commercial |  |  |  |
| Lane 1 | 399 | 403 | 63.2 |
| Lane 2 | 232 | 234 | 36.8 |
| Approach | 630 | 637 |  |
| West: EB Winneconne |  |  |  |
| Lane 1 | 523 | 528 | 100.0 |
| Lane 2 | 0 | 0 | 0.0 |
| Approach | 523 | 528 |  |

Roundabout Capacity Model: The US HCM 6 roundabout capacity model option is in use.
This model considers only the total circulating flow and not the flow rates in individual circulating lanes.
To model the effects of flow distribution in circulating lanes on the entry capacity results, you should use the SIDRA Standard roundabout capacity model.

| Gap Acceptance Cycle Parameters (Lanes) |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Opposed <br> Lane | Cycle Time sec | Blocked Time sec | Unblocked Time sec | Unblocked Time Ratio | Minimum Delay sec |
| South: NB Commercial |  |  |  |  |  |
| 1 | 12.23 | 5.82 | 6.42 | 0.525 | 5.0 |
| 2 | 11.53 | 5.11 | 6.42 | 0.556 | 4.7 |
| East: WB Winneconne |  |  |  |  |  |
| 1 | 12.35 | 7.59 | 4.77 | 0.386 | 6.8 |
| 2 | 11.32 | 6.55 | 4.77 | 0.421 | 6.2 |
| North: SB Commercial |  |  |  |  |  |
| 1 | 12.47 | 5.51 | 6.95 | 0.558 | 4.7 |
| 2 | 11.82 | 4.86 | 6.95 | 0.588 | 4.5 |
| West: EB Winneconne |  |  |  |  |  |
| 1 | 13.17 | 5.06 | 8.12 | 0.616 | 4.3 |
| 2 | 12.60 | 4.48 | 8.12 | 0.644 | 4.1 |

Roundabout Capacity Model: US HCM 6

| Gap Acceptance Cycle Parameters (Movements) |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| To Approach | Turn | Opsd | Cycle | Blocked | Unblocked | Unblocked | Minimum |
|  |  | Lane No | Time | Time | Time | Time Ratio | Delay |
|  |  | No |  |  |  |  |  |
|  |  |  | sec | sec | sec |  | sec |
| South: NB Commercial |  |  |  |  |  |  |  |
| West | L2 | 1 | 12.23 | 5.82 | 6.42 | 0.525 | 5.0 |
| North | T1 | 1 | 12.23 | 5.82 | 6.42 | 0.525 | 5.0 |
| North | T1 | 2 | 11.53 | 5.11 | 6.42 | 0.556 | 4.7 |


| East | R2 | 2 | 11.53 | 5.11 | 6.42 | 0.556 | 4.7 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| East: WB | Winneconne |  |  |  |  |  |  |
| South | L2 | 1 | 12.35 | 7.59 | 4.77 | 0.386 | 6.8 |
| West | T1 | 1 | 12.35 | 7.59 | 4.77 | 0.386 | 6.8 |
| West | T1 | 2 | 11.32 | 6.55 | 4.77 | 0.421 | 6.2 |
| North | R2 | 2 | 11.32 | 6.55 | 4.77 | 0.421 | 6.2 |
| North: | BB Commercial |  |  |  |  |  |  |
| East | L2 | 1 | 12.47 | 5.51 | 6.95 | 0.558 | 4.7 |
| South | T1 | 1 | 12.47 | 5.51 | 6.95 | 0.558 | 4.7 |
| West | R2 | 2 | 11.82 | 4.86 | 6.95 | 0.588 | 4.5 |
| West: EB Winneconne |  |  |  |  |  |  |  |
| North | L2 | 1 | 13.17 | 5.06 | 8.12 | 0.616 | 4.3 |
| East | T1 | 1 | 13.17 | 5.06 | 8.12 | 0.616 | 4.3 |
| East | T1 | 2 | 12.60 | 4.48 | 8.12 | 0.644 | 4.1 |
| South | R2 | 2 | 12.60 | 4.48 | 8.12 | 0.644 | 4.1 |

Roundabout Capacity Model: US HCM 6

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## SITE LAYOUT

$\forall$ Site: 1 [Commercial \& Winneconne 4-leg 2042 PM Peak (Site
Folder: 4-leg Alternative)]
Site Category: (None)
Roundabout

Layout pictures are schematic functional drawings reflecting input data. They are not design drawings.


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## INPUT VOLUMES

Vehicles and pedestrians per 60 minutes
© Site: 1 [Commercial \& Winneconne 4-leg 2042 PM Peak (Site
Folder: 4-leg Alternative)]

Site Category: (None)
Roundabout

Volume Display Method: Total and \%

|  | R2 | T1 | L2 |
| :--- | ---: | ---: | ---: |
| Tot | 465 | 404 | 15 |
| LV | $99 \%$ | $99 \%$ | $99 \%$ |
| HV | $1 \%$ | $1 \%$ | $1 \%$ |



|  | All MCs | Light Vehicles (LV) | Heavy Vehicles (HV) |
| :--- | :---: | :---: | :---: |
| S: NB Commercial | 651 | 644 | 7 |
| E: WB Winneconne | 424 | 420 | 4 |
| N: SB Commercial | 884 | 875 | 9 |
| W: EB Winneconne | 882 | 873 | 9 |
| Total | 2841 | 2813 | 28 |

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## LANE SUMMARY

## $\nabla$ Site: 1 [Commercial \& Winneconne 4-leg 2042 PM Peak (Site Folder: 4-leg Alternative)]

Site Category: (None)
Roundabout

| Lane Use and Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | DEMAND FLOWS |  | Cap. <br> veh/h | Deg. Satn v/c | Lane Util. \% | Aver. Delay sec | Level of Service | 95\% BACK OF QUEUE |  | Lane Config | Lane Length ft | Cap. Adj. \% | Prob. Block. $\qquad$ |
| South: NB Commercial |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane 1 | 343 | 1.0 | 719 | 0.477 | 100 | 11.9 | LOS B | 2.8 | 71.7 | Full | 1600 | 0.0 | 0.0 |
| Lane $2^{\text {d }}$ | 364 | 1.0 | 763 | 0.477 | 100 | 11.3 | LOS B | 2.8 | 69.4 | Full | 1600 | 0.0 | 0.0 |
| Approach | 708 | 1.0 |  | 0.477 |  | 11.6 | LOS B | 2.8 | 71.7 |  |  |  |  |
| East: WB Winneconne |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane 1 | 220 | 1.0 | 529 | 0.417 | 100 | 13.7 | LOS B | 1.9 | 49.1 | Full | 1600 | 0.0 | 0.0 |
| Lane $2^{\text {d }}$ | 240 | 1.0 | 577 | 0.417 | 100 | 12.7 | LOS B | 1.9 | 47.6 | Full | 1600 | 0.0 | 0.0 |
| Approach | 461 | 1.0 |  | 0.417 |  | 13.2 | LOS B | 1.9 | 49.1 |  |  |  |  |
| North: SB Commercial |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane 1 | 455 | 1.0 | 765 | 0.595 | $95^{5}$ | 14.4 | LOS B | 4.8 | 120.0 | Full | 1600 | 0.0 | 0.0 |
| Lane $2^{\text {d }}$ | 505 | 1.0 | 807 | 0.626 | 100 | 14.8 | LOS B | 5.3 | 133.3 | Full | 1600 | 0.0 | 0.0 |
| Approach | 961 | 1.0 |  | 0.626 |  | 14.6 | LOS B | 5.3 | 133.3 |  |  |  |  |
| West: EB Winneconne |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane 1 | 469 | 1.0 | 845 | 0.555 | 100 | 12.2 | LOS B | 4.4 | 110.0 | Full | 1600 | 0.0 | 0.0 |
| Lane $2^{\text {d }}$ | 490 | 1.0 | 883 | 0.555 | 100 | 11.8 | LOS B | 4.2 | 106.8 | Full | 1600 | 0.0 | 0.0 |
| Approach | 959 | 1.0 |  | 0.555 |  | 12.0 | LOS B | 4.4 | 110.0 |  |  |  |  |
| Intersection | 3088 | 1.0 |  | 0.626 |  | 12.9 | LOS B | 5.3 | 133.3 |  |  |  |  |

Site Level of Service (LOS) Method: Delay \& v/c (HCM 6). Site LOS Method is specified in the Parameter Settings dialog (Site tab).
Roundabout LOS Method: Same as Sign Control.
Lane LOS values are based on average delay and v/c ratio (degree of saturation) per lane.
LOS F will result if v/c > 1 irrespective of lane delay value (does not apply for approaches and intersection).
Intersection and Approach LOS values are based on average delay for all lanes ( $\mathrm{v} / \mathrm{c}$ not used as specified in HCM 6).
Roundabout Capacity Model: US HCM 6.
Delay Model: HCM Delay Formula (Geometric Delay is not included).
Queue Model: HCM Queue Formula.
Gap-Acceptance Capacity: Traditional M1.
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.
5 Lane under-utilisation found by the program
d Dominant lane on roundabout approach

Approach Lane Flows (veh/h)
South: NB Commercial

| Mov. <br> From S To Exit: | L2 W | T1 N | R2 E | Total | \%HV | Cap. veh/h | Deg. Satn v/c | Lane Util. \% | Prob. SL Ov. \% | $\begin{gathered} \text { Ov. } \\ \text { Lane } \\ \text { No. } \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane 1 | 178 | 165 | - | 343 | 1.0 | 719 | 0.477 | 100 | NA | NA |
| Lane 2 | - | 319 | 46 | 364 | 1.0 | 763 | 0.477 | 100 | NA | NA |
| Approach | 178 | 484 | 46 | 708 | 1.0 |  | 0.477 |  |  |  |


| East: WB Winneconne |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov. <br> From E To Exit: | L2 S | $\begin{aligned} & \text { T1 } \\ & \text { W } \end{aligned}$ | R2 N | Total | \%HV | Cap. veh/h | Deg. Satn v/c | Lane Util. \% | Prob. SL Ov. \% | Ov Lane No. |
| Lane 1 | 67 | 153 | - | 220 | 1.0 | 529 | 0.417 | 100 | NA | NA |
| Lane 2 | - | 232 | 9 | 240 | 1.0 | 577 | 0.417 | 100 | NA | NA |
| Approach | 67 | 385 | 9 | 461 | 1.0 |  | 0.417 |  |  |  |
| North: SB Commercial |  |  |  |  |  |  |  |  |  |  |
| Mov. From N To Exit: | L2 E | T1 S | R2 W | Total | \%HV | Cap. veh/h | Deg. Satn v/c | Lane Util. \% | Prob. SL Ov. \% | Ov. Lane No. |
| Lane 1 | 16 | 439 | - | 455 | 1.0 | 765 | 0.595 | $95^{5}$ | NA | NA |
| Lane 2 | - | - | 505 | 505 | 1.0 | 807 | 0.626 | 100 | NA | NA |
| Approach | 16 | 439 | 505 | 961 | 1.0 |  | 0.626 |  |  |  |
| West: EB Winneconne |  |  |  |  |  |  |  |  |  |  |
| Mov. <br> From W To Exit: | L2 N | T1 E | R2 S | Total | \%HV | Cap. veh/h | Deg. Satn v/c | Lane Util. \% | Prob. SL Ov. \% | Ov Lane No. |
| Lane 1 | 366 | 102 | - | 469 | 1.0 | 845 | 0.555 | 100 | NA | NA |
| Lane 2 | - | 212 | 278 | 490 | 1.0 | 883 | 0.555 | 100 | NA | NA |
| Approach | 366 | 314 | 278 | 959 | 1.0 |  | 0.555 |  |  |  |
| Total \%HV Deg.Satn (v/c) |  |  |  |  |  |  |  |  |  |  |
| Intersection | 3088 | 1.0 |  | 0.626 |  |  |  |  |  |  |

Lane flow rates given in this report are based on the arrival flow rates subject to upstream capacity constraint where applicable.
5 Lane under-utilisation found by the program

| Merge Analysis |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Exit Lane Number | Short Percent Opposing Lane Opng in Flow Rate Length Lane $\mathrm{ft} \quad \%$ veh/h pcu/h | Critical Gap sec | Follow-up Lane Headway Flow Rate sec veh/h | Capacity <br> veh/h | Deg. Satn v/c |  | Merge Delay sec |
| South Exit: NB Commercial Merge Type: Not Applied |  |  |  |  |  |  |  |
| Full Length Lane 1 <br> Full Length Lane 2 | Merge Analysis not applied. Merge Analysis not applied. |  |  |  |  |  |  |
| East Exit: WB Winneconne Merge Type: Not Applied |  |  |  |  |  |  |  |
| Full Length Lane 1 <br> Full Length Lane 2 | Merge Analysis not applied. Merge Analysis not applied. |  |  |  |  |  |  |
| North Exit: SB Commercial Merge Type: Not Applied |  |  |  |  |  |  |  |
| Full Length Lane 1 <br> Full Length Lane 2 | Merge Analysis not applied. <br> Merge Analysis not applied. |  |  |  |  |  |  |
| West Exit: EB Winneconne Merge Type: Not Applied |  |  |  |  |  |  |  |
| Full Length Lane 1 <br> Full Length Lane 2 | Merge Analysis not applied. <br> Merge Analysis not applied. |  |  |  |  |  |  |

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## SITE LAYOUT

$\nabla$ Site: 1 [Commercial \& Winneconne 5-leg 2022 AM Peak (Site
Folder: 5-leg Alternative)]
Site Category: (None)
Roundabout

Layout pictures are schematic functional drawings reflecting input data. They are not design drawings.


## INPUT VOLUMES

Vehicles and pedestrians per 60 minutes
B Site: 1 [Commercial \& Winneconne 5-leg 2022 AM Peak (Site
Folder: 5-leg Alternative)]

Site Category: (None)
Roundabout

Volume Display Method: Total and \%


|  | All MCs | Light Vehicles (LV) | Heavy Vehicles (HV) |
| :--- | :---: | :---: | :---: |
| S: NB Commercial | 583 | 566 | 17 |
| E: WB Winneconne | 359 | 355 | 4 |
| N: SB Commercial | 537 | 516 | 21 |
| NW: SB Church | 80 | 79 | 1 |
| W: EB Winneconne | 768 | 753 | 15 |
| Total | 2327 | 2268 | 59 |

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## LANE SUMMARY

Site: 1 [Commercial \& Winneconne 5-leg 2022 AM Peak (Site Folder: 5-leg Alternative)]

Site Category: (None)
Roundabout

| Lane Use and Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | $\begin{aligned} & \text { ND } \\ & \text { VS } \\ & \text { HV ] } \\ & \% \end{aligned}$ | Cap. <br> veh/h | Deg. Satn v/c | Lane Util. $\qquad$ \% | Aver. Delay <br> sec | Level of Service | $\begin{array}{r} 95 \% \\ \text { Q } \\ \text { [ Veh } \end{array}$ | $\begin{gathered} \mathrm{K} \text { OF } \\ \mathrm{JE} \\ \text { Dist ] } \\ \mathrm{ft} \end{gathered}$ | Lane Config | Lane Length ft | Cap. Adj. <br> \% | Prob. Block. <br> \% |
| South: NB Commercial |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane 1 | 341 | 3.0 | 703 | 0.485 | 100 | 12.3 | LOS B | 2.9 | 73.3 | Full | 1600 | 0.0 | 0.0 |
| Lane $2^{\text {d }}$ | 362 | 3.0 | 746 | 0.485 | 100 | 11.7 | LOS B | 2.8 | 71.1 | Full | 1600 | 0.0 | 0.0 |
| Approach | 702 | 3.0 |  | 0.485 |  | 12.0 | LOS B | 2.9 | 73.3 |  |  |  |  |
| East: WB Winneconne |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane 1 | 207 | 1.0 | 513 | 0.403 | 100 | 13.7 | LOS B | 1.8 | 46.0 | Full | 1600 | 0.0 | 0.0 |
| Lane $2^{\text {d }}$ | 226 | 1.0 | 561 | 0.403 | 100 | 12.7 | LOS B | 1.8 | 44.6 | Full | 1600 | 0.0 | 0.0 |
| Approach | 433 | 1.0 |  | 0.403 |  | 13.2 | LOS B | 1.8 | 46.0 |  |  |  |  |
| North: SB Commercial |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane 1 | 313 | 4.0 | 653 | 0.479 | 100 | 12.9 | LOS B | 2.7 | 69.1 | Full | 1600 | 0.0 | 0.0 |
| Lane ${ }^{\text {d }}$ | 334 | 4.0 | 697 | 0.479 | 100 | 12.2 | LOS B | 2.6 | 67.1 | Full | 1600 | 0.0 | 0.0 |
| Approach | 647 | 4.0 |  | 0.479 |  | 12.5 | LOS B | 2.7 | 69.1 |  |  |  |  |
| NorthWest: SB Church |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane $1^{\text {d }}$ | 96 | 1.0 | 356 | 0.271 | 100 | 15.2 | LOS C | 1.0 | 24.9 | Full | 1600 | 0.0 | 0.0 |
| Approach | 96 | 1.0 |  | 0.271 |  | 15.2 | LOS C | 1.0 | 24.9 |  |  |  |  |
| West: EB Winneconne |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane 1 | 455 | 2.0 | 927 | 0.490 | 100 | 10.0 | LOS B | 3.3 | 84.0 | Full | 1600 | 0.0 | 0.0 |
| Lane $2^{\text {d }}$ | 471 | 2.0 | 960 | 0.490 | 100 | 9.8 | LOSA | 3.2 | 80.2 | Full | 1600 | 0.0 | 0.0 |
| Approach | 925 | 2.0 |  | 0.490 |  | 9.9 | LOS A | 3.3 | 84.0 |  |  |  |  |
| Intersection | 2804 | 2.5 |  | 0.490 |  | 11.7 | LOS B | 3.3 | 84.0 |  |  |  |  |

Site Level of Service (LOS) Method: Delay \& v/c (HCM 6). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Roundabout LOS Method: Same as Sign Control.
Lane LOS values are based on average delay and v/c ratio (degree of saturation) per lane.
LOS $F$ will result if $v / c>1$ irrespective of lane delay value (does not apply for approaches and intersection).
Intersection and Approach LOS values are based on average delay for all lanes (v/c not used as specified in HCM 6).
Roundabout Capacity Model: US HCM 6.
Delay Model: HCM Delay Formula (Geometric Delay is not included).
Queue Model: HCM Queue Formula.
Gap-Acceptance Capacity: Traditional M1.
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.
d Dominant lane on roundabout approach

Approach Lane Flows (veh/h)
South: NB Commercial

| Mov. | L2 | L1 | T1 | R2 | Total | \%HV |  | Deg. | Lane | Prob. | Ov. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| From S | W | NW | N | E |  |  | Cap. veh/h | Satn v/c | Util. | SL Ov. | Lane No. |


| Lane 1 | 284 | 5 | 52 | - | 341 | 3.0 | 703 | 0.485 | 100 | NA | NA |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane 2 | - | - | 328 | 34 | 362 | 3.0 | 746 | 0.485 | 100 | NA | NA |
| Approach | 284 | 5 | 380 | 34 | 702 | 3.0 |  | 0.485 |  |  |  |
| East: WB Winneconne |  |  |  |  |  |  |  |  |  |  |  |
| Mov. <br> From E <br> To Exit: | L2 S | T1 W | R1 NW | R2 N | Total | \%HV | Cap. veh/h | Deg. Satn v/c | Lane Util. \% | Prob SL Ov. \% | Ov Lane No. |
| Lane 1 | 49 | 157 | - | - | 207 | 1.0 | 513 | 0.403 | 100 | NA | NA |
| Lane 2 | - | 215 | 6 | 5 | 226 | 1.0 | 561 | 0.403 | 100 | NA | NA |
| Approach | 49 | 372 | 6 | 5 | 433 | 1.0 |  | 0.403 |  |  |  |
| North: SB Commercial |  |  |  |  |  |  |  |  |  |  |  |
| Mov. From N To Exit: | L2 E | T1 S | R2 W | R3 <br> NW | Total | \%HV | Cap. veh/h | Deg. <br> Satn <br> v/c | Lane Util. \% | $\begin{aligned} & \text { Prob. } \\ & \text { SL Ov. } \\ & \% \end{aligned}$ | $\begin{gathered} \text { Ov. } \\ \text { Lane } \\ \text { No. } \end{gathered}$ |
| Lane 1 | 2 | 311 | - | - | 313 | 4.0 | 653 | 0.479 | 100 | NA | NA |
| Lane 2 | - | 15 | 314 | 5 | 334 | 4.0 | 697 | 0.479 | 100 | NA | NA |
| Approach | 2 | 325 | 314 | 5 | 647 | 4.0 |  | 0.479 |  |  |  |
| NorthWest: SB Church |  |  |  |  |  |  |  |  |  |  |  |
| Mov. <br> From NW To Exit: | L3 N | L1 E | R1 S | R3 W | Total | \%HV | Cap. veh/h | Deg. Satn v/c | Lane Util. \% | Prob. SL Ov. \% | Ov Lane No. |
| Lane 1 | 1 | 12 | 12 | 71 | 96 | 1.0 | 356 | 0.271 | 100 | NA | NA |
| Approach | 1 | 12 | 12 | 71 | 96 | 1.0 |  | 0.271 |  |  |  |
| West: EB Winneconne |  |  |  |  |  |  |  |  |  |  |  |
| Mov. <br> From W To Exit: | L3 NW | L2 N | T1 E | R2 S | Total | \%HV | Cap. veh/h | Deg. Satn v/c | Lane Util. \% | Prob. SL Ov. \% | Ov Lane No. |
| Lane 1 | 47 | 328 | 80 | - | 455 | 2.0 | 927 | 0.490 | 100 | NA | NA |
| Lane 2 | - | - | 224 | 247 | 471 | 2.0 | 960 | 0.490 | 100 | NA | NA |
| Approach | 47 | 328 | 304 | 247 | 925 | 2.0 |  | 0.490 |  |  |  |
| Total \%HV Deg.Satn (v/c) |  |  |  |  |  |  |  |  |  |  |  |
| Intersection | 2804 | 2.5 |  | 0.490 |  |  |  |  |  |  |  |

Lane flow rates given in this report are based on the arrival flow rates subject to upstream capacity constraint where applicable.

| Merge Analysis |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{array}{r} \text { Exit } \\ \text { Lane } \\ \text { Number } \end{array}$ | Short Percent Opposing Lane Opng in Flow Rate Length Lane $\mathrm{ft} \quad \%$ veh/h pcu/h | Critical Gap sec | Follow-up Headway sec | Lane Flow Rate veh/h | pacity <br> veh/h | Deg. Satn v/c |  | Merge Delay <br> sec |
| South Exit: NB Commercial Merge Type: Not Applied |  |  |  |  |  |  |  |  |
| Full Length Lane 1 <br> Full Length Lane 2 | Merge Analysis not applied. <br> Merge Analysis not applied. |  |  |  |  |  |  |  |
| East Exit: WB Winneconne Merge Type: Not Applied |  |  |  |  |  |  |  |  |
| Full Length Lane 1 <br> Full Length Lane 2 | Merge Analysis not applied. Merge Analysis not applied. |  |  |  |  |  |  |  |
| North Exit: SB Commercial Merge Type: Not Applied |  |  |  |  |  |  |  |  |


| Full Length Lane | 1 | Merge Analysis not applied. |
| :--- | ---: | :--- |
| Full Length Lane | 2 | Merge Analysis not applied. |
| NorthWest Exit: SB Church  <br> Merge Type: Not Applied  <br> Full Length Lane 1 <br> West Exit: EB Winneconne Analysis not applied.  <br> Merge Type: Not Applied  <br> Full Length Lane 1 |  |  |
| Full Length Lane | 2 | Merge Analysis not applied. |

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## ROUNDABOUT ANALYSIS

$\forall$ Site: 1 [Commercial \& Winneconne 5-leg 2022 AM Peak (Site Folder: 5-leg Alternative)]

Site Category: (None)
Roundabout

| Roundabout Basic Parameters |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Location | Name | Central Island Diam | Circ Width | Insc Diam | Entry Radius | Entry Angle | $\begin{aligned} & \text { Circ } \\ & \text { Lanes } \end{aligned}$ | Entry Lanes | Av.Entry Lane Width | App. Dist | Prop Queued Upstr Signal | Extra Bunching |
|  |  | ft | ft | ft | ft |  |  |  | ft | ft |  | \% |
| South | NB | $120.00{ }^{*}$ | $30.00{ }^{*}$ | $180.0{ }^{*}$ | $85.0{ }^{*}$ | $20.0{ }^{*}$ | 2 | 2 | $13.00{ }^{*}$ | 1600.0 | $N A^{5}$ | 0.0 |
| East | Commercial WB | $120.00{ }^{*}$ | $30.00{ }^{*}$ | $180.0{ }^{*}$ | $85.0{ }^{*}$ | $20.0{ }^{*}$ | 2 | 2 | $13.00{ }^{*}$ | 1600.0 | $N A^{5}$ | 0.0 |
| North | Winneconne SB <br> Commercial | $120.00{ }^{*}$ | 30.00 * | $180.0{ }^{*}$ | $85.0{ }^{*}$ | 20.0 * | 2 | 2 | $13.00{ }^{*}$ | 1600.0 | $N A^{5}$ | 0.0 |
| NorthWes <br> t | SB Church | 120.00 * | 30.00 * | $180.0{ }^{*}$ | 85.0 * | 20.0 * | 2 | 1 | $13.00{ }^{*}$ | 1600.0 | $N A^{5}$ | 0.0 |
| West | EB <br> Winneconne | 120.00 * | 30.00 * | $180.0{ }^{*}$ | 85.0 * | 20.0 * | 2 | 2 | $13.00{ }^{*}$ | 1600.0 | $N A^{5}$ | 0.0 |

## Roundabout Capacity Model: US HCM 6

5 Not Applicable (single Site analysis or unconnected Site in Network analysis).

* These parameters do not affect estimated capacity values in the HCM 6 Capacity Model.

| Roundabout Entry and Circulating / Exiting Stream Parameters |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { To Turn } \\ & \text { Approach } \end{aligned}$ | Lane <br> No | Lane Type | Opng Flow veh/h | Opng Flow pcu/h | InBunch B Hdwy sec | Prop. | Cap Const Effect | Priority Sharing | $\begin{gathered} \text { OD } \\ \text { Factor } \end{gathered}$ | HVE for Entry | Critica [ Hdwy <br> sec | Gap Dist ] ft | Follow- <br> up <br> Hdwy <br> sec |
| South: NB Commercial Model Calibration Factor (HCM 6): 1.00 Entry/Circ Flow Adj (HCM 6): None |  |  |  |  |  |  |  |  |  |  |  |  |  |
| West L2 | 1 | Subdom. | 694 | 708 | 0.00 | 0.000 | No | No | - | 1.03 | 4.60 | 141.5 | 2.60 |
| NorthWes L1 | 1 | Subdom. | 694 | 708 | 0.00 | 0.000 | No | No | - | 1.03 | 4.60 | 141.5 | 2.60 |
| North T1 | 1 | Subdom. | 694 | 708 | 0.00 | 0.000 | No | No | - | 1.03 | 4.60 | 141.5 | 2.60 |
| North T1 | 2 | Dominant | 694 | 708 | 0.00 | 0.000 | No | No | - | 1.03 | 4.30 | 132.2 | 2.60 |
| East R2 | 2 | Dominant | 694 | 708 | 0.00 | 0.000 | No | No | - | 1.03 | 4.30 | 132.2 | 2.60 |
| East: WB Winneconne <br> Model Calibration Factor (HCM 6): 1.00 <br> Entry/Circ Flow Adj (HCM 6): None |  |  |  |  |  |  |  |  |  |  |  |  |  |
| South L2 | 1 | Subdom. | 1045 | 1072 | 0.00 | 0.000 | No | No | - | 1.01 | 4.60 | 136.8 | 2.60 |
| West T1 | 1 | Subdom. | 1045 | 1072 | 0.00 | 0.000 | No | No | - | 1.01 | 4.60 | 136.8 | 2.60 |
| West T1 | 2 | Dominant | 1045 | 1072 | 0.00 | 0.000 | No | No | - | 1.01 | 4.30 | 127.8 | 2.60 |
| NorthWes R1 <br> t | 2 | Dominant | 1045 | 1072 | 0.00 | 0.000 | No | No | - | 1.01 | 4.30 | 127.8 | 2.60 |
| North R2 | 2 | Dominant | 1045 | 1072 | 0.00 | 0.000 | No | No | - | 1.01 | 4.30 | 127.8 | 2.60 |
| North: SB Commercial <br> Model Calibration Factor (HCM 6): 1.00 <br> Entry/Circ Flow Adj (HCM 6): None |  |  |  |  |  |  |  |  |  |  |  |  |  |
| East L2 | 1 | Subdom. | 764 | 778 | 0.00 | 0.000 | No | No | - | 1.04 | 4.60 | 145.1 | 2.60 |
| South T1 | 1 | Subdom. | 764 | 778 | 0.00 | 0.000 | No | No | - | 1.04 | 4.60 | 145.1 | 2.60 |
| South T1 | 2 | Dominant | 764 | 778 | 0.00 | 0.000 | No | No | - | 1.04 | 4.30 | 135.6 | 2.60 |
| West R2 | 2 | Dominant | 764 | 778 | 0.00 | 0.000 | No | No | - | 1.04 | 4.30 | 135.6 | 2.60 |
| NorthWes R3 | 2 | Dominant | 764 | 778 | 0.00 | 0.000 | No | No | - | 1.04 | 4.30 | 135.6 | 2.60 |


| NorthWest: SB Church <br> Model Calibration Factor (HCM 6): 1.00 <br> Entry/Circ Flow Adj (HCM 6): None |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| North | L3 | 1 | Dominant | 1348 | 1387 | 0.00 | 0.000 | No | No | - | 1.01 | 4.80 | 160.7 | 2.60 |
| East | L1 | 1 | Dominant | 1348 | 1387 | 0.00 | 0.000 | No | No | - | 1.01 | 4.80 | 160.7 | 2.60 |
| South | R1 | 1 | Dominant | 1348 | 1387 | 0.00 | 0.000 | No | No | - | 1.01 | 4.80 | 160.7 | 2.60 |
| West | R3 | 1 | Dominant | 1348 | 1387 | 0.00 | 0.000 | No | No | - | 1.01 | 4.80 | 160.7 | 2.60 |
| West: EB Winneconne <br> Model Calibration Factor (HCM 6): 1.00 <br> Entry/Circ Flow Adj (HCM 6): None |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| NorthV | L3 | 1 | Subdom. | 402 | 416 | 0.00 | 0.000 | No | No | - | 1.02 | 4.60 | 166.6 | 2.60 |
| North | L2 | 1 | Subdom. | 402 | 416 | 0.00 | 0.000 | No | No | - | 1.02 | 4.60 | 166.6 | 2.60 |
| East | T1 | 1 | Subdom. | 402 | 416 | 0.00 | 0.000 | No | No | - | 1.02 | 4.60 | 166.6 | 2.60 |
| East | T1 | 2 | Dominant | 402 | 416 | 0.00 | 0.000 | No | No | - | 1.02 | 4.30 | 155.7 | 2.60 |
| South | R2 | 2 | Dominant | 402 | 416 | 0.00 | 0.000 | No | No | - | 1.02 | 4.30 | 155.7 | 2.60 |

Roundabout Capacity Model: US HCM 6

## Circulating Lane Flow Rates

| Circ. <br> Lane <br> No | Circulating Flow Rate |  |  |
| :--- | ---: | ---: | ---: |
|  | veh/h | pcu/h | Percent |
| South: NB Commercial |  |  |  |
| Lane 1 | 470 | 480 | 67.8 |
| Lane 2 | 224 | 228 | 32.2 |
| Approach | 694 | 708 |  |
| East: WB Winneconne |  |  |  |
| Lane 1 | 717 | 734 | 68.5 |
| Lane 2 | 328 | 338 | 31.5 |
| Approach | 1045 | 1072 |  |
| North: SB Commercial |  |  |  |
| Lane 1 | 207 | 209 | 26.8 |
| Lane 2 | 557 | 569 | 73.2 |
| Approach | 764 | 778 |  |
| NorthWest: SB Church |  |  |  |
| Lane 1 | 804 | 827 | 59.6 |
| Lane 2 | 544 | 560 | 40.4 |
| Approach | 1348 | 1387 |  |
| West: EB Winneconne |  |  |  |
| Lane 1 | 388 | 15 | 401 |
| Lane 2 | 402 | 416 | 96.3 |
| Approach |  |  | 3.7 |

Roundabout Capacity Model: The US HCM 6 roundabout capacity model option is in use.
This model considers only the total circulating flow and not the flow rates in individual circulating lanes.
To model the effects of flow distribution in circulating lanes on the entry capacity results, you should use the SIDRA Standard roundabout capacity model.

Gap Acceptance Cycle Parameters (Lanes)

| Opposed | Cycle | Blocked | Unblocked | Unblocked | Minimum <br> Lime |
| :--- | :---: | ---: | :---: | ---: | :--- |
| Time | sec | Time | Time | sec | sime Ratio | | Delay |
| ---: |
| sec |


| South: NB Commercial |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 12.22 | 5.83 | 6.39 | 0.523 | 5.1 |
| 2 | 11.52 | 5.13 | 6.39 | 0.555 | 4.8 |
| East: WB Winneconne |  |  |  |  |  |
| 1 | 12.45 | 7.79 | 4.66 | 0.374 | 7.0 |
| 2 | 11.38 | 6.72 | 4.66 | 0.409 | 6.4 |
| North: SB Commercial |  |  |  |  |  |
| 1 | 12.10 | 6.17 | 5.93 | 0.490 | 5.5 |
| 2 | 11.33 | 5.40 | 5.93 | 0.523 | 5.2 |
| NorthWest: SB Church |  |  |  |  |  |
| 1 | 15.00 | 11.10 | 3.90 | 0.260 | 10.1 |
| West: EB Winneconne |  |  |  |  |  |
| 1 | 14.57 | 4.62 | 9.95 | 0.683 | 3.9 |
| 2 | 14.07 | 4.12 | 9.95 | 0.707 | 3.8 |

Roundabout Capacity Model: US HCM 6

| Gap Acceptance Cycle Parameters (Movements) |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| To Approach |  | Opsd Lane No | Cycle Time | Blocked Time | Unblocked Time | Unblocked Time Ratio | Minimum Delay |
|  |  |  | sec | sec | sec |  | sec |
| South: NB Commercial |  |  |  |  |  |  |  |
| West L | L2 | 1 | 12.22 | 5.83 | 6.39 | 0.523 | 5.1 |
| NorthWes ${ }_{\text {L }}$ |  | 1 | 12.22 | 5.83 | 6.39 | 0.523 | 5.1 |
| t |  |  |  |  |  |  |  |
| North T1 | T1 | 1 | 12.22 | 5.83 | 6.39 | 0.523 | 5.1 |
| North T1 | T1 | 2 | 11.52 | 5.13 | 6.39 | 0.555 | 4.8 |
| East P | R2 | 2 | 11.52 | 5.13 | 6.39 | 0.555 | 4.8 |
| East: WB Winneconne |  |  |  |  |  |  |  |
| South L | L2 | 1 | 12.45 | 7.79 | 4.66 | 0.374 | 7.0 |
| West T1 | T1 | 1 | 12.45 | 7.79 | 4.66 | 0.374 | 7.0 |
| West Ti | T1 | 2 | 11.38 | 6.72 | 4.66 | 0.409 | 6.4 |
| NorthWes ${ }_{\text {R }}$ |  | 2 | 11.38 | 6.72 | 4.66 | 0.409 | 6.4 |
| t |  |  |  |  |  |  |  |
| North | R2 | 2 | 11.38 | 6.72 | 4.66 | 0.409 | 6.4 |
| North: SB Commercial |  |  |  |  |  |  |  |
| East L | L2 | 1 | 12.10 | 6.17 | 5.93 | 0.490 | 5.5 |
| South T1 | T1 | 1 | 12.10 | 6.17 | 5.93 | 0.490 | 5.5 |
| South T1 | T1 | 2 | 11.33 | 5.40 | 5.93 | 0.523 | 5.2 |
| West $\quad$ R | R2 | 2 | 11.33 | 5.40 | 5.93 | 0.523 | 5.2 |
| NorthWes <br> t |  | 2 | 11.33 | 5.40 | 5.93 | 0.523 | 5.2 |
| NorthWest: SB Church |  |  |  |  |  |  |  |
| North L3 | L3 | 1 | 15.00 | 11.10 | 3.90 | 0.260 | 10.1 |
| East | L1 | 1 | 15.00 | 11.10 | 3.90 | 0.260 | 10.1 |
| South R | R1 | 1 | 15.00 | 11.10 | 3.90 | 0.260 | 10.1 |
| West R | R3 | 1 | 15.00 | 11.10 | 3.90 | 0.260 | 10.1 |
| West: EB Winneconne |  |  |  |  |  |  |  |
| NorthWes <br> t |  | 1 | 14.57 | 4.62 | 9.95 | 0.683 | 3.9 |
| North L | L2 | 1 | 14.57 | 4.62 | 9.95 | 0.683 | 3.9 |
| East T1 | T1 | 1 | 14.57 | 4.62 | 9.95 | 0.683 | 3.9 |
| East T1 | T1 | 2 | 14.07 | 4.12 | 9.95 | 0.707 | 3.8 |
| South R | R2 | 2 | 14.07 | 4.12 | 9.95 | 0.707 | 3.8 |

Roundabout Capacity Model: US HCM 6

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## SITE LAYOUT

$\nabla$ Site: 1 [Commercial \& Winneconne 5-leg 2022 PM Peak (Site
Folder: 5-leg Alternative)]
Site Category: (None)
Roundabout

Layout pictures are schematic functional drawings reflecting input data. They are not design drawings.


## INPUT VOLUMES

Vehicles and pedestrians per 60 minutes
$\nabla$ Site: 1 [Commercial \& Winneconne 5-leg 2022 PM Peak (Site Folder: 5-leg Alternative)]

Site Category: (None)
Roundabout

Volume Display Method: Total and \%


|  | All MCs | Light Vehicles (LV) | Heavy Vehicles (HV) |
| :--- | :---: | :---: | :---: |
| S: NB Commercial | 558 | 552 | 6 |
| E: WB Winneconne | 363 | 359 | 4 |
| N: SB Commercial | 756 | 748 | 8 |
| NW: SB Church | 57 | 56 | 1 |
| W: EB Winneconne | 807 | 799 | 8 |
| Total | 2541 | 2516 | 25 |

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## LANE SUMMARY

## $\nabla$ Site: 1 [Commercial \& Winneconne 5-leg 2022 PM Peak (Site Folder: 5-leg Alternative)]

Site Category: (None)
Roundabout

| Lane Use and Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | $\begin{aligned} & \text { ND } \\ & \text { NS } \\ & \text { HV ] } \\ & \% \end{aligned}$ | Cap. <br> veh/h | Deg. Satn v/c | Lane Util. \% | Aver. Delay sec | Level of Service | 95\% <br> [ Veh | $\begin{gathered} \mathrm{K} \text { OF } \\ \mathrm{JE} \\ \text { Dist ] } \\ \mathrm{ft} \end{gathered}$ | Lane Config | Lane Length ft | Cap. Adj. \% | Prob. Block. <br> \% |
| South: NB Commercial |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane 1 | 295 | 1.0 | 739 | 0.399 | 100 | 10.1 | LOS B | 2.0 | 51.3 | Full | 1600 | 0.0 | 0.0 |
| Lane $2^{\text {d }}$ | 312 | 1.0 | 782 | 0.399 | 100 | 9.6 | LOS A | 1.9 | 49.1 | Full | 1600 | 0.0 | 0.0 |
| Approach | 607 | 1.0 |  | 0.399 |  | 9.8 | LOS A | 2.0 | 51.3 |  |  |  |  |
| East: WB Winneconne |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane 1 | 189 | 1.0 | 567 | 0.334 | 100 | 11.2 | LOS B | 1.4 | 35.5 | Full | 1600 | 0.0 | 0.0 |
| Lane $2^{\text {d }}$ | 205 | 1.0 | 615 | 0.334 | 100 | 10.4 | LOS B | 1.4 | 34.1 | Full | 1600 | 0.0 | 0.0 |
| Approach | 395 | 1.0 |  | 0.334 |  | 10.8 | LOS B | 1.4 | 35.5 |  |  |  |  |
| North: SB Commercial |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane 1 | 389 | 1.0 | 779 | 0.500 | $95^{5}$ | 11.6 | LOS B | 3.3 | 82.2 | Full | 1600 | 0.0 | 0.0 |
| Lane $2^{\text {d }}$ | 433 | 1.0 | 820 | 0.527 | 100 | 11.8 | LOS B | 3.6 | 89.7 | Full | 1600 | 0.0 | 0.0 |
| Approach | 822 | 1.0 |  | 0.527 |  | 11.7 | LOS B | 3.6 | 89.7 |  |  |  |  |
| NorthWest: SB Church |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane $1^{\text {d }}$ | 62 | 1.0 | 369 | 0.168 | 100 | 12.6 | LOS B | 0.6 | 14.6 | Full | 1600 | 0.0 | 0.0 |
| Approach | 62 | 1.0 |  | 0.168 |  | 12.6 | LOS B | 0.6 | 14.6 |  |  |  |  |
| West: EB Winneconne |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane 1 | 430 | 1.0 | 894 | 0.481 | 100 | 10.1 | LOS B | 3.2 | 80.1 | Full | 1600 | 0.0 | 0.0 |
| Lane $2^{\text {d }}$ | 447 | 1.0 | 930 | 0.481 | 100 | 9.8 | LOS A | 3.0 | 76.7 | Full | 1600 | 0.0 | 0.0 |
| Approach | 877 | 1.0 |  | 0.481 |  | 10.0 | LOS A | 3.2 | 80.1 |  |  |  |  |
| Intersection | 2762 | 1.0 |  | 0.527 |  | 10.6 | LOS B | 3.6 | 89.7 |  |  |  |  |

Site Level of Service (LOS) Method: Delay \& v/c (HCM 6). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Roundabout LOS Method: Same as Sign Control.
Lane LOS values are based on average delay and v/c ratio (degree of saturation) per lane.
LOS $F$ will result if $\mathrm{v} / \mathrm{c}>1$ irrespective of lane delay value (does not apply for approaches and intersection).
Intersection and Approach LOS values are based on average delay for all lanes (v/c not used as specified in HCM 6).
Roundabout Capacity Model: US HCM 6.
Delay Model: HCM Delay Formula (Geometric Delay is not included).
Queue Model: HCM Queue Formula.
Gap-Acceptance Capacity: Traditional M1.
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.
5 Lane under-utilisation found by the program
d Dominant lane on roundabout approach

## Approach Lane Flows (veh/h)

South: NB Commercial

| Mov. | L2 | L1 | T1 | R2 | Total | \%HV |  | Deg. | Lane | Prob. | Ov. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| From S To Exit: | W | NW | N | E |  |  | Cap. veh/h | Satn v/c |  | $\begin{array}{r} \text { SL Ov. } \\ \% \end{array}$ | Lane No. |


| Lane 1 | 149 | 4 | 141 | - | 295 | 1.0 | 739 | 0.399 | 100 | NA | NA |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane 2 | - | - | 273 | 39 | 312 | 1.0 | 782 | 0.399 | 100 | NA | NA |
| Approach | 149 | 4 | 414 | 39 | 607 | 1.0 |  | 0.399 |  |  |  |
| East: WB Winneconne |  |  |  |  |  |  |  |  |  |  |  |
| Mov. <br> From E <br> To Exit: | L2 S | T1 W | R1 NW | R2 N | Total | \%HV | Cap. veh/h | Deg. Satn v/c | Lane Util. \% | Prob. SL Ov. \% | $\begin{gathered} \text { Ov. } \\ \text { Lane } \\ \text { No. } \end{gathered}$ |
| Lane 1 | 58 | 132 | - | - | 189 | 1.0 | 567 | 0.334 | 100 | NA | NA |
| Lane 2 | - | 189 | 9 | 8 | 205 | 1.0 | 615 | 0.334 | 100 | NA | NA |
| Approach | 58 | 321 | 9 | 8 | 395 | 1.0 |  | 0.334 |  |  |  |
| North: SB Commercial |  |  |  |  |  |  |  |  |  |  |  |
| Mov. <br> From N To Exit: | L2 E | T1 S | R2 W | R3 NW | Total | \%HV | Cap. veh/h | Deg. Satn v/c | Lane Util. \% | Prob. SL Ov. \% | Ov. Lane |
| Lane 1 | 13 | 376 | - | - | 389 | 1.0 | 779 | 0.500 | $95^{5}$ | NA | NA |
| Lane 2 | - | - | 422 | 11 | 433 | 1.0 | 820 | 0.527 | 100 | NA | NA |
| Approach | 13 | 376 | 422 | 11 | 822 | 1.0 |  | 0.527 |  |  |  |
| NorthWest: SB Church |  |  |  |  |  |  |  |  |  |  |  |
| Mov. <br> From NW <br> To Exit: | L3 N | L1 E | R1 S | R3 W | Total | \%HV | Cap. veh/h | Deg. Satn v/c | Lane Util. \% | Prob. SL Ov. \% | $\begin{gathered} \text { Ov. } \\ \text { Lane } \\ \text { No. } \end{gathered}$ |
| Lane 1 | 1 | 7 | 8 | 47 | 62 | 1.0 | 369 | 0.168 | 100 | NA | NA |
| Approach | 1 | 7 | 8 | 47 | 62 | 1.0 |  | 0.168 |  |  |  |
| West: EB Winneconne |  |  |  |  |  |  |  |  |  |  |  |
| Mov. <br> From W To Exit: | L3 NW | L2 N | T1 E | R2 S | Total | \%HV | Cap. veh/h | Deg. Satn v/c | Lane Util. \% | Prob. SL Ov. \% | $\begin{gathered} \text { Ov. } \\ \text { Lane } \\ \text { No. } \end{gathered}$ |
| Lane 1 | 71 | 314 | 45 | - | 430 | 1.0 | 894 | 0.481 | 100 | NA | NA |
| Lane 2 | - | - | 217 | 230 | 447 | 1.0 | 930 | 0.481 | 100 | NA | NA |
| Approach | 71 | 314 | 262 | 230 | 877 | 1.0 |  | 0.481 |  |  |  |
| Total \%HV Deg.Satn (v/c) |  |  |  |  |  |  |  |  |  |  |  |
| Intersection | 2762 | 1.0 |  | 0.527 |  |  |  |  |  |  |  |

Lane flow rates given in this report are based on the arrival flow rates subject to upstream capacity constraint where applicable.
5 Lane under-utilisation found by the program

| Merge Analysis |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{array}{r} \text { Exit } \\ \text { Lane } \\ \text { Number } \end{array}$ | Short Percent Opposing Lane Opng in Flow Rate Length Lane ft $\%$ veh/h pcu/h | Critical Gap sec | Follow-up Lane Headway Flow Rate sec veh/h | Capacity <br> veh/h | Deg. Min. Satn Delay v/c sec | Merge Delay <br> sec |
| South Exit: NB Commercial Merge Type: Not Applied |  |  |  |  |  |  |
| Full Length Lane 1 <br> Full Length Lane 2 | Merge Analysis not applied. Merge Analysis not applied. |  |  |  |  |  |
| East Exit: WB Winneconne Merge Type: Not Applied |  |  |  |  |  |  |
| Full Length Lane 1 <br> Full Length Lane 2 | Merge Analysis not applied. Merge Analysis not applied. |  |  |  |  |  |
| North Exit: SB Commercial |  |  |  |  |  |  |


| Merge Type: Not Applied |  |  |
| :--- | ---: | :--- |
| Full Length Lane | 1 | Merge Analysis not applied. |
| Full Length Lane | 2 | Merge Analysis not applied. |
| NorthWest Exit: SB Church |  |  |
| Merge Type: Not Applied |  |  |
| Full Length Lane | 1 | Merge Analysis not applied. |
| West Exit: EB Winneconne |  |  |
| Merge Type: Not Applied |  |  |
| Full Length Lane | 1 | Merge Analysis not applied. |
| Full Length Lane | 2 | Merge Analysis not applied. |

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## ROUNDABOUT ANALYSIS

## $\nabla$ Site: 1 [Commercial \& Winneconne 5-leg 2022 PM Peak (Site <br> Folder: 5-leg Alternative)]

Site Category: (None)
Roundabout

| Roundabout Basic Parameters |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Location | Name | Central Island Diam | Circ | Insc Diam | Entry Radius | Entry Angle | Circ Lanes | Entry Lanes | Av.Entry Lane Width | App. Dist | Prop Queued Upstr Signal | Extra Bunching |
|  |  | ft | ft | ft | ft |  |  |  | ft | ft |  | \% |
| South |  | $120.00{ }^{*}$ | 30.00 * | $180.0{ }^{*}$ | $85.0{ }^{*}$ | $20.0 *$ | 2 | 2 | $13.00{ }^{*}$ | 1600.0 | $N A^{5}$ | 0.0 |
|  |  | $120.00{ }^{*}$ | $30.00{ }^{*}$ | $180.0{ }^{*}$ | 85.0* | $20.0{ }^{*}$ | 2 | 2 | 13.00 * | 1600.0 | $N A^{5}$ | 0.0 |
| North | Winnec | $120.00{ }^{*}$ | 30.00 * | $180.0{ }^{*}$ | $85.0{ }^{*}$ | $20.0{ }^{*}$ | 2 | 2 | $13.00{ }^{*}$ | 1600.0 | $N A^{5}$ | 0.0 |
|  | Comm |  |  |  |  |  |  |  |  |  |  |  |
| NorthWestSB Church |  | $120.00{ }^{*}$ | 30.00 * | $180.0{ }^{*}$ | 85.0 * | 20.0 * | 2 | 1 | 13.0013.00 | 1600.0 | $N A^{5}$ | 0.0 |
| West | EB | $120.00{ }^{*}$ | $30.00{ }^{*}$ | $180.0{ }^{*}$ | $85.0{ }^{*}$ | $20.0{ }^{*}$ | 2 | 2 |  | 1600.0 | $N A^{5}$ | 0.0 |

Roundabout Capacity Model: US HCM 6
5 Not Applicable (single Site analysis or unconnected Site in Network analysis).

* These parameters do not affect estimated capacity values in the HCM 6 Capacity Model.

| Roundabout Entry and Circulating / Exiting Stream Parameters |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { To Turn } \\ & \text { Approach } \end{aligned}$ | Lane <br> No | Lane Type | Opng Flow veh/h | Opng Flow <br> pcu/h | InBunch Hdwy sec | $\begin{aligned} & \text { Prop. } \\ & \text { 3unched } \end{aligned}$ | Cap Const Effect | Priority Sharing | $\begin{gathered} \text { OD } \\ \text { Factor } \end{gathered}$ | HVE for Entry | Critica [ Hdwy sec | Gap Dist ] | Followup Hdwy sec |
| South: NB Commercial <br> Model Calibration Factor (HCM 6): 1.00 <br> Entry/Circ Flow Adj (HCM 6): None |  |  |  |  |  |  |  |  |  |  |  |  |  |
| West L2 | 1 | Subdom. | 667 | 674 | 0.00 | 0.000 | No | No | - | 1.01 | 4.60 | 138.6 | 2.60 |
| $\text { NorthWes }_{\text {L1 }}$ t | 1 | Subdom. | 667 | 674 | 0.00 | 0.000 | No | No | - | 1.01 | 4.60 | 138.6 | 2.60 |
| North T1 | 1 | Subdom. | 667 | 674 | 0.00 | 0.000 | No | No | - | 1.01 | 4.60 | 138.6 | 2.60 |
| North T1 | 2 | Dominant | 667 | 674 | 0.00 | 0.000 | No | No | - | 1.01 | 4.30 | 129.5 | 2.60 |
| East R2 | 2 | Dominant | 667 | 674 | 0.00 | 0.000 | No | No | - | 1.01 | 4.30 | 129.5 | 2.60 |
| East: WB Winneconne <br> Model Calibration Factor (HCM 6): 1.00 <br> Entry/Circ Flow Adj (HCM 6): None |  |  |  |  |  |  |  |  |  |  |  |  |  |
| South L2 | 1 | Subdom. | 953 | 963 | 0.00 | 0.000 | No | No | - | 1.01 | 4.60 | 141.3 | 2.60 |
| West T1 | 1 | Subdom. | 953 | 963 | 0.00 | 0.000 | No | No | - | 1.01 | 4.60 | 141.3 | 2.60 |
| West T1 | 2 | Dominant | 953 | 963 | 0.00 | 0.000 | No | No | - | 1.01 | 4.30 | 132.0 | 2.60 |
| NorthWes R1 <br> t | 2 | Dominant | 953 | 963 | 0.00 | 0.000 | No | No | - | 1.01 | 4.30 | 132.0 | 2.60 |
| North R2 | 2 | Dominant | 953 | 963 | 0.00 | 0.000 | No | No | - | 1.01 | 4.30 | 132.0 | 2.60 |
| North: SB Commercial <br> Model Calibration Factor (HCM 6): 1.00 <br> Entry/Circ Flow Adj (HCM 6): None |  |  |  |  |  |  |  |  |  |  |  |  |  |
| East L2 | 1 | Subdom. | 611 | 617 | 0.00 | 0.000 | No | No | - | 1.01 | 4.60 | 147.9 | 2.60 |
| South T1 | 1 | Subdom. | 611 | 617 | 0.00 | 0.000 | No | No | - | 1.01 | 4.60 | 147.9 | 2.60 |
| West R2 | 2 | Dominant | 611 | 617 | 0.00 | 0.000 | No | No | - | 1.01 | 4.30 | 138.1 | 2.60 |
| NorthWes R3 t | 2 | Dominant | 611 | 617 | 0.00 | 0.000 | No | No | - | 1.01 | 4.30 | 138.1 | 2.60 |
| NorthWest: SB Church |  |  |  |  |  |  |  |  |  |  |  |  |  |


| Model Calibration Factor (HCM 6): 1.00 Entry/Circ Flow Adj (HCM 6): None |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| North | L3 | 1 | Dominant | 1338 | 1351 | 0.00 | 0.000 | No | No | - | 1.01 | 4.80 | 163.7 | 2.60 |
| East | L1 | 1 | Dominant | 1338 | 1351 | 0.00 | 0.000 | No | No | - | 1.01 | 4.80 | 163.7 | 2.60 |
| South | R1 | 1 | Dominant | 1338 | 1351 | 0.00 | 0.000 | No | No | - | 1.01 | 4.80 | 163.7 | 2.60 |
| West | R3 | 1 | Dominant | 1338 | 1351 | 0.00 | 0.000 | No | No | - | 1.01 | 4.80 | 163.7 | 2.60 |
| West: EB Winneconne <br> Model Calibration Factor (HCM 6): 1.00 <br> Entry/Circ Flow Adj (HCM 6): None |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| NorthW <br> t | L3 | 1 | Subdom. | 462 | 467 | 0.00 | 0.000 | No | No | - | 1.01 | 4.60 | 166.2 | 2.60 |
| North | L2 | 1 | Subdom. | 462 | 467 | 0.00 | 0.000 | No | No | - | 1.01 | 4.60 | 166.2 | 2.60 |
| East | T1 | 1 | Subdom. | 462 | 467 | 0.00 | 0.000 | No | No | - | 1.01 | 4.60 | 166.2 | 2.60 |
| East | T1 | 2 | Dominant | 462 | 467 | 0.00 | 0.000 | No | No | - | 1.01 | 4.30 | 155.2 | 2.60 |
| South | R2 | 2 | Dominant | 462 | 467 | 0.00 | 0.000 | No | No | - | 1.01 | 4.30 | 155.2 | 2.60 |

Roundabout Capacity Model: US HCM 6

| Circulating Lane Flow Rates |  |  |  |
| :---: | :---: | :---: | :---: |
| Circ. <br> Lane <br> No | Circulating Flow Rate |  |  |
|  | veh/h | pcu/h | Percent |
| South: NB Commercial |  |  |  |
| Lane 1 | 451 | 455 | 67.5 |
| Lane 2 | 217 | 219 | 32.5 |
| Approach | 667 | 674 |  |
| East: WB Winneconne |  |  |  |
| Lane 1 | 681 | 687 | 71.4 |
| Lane 2 | 273 | 275 | 28.6 |
| Approach | 953 | 963 |  |
| North: SB Commercial |  |  |  |
| Lane 1 | 189 | 191 | 31.0 |
| Lane 2 | 422 | 426 | 69.0 |
| Approach | 611 | 617 |  |
| NorthWest: SB Church |  |  |  |
| Lane 1 | 727 | 735 | 54.4 |
| Lane 2 | 611 | 617 | 45.6 |
| Approach | 1338 | 1351 |  |
| West: EB Winneconne |  |  |  |
| Lane 1 | 462 | 467 | 100.0 |
| Lane 2 | 0 | 0 | 0.0 |
| Approach | 462 | 467 |  |

Roundabout Capacity Model: The US HCM 6 roundabout capacity model option is in use.
This model considers only the total circulating flow and not the flow rates in individual circulating lanes.
To model the effects of flow distribution in circulating lanes on the entry capacity results, you should use the SIDRA Standard roundabout capacity model.

| Gap Acceptance Cycle Parameters (Lanes) |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: |
| Opposed <br> Lane | Cycle <br> Time <br> sec | Blocked <br> Time <br> sec | Unblocked <br> Time <br> sec | Unblocked <br> Time Ratio | Minimum <br> Delay <br> sec |
| South: NB Commercial |  |  |  |  |  |
| 1 | 12.32 | 5.68 | 6.64 | 0.539 | 4.9 |


| 2 | 11.64 | 5.00 | 6.64 | 0.570 | 4.6 |
| :---: | :---: | :---: | :---: | :---: | :---: |
| East: WB Winneconne |  |  |  |  |  |
| 1 | 12.18 | 7.14 | 5.04 | 0.414 | 6.3 |
| 2 | 11.24 | 6.20 | 5.04 | 0.448 | 5.9 |
| North: SB Commercial |  |  |  |  |  |
| 1 | 12.56 | 5.43 | 7.13 | 0.568 | 4.6 |
| 2 | 11.93 | 4.79 | 7.13 | 0.598 | 4.4 |
| NorthWest: SB Church |  |  |  |  |  |
| 1 | 14.74 | 10.78 | 3.96 | 0.269 | 9.8 |
| West: EB Winneconne |  |  |  |  |  |
| 1 | 13.83 | 4.81 | 9.02 | 0.652 | 4.0 |
| 2 | 13.30 | 4.28 | 9.02 | 0.678 | 3.9 |

Roundabout Capacity Model: US HCM 6

| Gap Acceptance Cycle Parameters (Movements) |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| To Approach | Turn | Opsd | Cycle | Blocked | Unblocked | Unblocked | Minimum |
|  |  | Lane | Time | Time | Time | Time Ratio | Delay |
|  |  |  | sec | sec | sec |  | sec |
| South: NB Commercial |  |  |  |  |  |  |  |
| West <br> NorthWes <br> t |  | 1 | 12.32 | 5.68 | 6.64 | 0.539 | 4.9 |
|  |  | 1 | 12.32 | 5.68 | 6.64 | 0.539 | 4.9 |
|  |  |  |  |  |  |  |  |
| North <br> North <br> East | T1 | 1 | 12.32 | 5.68 | 6.64 | 0.539 | 4.9 |
|  | T1 | 2 | 11.64 | 5.00 | 6.64 | 0.570 | 4.6 |
|  | R2 | 2 | 11.64 | 5.00 | 6.64 | 0.570 | 4.6 |
| East: WB Winneconne |  |  |  |  |  |  |  |
| South | L2 | 1 | 12.18 | 7.14 | 5.04 | 0.414 | 6.3 |
| West | T1 | 1 | 12.18 | 7.14 | 5.04 | 0.414 | 6.3 |
| West <br> NorthWes | T1 | 2 | 11.24 | 6.20 | 5.04 | 0.448 | 5.9 |
|  |  | 2 | 11.24 | 6.20 | 5.04 | 0.448 | 5.9 |
| t |  |  |  |  |  |  |  |
| North | R2 | 2 | 11.24 | 6.20 | 5.04 | 0.448 | 5.9 |
| North: SB Commercial |  |  |  |  |  |  |  |
| East | L2 | 1 | 12.56 | 5.43 | 7.13 | 0.568 | 4.6 |
| South | T1 | 1 | 12.56 | 5.43 | 7.13 | 0.568 | 4.6 |
| West <br> NorthWes | R2 | 2 | 11.93 | 4.79 | 7.13 | 0.598 | 4.4 |
|  |  | 2 | 11.93 | 4.79 | 7.13 | 0.598 | 4.4 |
| NorthWest: SB Church |  |  |  |  |  |  |  |
| North <br> East <br> South | L3 | 1 | 14.74 | 10.78 | 3.96 | 0.269 | 9.8 |
|  | L1 | 1 | 14.74 | 10.78 | 3.96 | 0.269 | 9.8 |
|  | R1 | 1 | 14.74 | 10.78 | 3.96 | 0.269 | 9.8 |
|  | West R3 1 14.74 10.78 3.96 0.269 <br> West: EB Winneconne    9.8   |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |
| NorthWes ${ }_{\text {L3 }}$ <br> t |  | 1 | 13.83 | 4.81 | 9.02 | 0.652 | 4.0 |
|  |  |  |  |  |  |  |  |
| North | L2 | 1 | 13.83 | 4.81 | 9.02 | 0.652 | 4.0 |
| East | T1 | 1 | 13.83 | 4.81 | 9.02 | 0.652 | 4.0 |
| East <br> South | T1 | 2 | 13.30 | 4.28 | 9.02 | 0.678 | 3.9 |
|  | R2 | 2 | 13.30 | 4.28 | 9.02 | 0.678 | 3.9 |

Roundabout Capacity Model: US HCM 6

Project: \Imsa-ps.com|fs\Project107\07578107578063|Traffic|SIDRAICommercial-Winneconne RAB Analysis.sip9

## SITE LAYOUT

$\forall$ Site: 1 [Commercial \& Winneconne 5-leg 2042 AM Peak (Site
Folder: 5-leg Alternative)]
Site Category: (None)
Roundabout

Layout pictures are schematic functional drawings reflecting input data. They are not design drawings.


## INPUT VOLUMES

Vehicles and pedestrians per 60 minutes
$\nabla$ Site: 1 [Commercial \& Winneconne 5-leg 2042 AM Peak (Site Folder: 5-leg Alternative)]

Site Category: (None)
Roundabout

Volume Display Method: Total and \%


|  | All MCs | Light Vehicles (LV) | Heavy Vehicles (HV) |
| :--- | :---: | :---: | :---: |
| S: NB Commercial | 680 | 660 | 20 |
| E: WB Winneconne | 419 | 415 | 4 |
| N: SB Commercial | 626 | 601 | 25 |
| NW: SB Church | 93 | 92 | 1 |
| W: EB Winneconne | 898 | 880 | 18 |
| Total | 2716 | 2647 | 69 |

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## LANE SUMMARY

## $\nabla$ Site: 1 [Commercial \& Winneconne 5-leg 2042 AM Peak (Site Folder: 5-leg Alternative)]

Site Category: (None)
Roundabout

| Lane Use and Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | DEMAND FLOWS |  | Cap. <br> veh/h | Deg. Satn v/c | Lane Util. \% | Aver. Delay <br> sec | Level of Service | 95\% BACK OF QUEUE |  | Lane Config | Lane Length ft | Cap. Prob. <br> Adj. Block. <br> \% \% |  |
| South: NB Commercial |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane 1 | 395 | 3.0 | 630 | 0.628 | 100 | 18.0 | LOS C | 4.5 | 116.3 | Full | 1600 | 0.0 | 0.0 |
| Lane $2^{\text {d }}$ | 424 | 3.0 | 675 | 0.628 | 100 | 17.0 | LOS C | 4.5 | 114.8 | Full | 1600 | 0.0 | 0.0 |
| Approach | 819 | 3.0 |  | 0.628 |  | 17.5 | LOS C | 4.5 | 116.3 |  |  |  |  |
| East: WB Winneconne |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane 1 | 239 | 1.0 | 435 | 0.549 | 100 | 20.6 | LOS C | 2.8 | 70.6 | Full | 1600 | 0.0 | 0.0 |
| Lane $2^{\text {d }}$ | 266 | 1.0 | 483 | 0.549 | 100 | 18.9 | LOS C | 2.8 | 69.8 | Full | 1600 | 0.0 | 0.0 |
| Approach | 505 | 1.0 |  | 0.549 |  | 19.7 | LOS C | 2.8 | 70.6 |  |  |  |  |
| North: SB Commercial |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane 1 | 363 | 4.0 | 579 | 0.626 | 100 | 19.2 | LOS C | 4.2 | 108.9 | Full | 1600 | 0.0 | 0.0 |
| Lane $2^{\text {d }}$ | 391 | 4.0 | 625 | 0.626 | 100 | 18.0 | LOS C | 4.2 | 107.7 | Full | 1600 | 0.0 | 0.0 |
| Approach | 754 | 4.0 |  | 0.626 |  | 18.6 | LOS C | 4.2 | 108.9 |  |  |  |  |
| NorthWest: SB Church |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane $1^{\text {d }}$ | 112 | 1.0 | 285 | 0.393 | 100 | 22.6 | LOS C | 1.5 | 38.3 | Full | 1600 | 0.0 | 0.0 |
| Approach | 112 | 1.0 |  | 0.393 |  | 22.6 | LOS C | 1.5 | 38.3 |  |  |  |  |
| West: EB Winneconne |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane 1 | 530 | 2.0 | 871 | 0.609 | 100 | 13.4 | LOS B | 5.7 | 143.7 | Full | 1600 | 0.0 | 0.0 |
| Lane $2^{\text {d }}$ | 552 | 2.0 | 907 | 0.609 | 100 | 13.0 | LOS B | 5.5 | 140.3 | Full | 1600 | 0.0 | 0.0 |
| Approach | 1082 | 2.0 |  | 0.609 |  | 13.2 | LOS B | 5.7 | 143.7 |  |  |  |  |
| Intersection | 3272 | 2.5 |  | 0.628 |  | 16.8 | LOS C | 5.7 | 143.7 |  |  |  |  |

Site Level of Service (LOS) Method: Delay \& v/c (HCM 6). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Roundabout LOS Method: Same as Sign Control.
Lane LOS values are based on average delay and $\mathrm{v} / \mathrm{c}$ ratio (degree of saturation) per lane.
LOS $F$ will result if $\mathrm{v} / \mathrm{c}>1$ irrespective of lane delay value (does not apply for approaches and intersection).
Intersection and Approach LOS values are based on average delay for all lanes (v/c not used as specified in HCM 6).
Roundabout Capacity Model: US HCM 6.
Delay Model: HCM Delay Formula (Geometric Delay is not included).
Queue Model: HCM Queue Formula.
Gap-Acceptance Capacity: Traditional M1.
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.
d Dominant lane on roundabout approach

## Approach Lane Flows (veh/h)

South: NB Commercial

| Mov. | L2 | L1 | T1 | R2 | Total | \%HV |  | Deg. | Lane | Prob | Ov. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| From S To Exit: | W | NW | N | E |  |  | Cap. veh/h | Satn v/c |  | $\begin{gathered} \text { SL Ov. } \\ \% \end{gathered}$ | Lane No. |
| Lane 1 | 333 | 5 | 58 | - | 395 | 3.0 | 630 | 0.628 | 100 | NA | NA |


| Lane 2 | - | - | 384 | 40 | 424 | 3.0 | 675 | 0.628 | 100 | NA | NA |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Approach | 333 | 5 | 442 | 40 | 819 | 3.0 |  | 0.628 |  |  |  |
| East: WB Winneconne |  |  |  |  |  |  |  |  |  |  |  |
| Mov. <br> From E To Exit: | L2 S | T1 W | R1 NW | R2 N | Total | \%HV | Cap. veh/h | Deg. Satn v/c | Lane Util. \% | Prob. SL Ov. \% | $\begin{array}{r} \text { Ov. } \\ \text { Lane } \\ \text { No. } \end{array}$ |
| Lane 1 | 58 | 181 | - | - | 239 | 1.0 | 435 | 0.549 | 100 | NA | NA |
| Lane 2 | - | 252 | 7 | 6 | 266 | 1.0 | 483 | 0.549 | 100 | NA | NA |
| Approach | 58 | 434 | 7 | 6 | 505 | 1.0 |  | 0.549 |  |  |  |
| North: SB Commercial |  |  |  |  |  |  |  |  |  |  |  |
| Mov. <br> From N To Exit: | L2 E | T1 S | R2 W | R3 <br> NW | Total | \%HV | Cap. veh/h | Deg. Satn v/c | Lane Util. \% | Prob. SL Ov. \% | $\begin{aligned} & \text { Ov. } \\ & \text { Lane } \\ & \text { No. } \end{aligned}$ |
| Lane 1 | 2 | 360 | - | - | 363 | 4.0 | 579 | 0.626 | 100 | NA | NA |
| Lane 2 | - | 19 | 366 | 6 | 391 | 4.0 | 625 | 0.626 | 100 | NA | NA |
| Approach | 2 | 380 | 366 | 6 | 754 | 4.0 |  | 0.626 |  |  |  |
| NorthWest: SB Church |  |  |  |  |  |  |  |  |  |  |  |
| Mov. <br> From NW <br> To Exit: | L3 N | L1 E | R1 S | R3 W | Total | \%HV | Cap. veh/h | Deg. Satn v/c | Lane Util. \% | Prob. SL Ov. \% | $\begin{gathered} \text { Ov. } \\ \text { Lane } \\ \text { No. } \end{gathered}$ |
| Lane 1 | 1 | 14 | 13 | 83 | 112 | 1.0 | 285 | 0.393 | 100 | NA | NA |
| Approach | 1 | 14 | 13 | 83 | 112 | 1.0 |  | 0.393 |  |  |  |
| West: EB Winneconne |  |  |  |  |  |  |  |  |  |  |  |
| Mov. From W To Exit: | L3 NW | L2 N | T1 E | R2 S | Total | \%HV | Cap. veh/h | Deg. Satn v/c | Lane Util. \% | Prob. SL Ov. \% | $\begin{gathered} \text { Ov. } \\ \text { Lane } \\ \text { No. } \end{gathered}$ |
| Lane 1 | 55 | 383 | 91 | - | 530 | 2.0 | 871 | 0.609 | 100 | NA | NA |
| Lane 2 | - | - | 263 | 289 | 552 | 2.0 | 907 | 0.609 | 100 | NA | NA |
| Approach | 55 | 383 | 354 | 289 | 1082 | 2.0 |  | 0.609 |  |  |  |
| Total \%HV Deg.Satn (v/c) |  |  |  |  |  |  |  |  |  |  |  |
| Intersection | 3272 | 2.5 |  | 0.628 |  |  |  |  |  |  |  |

Lane flow rates given in this report are based on the arrival flow rates subject to upstream capacity constraint where applicable.

| Merge Analysis |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{array}{r} \text { Exit } \\ \text { Lane } \\ \text { Number } \end{array}$ |  | Critical Gap sec | Follow-up Lane Headway Flow Rate sec veh/h | Capacity <br> veh/h | Deg. Min. Satn Delay <br> v/c sec | Merge Delay <br> sec |
| South Exit: NB Commercial Merge Type: Not Applied |  |  |  |  |  |  |
| Full Length Lane 1 <br> Full Length Lane 2 | Merge Analysis not applied. <br> Merge Analysis not applied. |  |  |  |  |  |
| East Exit: WB Winneconne Merge Type: Not Applied |  |  |  |  |  |  |
| Full Length Lane 1 <br> Full Length Lane 2 | Merge Analysis not applied. <br> Merge Analysis not applied. |  |  |  |  |  |
| North Exit: SB Commercial Merge Type: Not Applied |  |  |  |  |  |  |
| Full Length Lane 1 | Merge Analysis not applied. |  |  |  |  |  |


| Full Length Lane | 2 | Merge Analysis not applied. |
| :--- | :--- | :--- |
| NorthWest Exit: SB Church <br> Merge Type: Not Applied |  |  |
| Full Length Lane | 1 | Merge Analysis not applied. |
| West Exit: EB Winneconne <br> Merge Type: Not Applied |  |  |
| Full Length Lane | 1 | Merge Analysis not applied. |
| Full Length Lane | 2 | Merge Analysis not applied. |

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## ROUNDABOUT ANALYSIS

$\Rightarrow$ Site: 1 [Commercial \& Winneconne 5-leg 2042 AM Peak (Site
Folder: 5-leg Alternative)]

Site Category: (None)
Roundabout

| Roundabout Basic Parameters |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Location | Name | Central Island Diam | Circ | Insc Diam | Entry Radius | Entry Angle | $\begin{aligned} & \text { Circ } \\ & \text { Lanes } \end{aligned}$ | Entry Lanes | Av.Entry Lane Width | App. Dist | Prop Queued Upstr Signal | Extra Bunching |
|  |  | ft | ft | ft | ft | 。 |  |  | ft | ft |  | \% |
| South | NB | 120.00 * | $30.00{ }^{*}$ | $180.0{ }^{*}$ | $85.0{ }^{*}$ | $20.0{ }^{*}$ | 2 | 2 | $13.00{ }^{*}$ | 1600.0 | $N A^{5}$ | 0.0 |
| East | Commercial WB | 120.00 * | 30.00 * | $180.0{ }^{*}$ | $85.0{ }^{*}$ | $20.0{ }^{*}$ | 2 | 2 | 13.00 | 1600.0 | $N A^{5}$ | 0.0 |
| North | Winneconne SB <br> Commercial | $120.0{ }^{*}$ | $30.00{ }^{*}$ | $180.0{ }^{*}$ | $85.0{ }^{*}$ | $20.0{ }^{*}$ | 2 | 2 | $13.00{ }^{*}$ | 1600.0 | $N A^{5}$ | 0.0 |
| NorthWestSB Church |  | ${ }_{120.00}{ }^{*}$ | $30.00{ }^{*}$$30.00^{*}$ | 180.0180.0 | 85.085.0 | 20.020.0 | 2 | 1 | $\begin{aligned} & 13.00^{*} \\ & 13.00^{*} \end{aligned}$ | 1600.01600.0 | $N A^{5}$ | 0.0 |
| West | EB |  |  |  |  |  |  |  |  |  | $N A^{5}$ | 0.0 |

Roundabout Capacity Model: US HCM 6
5 Not Applicable (single Site analysis or unconnected Site in Network analysis).

* These parameters do not affect estimated capacity values in the HCM 6 Capacity Model.

| Roundabout Entry and Circulating / Exiting Stream Parameters |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| To Turn Approach | Lane <br> No | Lane Type | Opng Flow veh/h | Opng Flow pcu/h | InBunch Hdwy sec | Prop. | Cap Const Effect | Priority Sharing | $\begin{gathered} \text { OD } \\ \text { Factor } \end{gathered}$ | HVE for Entry | Critica [ Hdwy <br> sec | Gap Dist ] | Followup Hdwy sec |
| South: NB Commercial <br> Model Calibration Factor (HCM 6): 1.00 <br> Entry/Circ Flow Adj (HCM 6): None |  |  |  |  |  |  |  |  |  |  |  |  |  |
| West L2 | 1 | Subdom. | 811 | 827 | 0.00 | 0.000 | No | No | - | 1.03 | 4.60 | 141.4 | 2.60 |
| NorthWes L1 <br> t | 1 | Subdom. | 811 | 827 | 0.00 | 0.000 | No | No | - | 1.03 | 4.60 | 141.4 | 2.60 |
| North T1 | 1 | Subdom. | 811 | 827 | 0.00 | 0.000 | No | No | - | 1.03 | 4.60 | 141.4 | 2.60 |
| North T1 | 2 | Dominant | 811 | 827 | 0.00 | 0.000 | No | No | - | 1.03 | 4.30 | 132.1 | 2.60 |
| East R2 | 2 | Dominant | 811 | 827 | 0.00 | 0.000 | No | No | - | 1.03 | 4.30 | 132.1 | 2.60 |
| East: WB Winneconne <br> Model Calibration Factor (HCM 6): 1.00 <br> Entry/Circ Flow Adj (HCM 6): None |  |  |  |  |  |  |  |  |  |  |  |  |  |
| South L2 | 1 | Subdom. | 1219 | 1251 | 0.00 | 0.000 | No | No | - | 1.01 | 4.60 | 136.8 | 2.60 |
| West T1 | 1 | Subdom. | 1219 | 1251 | 0.00 | 0.000 | No | No | - | 1.01 | 4.60 | 136.8 | 2.60 |
| West T1 | 2 | Dominant | 1219 | 1251 | 0.00 | 0.000 | No | No | - | 1.01 | 4.30 | 127.8 | 2.60 |
| NorthWes R1 <br> t | 2 | Dominant | 1219 | 1251 | 0.00 | 0.000 | No | No | - | 1.01 | 4.30 | 127.8 | 2.60 |
| North R2 | 2 | Dominant | 1219 | 1251 | 0.00 | 0.000 | No | No | - | 1.01 | 4.30 | 127.8 | 2.60 |
| North: SB Commercial <br> Model Calibration Factor (HCM 6): 1.00 <br> Entry/Circ Flow Adj (HCM 6): None |  |  |  |  |  |  |  |  |  |  |  |  |  |
| East L2 | 1 | Subdom. | 892 | 908 | 0.00 | 0.000 | No | No | - | 1.04 | 4.60 | 145.1 | 2.60 |
| South T1 | 1 | Subdom. | 892 | 908 | 0.00 | 0.000 | No | No | - | 1.04 | 4.60 | 145.1 | 2.60 |
| South T1 | 2 | Dominant | 892 | 908 | 0.00 | 0.000 | No | No | - | 1.04 | 4.30 | 135.5 | 2.60 |
| West R2 | 2 | Dominant | 892 | 908 | 0.00 | 0.000 | No | No | - | 1.04 | 4.30 | 135.5 | 2.60 |
| NorthWes R3 | 2 | Dominant | 892 | 908 | 0.00 | 0.000 | No | No | - | 1.04 | 4.30 | 135.5 | 2.60 |


| North <br> Model <br> Entry/C |  |  | (HCM 6): 1 <br> 6): None |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| North | L3 | 1 | Dominant | 1572 | 1617 | 0.00 | 0.000 | No | No | - | 1.01 | 4.80 | 160.7 | 2.60 |
| East | L1 | 1 | Dominant | 1572 | 1617 | 0.00 | 0.000 | No | No | - | 1.01 | 4.80 | 160.7 | 2.60 |
| South | R1 | 1 | Dominant | 1572 | 1617 | 0.00 | 0.000 | No | No | - | 1.01 | 4.80 | 160.7 | 2.60 |
| West | R3 | 1 | Dominant | 1572 | 1617 | 0.00 | 0.000 | No | No | - | 1.01 | 4.80 | 160.7 | 2.60 |
| West: <br> Model <br> Entry/C | Wi <br> libra Flo | $\mathrm{Fa}$ | (HCM 6): 1 <br> 6): None |  |  |  |  |  |  |  |  |  |  |  |
| NorthW <br> t |  | 1 | Subdom. | 469 | 485 | 0.00 | 0.000 | No | No | - | 1.02 | 4.60 | 166.6 | 2.60 |
| North | L2 | 1 | Subdom. | 469 | 485 | 0.00 | 0.000 | No | No | - | 1.02 | 4.60 | 166.6 | 2.60 |
| East | T1 | 1 | Subdom. | 469 | 485 | 0.00 | 0.000 | No | No | - | 1.02 | 4.60 | 166.6 | 2.60 |
| East | T1 | 2 | Dominant | 469 | 485 | 0.00 | 0.000 | No | No | - | 1.02 | 4.30 | 155.7 | 2.60 |
| South | R2 | 2 | Dominant | 469 | 485 | 0.00 | 0.000 | No | No | - | 1.02 | 4.30 | 155.7 | 2.60 |

Roundabout Capacity Model: US HCM 6

| Circulating Lane Flow Rates |  |  |  |
| :---: | :---: | :---: | :---: |
| Circ. <br> Lane <br> No | Circulating Flow Rate |  |  |
| South: NB Commercial |  |  |  |
| Lane 1 | 548 | 559 | 67.6 |
| Lane 2 | 263 | 268 | 32.4 |
| Approach | 811 | 827 |  |
| East: WB Winneconne |  |  |  |
| Lane 1 | 835 | 856 | 68.4 |
| Lane 2 | 384 | 396 | 31.6 |
| Approach | 1219 | 1251 |  |
| North: SB Commercial |  |  |  |
| Lane 1 | 239 | 242 | 26.6 |
| Lane 2 | 652 | 666 | 73.4 |
| Approach | 892 | 908 |  |
| NorthWest: SB Church |  |  |  |
| Lane 1 | 934 | 961 | 59.4 |
| Lane 2 | 638 | 656 | 40.6 |
| Approach | 1572 | 1617 |  |
| West: EB Winneconne |  |  |  |
| Lane 1 | 449 | 465 | 95.9 |
| Lane 2 | 19 | 20 | 4.1 |
| Approach | 469 | 485 |  |

Roundabout Capacity Model: The US HCM 6 roundabout capacity model option is in use.
This model considers only the total circulating flow and not the flow rates in individual circulating lanes.
To model the effects of flow distribution in circulating lanes on the entry capacity results, you should use the SIDRA Standard roundabout capacity model.

Gap Acceptance Cycle Parameters (Lanes)

| Opposed | Cycle | Blocked | Unblocked | Unblocked | Minimum |
| :--- | ---: | ---: | ---: | ---: | ---: |
| Lane | Time | Time | Time | Time Ratio | Delay <br> sec |
| South: NB Commercial | sec | sec |  |  |  |


| 1 | 12.07 | 6.41 | 5.65 | 0.468 | 5.7 |
| :--- | ---: | :--- | :--- | :--- | :--- |
| 2 | 11.26 | 5.60 | 5.65 | 0.502 | 5.3 |
| East: WB Winneconne |  |  |  |  |  |
| 1 | 13.16 | 8.98 | 4.18 | 0.317 | 8.3 |
| 2 | 11.84 | 7.67 | 4.18 | 0.353 | 7.4 |
| North: SB Commercial |  |  |  |  |  |
| 1 | 12.10 | 6.84 | 5.27 | 0.435 | 6.2 |
| 2 | 11.22 | 5.95 | 5.27 | 0.469 | 5.8 |
| NorthWest: SB Church |  |  |  |  |  |
| 1 | 16.98 | 13.45 | 3.53 | 0.208 | 12.6 |
| West: EB Winneconne |  |  |  |  |  |
| 1 | 13.61 | 4.88 | 8.73 | 0.641 | 4.1 |
| 2 | 13.07 | 4.34 | 8.73 | 0.668 | 4.0 |

Roundabout Capacity Model: US HCM 6


Roundabout Capacity Model: US HCM 6

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## SITE LAYOUT

$\nabla$ Site: 1 [Commercial \& Winneconne 5-leg 2042 PM Peak (Site
Folder: 5-leg Alternative)]
Site Category: (None)
Roundabout

Layout pictures are schematic functional drawings reflecting input data. They are not design drawings.


## INPUT VOLUMES

Vehicles and pedestrians per 60 minutes
© Site: 1 [Commercial \& Winneconne 5-leg 2042 PM Peak (Site Folder: 5 -leg Alternative)]

Site Category: (None)
Roundabout

Volume Display Method: Total and \%


|  | All MCs | Light Vehicles (LV) | Heavy Vehicles (HV) |
| :--- | :---: | :---: | :---: |
| S: NB Commercial | 651 | 644 | 7 |
| E: WB Winneconne | 424 | 420 | 4 |
| N: SB Commercial | 884 | 875 | 9 |
| NW: SB Church | 68 | 67 | 1 |
| W: EB Winneconne | 941 | 932 | 9 |
| Total | 2968 | 2938 | 30 |

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## LANE SUMMARY

## $\nabla$ Site: 1 [Commercial \& Winneconne 5-leg 2042 PM Peak (Site Folder: 5-leg Alternative)]

Site Category: (None)
Roundabout

| Lane Use and Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | $\begin{aligned} & \text { ND } \\ & \text { NS } \\ & \text { HV ] } \\ & \% \end{aligned}$ | Cap. <br> veh/h | Deg. Satn <br> v/c | Lane Util. \% | Aver. Delay <br> sec | Level of Service | 95\% <br> [ Veh | OF JE Dist ] ft | Lane Config | Lane Length ft | Cap. Adj. \% | Prob. <br> Block. <br> \% |
| South: NB Commercial |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane 1 | 342 | 1.0 | 666 | 0.514 | 100 | 13.6 | LOS B | 3.1 | 79.2 | Full | 1600 | 0.0 | 0.0 |
| Lane $2^{\text {d }}$ | 366 | 1.0 | 711 | 0.514 | 100 | 12.9 | LOS B | 3.1 | 77.2 | Full | 1600 | 0.0 | 0.0 |
| Approach | 708 | 1.0 |  | 0.514 |  | 13.2 | LOS B | 3.1 | 79.2 |  |  |  |  |
| East: WB Winneconne |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane 1 | 220 | 1.0 | 490 | 0.448 | 100 | 15.4 | LOS C | 2.1 | 53.5 | Full | 1600 | 0.0 | 0.0 |
| Lane $2^{\text {d }}$ | 241 | 1.0 | 538 | 0.448 | 100 | 14.3 | LOS B | 2.1 | 52.2 | Full | 1600 | 0.0 | 0.0 |
| Approach | 461 | 1.0 |  | 0.448 |  | 14.8 | LOS B | 2.1 | 53.5 |  |  |  |  |
| North: SB Commercial |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane 1 | 455 | 1.0 | 708 | 0.643 | $96{ }^{5}$ | 17.0 | LOS C | 5.3 | 134.4 | Full | 1600 | 0.0 | 0.0 |
| Lane $2^{\text {d }}$ | 505 | 1.0 | 753 | 0.672 | 100 | 17.3 | LOS C | 5.9 | 148.3 | Full | 1600 | 0.0 | 0.0 |
| Approach | 961 | 1.0 |  | 0.672 |  | 17.2 | LOS C | 5.9 | 148.3 |  |  |  |  |
| NorthWest: SB Church |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane $1^{\text {d }}$ | 74 | 1.0 | 295 | 0.250 | 100 | 17.5 | LOS C | 0.9 | 21.8 | Full | 1600 | 0.0 | 0.0 |
| Approach | 74 | 1.0 |  | 0.250 |  | 17.5 | LOS C | 0.9 | 21.8 |  |  |  |  |
| West: EB Winneconne |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane 1 | 500 | 1.0 | 830 | 0.602 | 100 | 13.7 | LOS B | 5.3 | 132.7 | Full | 1600 | 0.0 | 0.0 |
| Lane $2^{\text {d }}$ | 523 | 1.0 | 869 | 0.602 | 100 | 13.2 | LOS B | 5.1 | 129.7 | Full | 1600 | 0.0 | 0.0 |
| Approach | 1023 | 1.0 |  | 0.602 |  | 13.4 | LOS B | 5.3 | 132.7 |  |  |  |  |
| Intersection | 3226 | 1.0 |  | 0.672 |  | 14.8 | LOS B | 5.9 | 148.3 |  |  |  |  |

Site Level of Service (LOS) Method: Delay \& v/c (HCM 6). Site LOS Method is specified in the Parameter Settings dialog (Site tab). Roundabout LOS Method: Same as Sign Control.
Lane LOS values are based on average delay and $\mathrm{v} / \mathrm{c}$ ratio (degree of saturation) per lane.
LOS $F$ will result if $\mathrm{v} / \mathrm{c}>1$ irrespective of lane delay value (does not apply for approaches and intersection).
Intersection and Approach LOS values are based on average delay for all lanes (v/c not used as specified in HCM 6).
Roundabout Capacity Model: US HCM 6.
Delay Model: HCM Delay Formula (Geometric Delay is not included).
Queue Model: HCM Queue Formula.
Gap-Acceptance Capacity: Traditional M1.
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.
5 Lane under-utilisation found by the program
d Dominant lane on roundabout approach

## Approach Lane Flows (veh/h)

South: NB Commercial

| Mov. | L2 | L1 | T1 | R2 | Total | \%HV |  | Deg. | Lane | Prob. | Ov. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| From S | W | NW | N | E |  |  | Cap. veh/h | Satn v/c | Util. | SL Ov. | Lane No. |


| Lane 1 | 174 | 4 | 164 | - | 342 | 1.0 | 666 | 0.514 | 100 | NA | NA |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane 2 | - | - | 320 | 46 | 366 | 1.0 | 711 | 0.514 | 100 | NA | NA |
| Approach | 174 | 4 | 484 | 46 | 708 | 1.0 |  | 0.514 |  |  |  |
| East: WB Winneconne |  |  |  |  |  |  |  |  |  |  |  |
| Mov. <br> From E To Exit: | L2 S | T1 W | R1 NW | R2 N | Total | \%HV | Cap. veh/h | Deg. Satn v/c | Lane Util. \% | Prob. SL Ov. \% | $\begin{gathered} \text { Ov. } \\ \text { Lane } \\ \text { No. } \end{gathered}$ |
| Lane 1 | 67 | 152 | - | - | 220 | 1.0 | 490 | 0.448 | 100 | NA | NA |
| Lane 2 | - | 223 | 10 | 9 | 241 | 1.0 | 538 | 0.448 | 100 | NA | NA |
| Approach | 67 | 375 | 10 | 9 | 461 | 1.0 |  | 0.448 |  |  |  |
| North: SB Commercial |  |  |  |  |  |  |  |  |  |  |  |
| Mov. <br> From N To Exit: | L2 E | T1 S | R2 W | R3 NW | Total | \%HV | Cap. veh/h | Deg. Satn v/c | Lane Util. \% | Prob. SL Ov. \% | $\begin{gathered} \text { Ov. } \\ \text { Lane } \\ \text { No. } \end{gathered}$ |
| Lane 1 | 16 | 439 | - | - | 455 | 1.0 | 708 | 0.643 | $96^{5}$ | NA | NA |
| Lane 2 | - | - | 492 | 13 | 505 | 1.0 | 753 | 0.672 | 100 | NA | NA |
| Approach | 16 | 439 | 492 | 13 | 961 | 1.0 |  | 0.672 |  |  |  |
| NorthWest: SB Church |  |  |  |  |  |  |  |  |  |  |  |
| Mov. <br> From NW <br> To Exit: | L3 N | L1 E | R1 S | R3 W | Total | \%HV | Cap. veh/h | Deg. Satn v/c | Lane Util. \% | Prob. SL Ov. \% | $\begin{gathered} \text { Ov. } \\ \text { Lane } \\ \text { No. } \end{gathered}$ |
| Lane 1 | 1 | 9 | 10 | 54 | 74 | 1.0 | 295 | 0.250 | 100 | NA | NA |
| Approach | 1 | 9 | 10 | 54 | 74 | 1.0 |  | 0.250 |  |  |  |
| West: EB Winneconne |  |  |  |  |  |  |  |  |  |  |  |
| Mov. <br> From W To Exit: | L3 NW | L2 N | T1 E | R2 S | Total | \%HV | Cap. veh/h | Deg. Satn v/c | Lane Util. \% | Prob. SL Ov. \% | Ov. Lane No. |
| Lane 1 | 83 | 366 | 51 | - | 500 | 1.0 | 830 | 0.602 | 100 | NA | NA |
| Lane 2 | - | - | 255 | 268 | 523 | 1.0 | 869 | 0.602 | 100 | NA | NA |
| Approach | 83 | 366 | 305 | 268 | 1023 | 1.0 |  | 0.602 |  |  |  |
| Total \%HV Deg.Satn (v/c) |  |  |  |  |  |  |  |  |  |  |  |
| Intersection | 3226 | 1.0 |  | 0.672 |  |  |  |  |  |  |  |

Lane flow rates given in this report are based on the arrival flow rates subject to upstream capacity constraint where applicable.
5 Lane under-utilisation found by the program

| Merge Analysis |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Exit Lane Number | Short Percent Opposing Lane Opng in Flow Rate Length Lane $\mathrm{ft} \quad \%$ veh/h pcu/h | Critical Gap sec | Follow-up Lane Headway Flow Rate sec veh/h | Capacity <br> veh/h |  |  | Merge Delay <br> sec |
| South Exit: NB Commercial Merge Type: Not Applied |  |  |  |  |  |  |  |
| Full Length Lane 1 <br> Full Length Lane 2 | Merge Analysis not applied. <br> Merge Analysis not applied. |  |  |  |  |  |  |
| East Exit: WB Winneconne Merge Type: Not Applied |  |  |  |  |  |  |  |
| Full Length Lane 1 <br> Full Length Lane 2 | Merge Analysis not applied. <br> Merge Analysis not applied. |  |  |  |  |  |  |
| North Exit: SB Commercial |  |  |  |  |  |  |  |


| Merge Type: Not Applied |  |  |
| :--- | ---: | :--- |
| Full Length Lane | 1 | Merge Analysis not applied. |
| Full Length Lane | 2 | Merge Analysis not applied. |
| NorthWest Exit: SB Church |  |  |
| Merge Type: Not Applied |  |  |
| Full Length Lane | 1 | Merge Analysis not applied. |
| West Exit: EB Winneconne |  |  |
| Merge Type: Not Applied |  |  |
| Full Length Lane | 1 | Merge Analysis not applied. |
| Full Length Lane | 2 | Merge Analysis not applied. |

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## ROUNDABOUT ANALYSIS

## $\nabla$ Site: 1 [Commercial \& Winneconne 5-leg 2042 PM Peak (Site <br> Folder: 5-leg Alternative)]

Site Category: (None)
Roundabout

| Roundabout Basic Parameters |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Location | Name | Central Island Diam | Circ Width | Insc Diam | Entry Radius | Entry Angle | Circ Lanes | Entry Lanes | Av.Entry Lane Width | App. Dist | Prop Queued Upstr Signal | Extra Bunching |
|  |  | ft | ft | ft | ft | . |  |  | f | ft |  | \% |
| South |  | $120.00{ }^{*}$ | 30.00 * | $180.0{ }^{*}$ | $85.0{ }^{*}$ | $20.0{ }^{*}$ | 2 | 2 | $13.00{ }^{*}$ | 1600.0 | $N A^{5}$ | 0.0 |
|  |  | $120.00{ }^{*}$ | $30.00{ }^{*}$ | $180.0{ }^{*}$ | 85.0 * | 20.0 * | 2 | 2 | $13.00^{*}$ | 1600.0 | $N A^{5}$ | 0.0 |
| North | Winnec | $120.00{ }^{*}$ | 30.00 * | $180.0{ }^{*}$ | $85.0{ }^{*}$ | $20.0{ }^{*}$ | 2 | 2 | $13.00{ }^{*}$ | 1600.0 | $N A^{5}$ | 0.0 |
|  | Comm |  |  |  |  |  |  |  |  |  |  |  |
| NorthWestSB Church West EB |  | 120.00 * | 30.00 * | $180.0{ }^{*}$ | 85.0 * | 20.0 * | 2 | 1 | 13.00 * | 1600.0 | $N A^{5}$ | 0.0 |
|  |  | $120.00{ }^{*}$ | 30.00 * | $180.0{ }^{*}$ | $85.0{ }^{*}$ | 20.0 * | 2 | 2 | $13.00{ }^{*}$ | 1600.0 | $N A^{5}$ | 0.0 |

Roundabout Capacity Model: US HCM 6
5 Not Applicable (single Site analysis or unconnected Site in Network analysis).

* These parameters do not affect estimated capacity values in the HCM 6 Capacity Model.

| Roundabout Entry and Circulating / Exiting Stream Parameters |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { To Turn } \\ & \text { Approach } \end{aligned}$ | Lane No | Lane Type | Opng Flow veh/h | Opng Flow <br> pcu/h | InBunch Hdwy sec | Prop. | Cap Const Effect | Priority Sharing | $\begin{gathered} \text { OD } \\ \text { Factor } \end{gathered}$ | HVE for Entry | Critical [ Hdwy <br> sec | Gap Dist ] ft | Follow- <br> up <br> Hdwy <br> sec |
| South: NB Commercial <br> Model Calibration Factor (HCM 6): 1.00 <br> Entry/Circ Flow Adj (HCM 6): None |  |  |  |  |  |  |  |  |  |  |  |  |  |
| West L2 | 1 | Subdom. | 780 | 788 | 0.00 | 0.000 | No | No | - | 1.01 | 4.60 | 138.6 | 2.60 |
| NorthWes L1 <br> t | 1 | Subdom. | 780 | 788 | 0.00 | 0.000 | No | No | - | 1.01 | 4.60 | 138.6 | 2.60 |
| North T1 | 1 | Subdom. | 780 | 788 | 0.00 | 0.000 | No | No | - | 1.01 | 4.60 | 138.6 | 2.60 |
| North T1 | 2 | Dominant | 780 | 788 | 0.00 | 0.000 | No | No | - | 1.01 | 4.30 | 129.5 | 2.60 |
| East R2 | 2 | Dominant | 780 | 788 | 0.00 | 0.000 | No | No | - | 1.01 | 4.30 | 129.5 | 2.60 |
| East: WB Winneconne <br> Model Calibration Factor (HCM 6): 1.00 <br> Entry/Circ Flow Adj (HCM 6): None |  |  |  |  |  |  |  |  |  |  |  |  |  |
| South L2 | 1 | Subdom. | 1112 | 1123 | 0.00 | 0.000 | No | No | - | 1.01 | 4.60 | 141.3 | 2.60 |
| West T1 | 1 | Subdom. | 1112 | 1123 | 0.00 | 0.000 | No | No | - | 1.01 | 4.60 | 141.3 | 2.60 |
| West T1 | 2 | Dominant | 1112 | 1123 | 0.00 | 0.000 | No | No | - | 1.01 | 4.30 | 132.0 | 2.60 |
| NorthWes R1 t | 2 | Dominant | 1112 | 1123 | 0.00 | 0.000 | No | No | - | 1.01 | 4.30 | 132.0 | 2.60 |
| North R2 | 2 | Dominant | 1112 | 1123 | 0.00 | 0.000 | No | No | - | 1.01 | 4.30 | 132.0 | 2.60 |
| North: SB Commercial <br> Model Calibration Factor (HCM 6): 1.00 <br> Entry/Circ Flow Adj (HCM 6): None |  |  |  |  |  |  |  |  |  |  |  |  |  |
| East L2 | 1 | Subdom. | 713 | 720 | 0.00 | 0.000 | No | No | - | 1.01 | 4.60 | 147.9 | 2.60 |
| South T1 | 1 | Subdom. | 713 | 720 | 0.00 | 0.000 | No | No | - | 1.01 | 4.60 | 147.9 | 2.60 |
| West R2 | 2 | Dominant | 713 | 720 | 0.00 | 0.000 | No | No | - | 1.01 | 4.30 | 138.2 | 2.60 |
| NorthWes R3 <br> t | 2 | Dominant | 713 | 720 | 0.00 | 0.000 | No | No | - | 1.01 | 4.30 | 138.2 | 2.60 |
| NorthWest: SB Church |  |  |  |  |  |  |  |  |  |  |  |  |  |


| Model Calibration Factor (HCM 6): 1.00 Entry/Circ Flow Adj (HCM 6): None |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| North | L3 | 1 | Dominant | 1564 | 1580 | 0.00 | 0.000 | No | No | - | 1.01 | 4.80 | 163.6 | 2.60 |
| East | L1 | 1 | Dominant | 1564 | 1580 | 0.00 | 0.000 | No | No | - | 1.01 | 4.80 | 163.6 | 2.60 |
| South | R1 | 1 | Dominant | 1564 | 1580 | 0.00 | 0.000 | No | No | - | 1.01 | 4.80 | 163.6 | 2.60 |
| West | R3 | 1 | Dominant | 1564 | 1580 | 0.00 | 0.000 | No | No | - | 1.01 | 4.80 | 163.6 | 2.60 |
| West: EB Winneconne <br> Model Calibration Factor (HCM 6): 1.00 <br> Entry/Circ Flow Adj (HCM 6): None |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| NorthW <br> t | L3 | 1 | Subdom. | 542 | 548 | 0.00 | 0.000 | No | No | - | 1.01 | 4.60 | 166.0 | 2.60 |
| North | L2 | 1 | Subdom. | 542 | 548 | 0.00 | 0.000 | No | No | - | 1.01 | 4.60 | 166.0 | 2.60 |
| East | T1 | 1 | Subdom. | 542 | 548 | 0.00 | 0.000 | No | No | - | 1.01 | 4.60 | 166.0 | 2.60 |
| East | T1 | 2 | Dominant | 542 | 548 | 0.00 | 0.000 | No | No | - | 1.01 | 4.30 | 155.1 | 2.60 |
| South | R2 | 2 | Dominant | 542 | 548 | 0.00 | 0.000 | No | No | - | 1.01 | 4.30 | 155.1 | 2.60 |

Roundabout Capacity Model: US HCM 6

| Circulating Lane Flow Rates |  |  |  |
| :---: | :---: | :---: | :---: |
| Circ. <br> Lane <br> No | Circulating Flow Rate |  |  |
|  | veh/h | pcu/h | Percent |
| South: NB Commercial |  |  |  |
| Lane 1 | 526 | 531 | 67.4 |
| Lane 2 | 255 | 257 | 32.6 |
| Approach | 780 | 788 |  |
| East: WB Winneconne |  |  |  |
| Lane 1 | 792 | 800 | 71.2 |
| Lane 2 | 320 | 323 | 28.8 |
| Approach | 1112 | 1123 |  |
| North: SB Commercial |  |  |  |
| Lane 1 | 220 | 222 | 30.8 |
| Lane 2 | 493 | 498 | 69.2 |
| Approach | 713 | 720 |  |
| NorthWest: SB Church |  |  |  |
| Lane 1 | 849 | 857 | 54.3 |
| Lane 2 | 715 | 722 | 45.7 |
| Approach | 1564 | 1580 |  |
| West: EB Winneconne |  |  |  |
| Lane 1 | 542 | 548 | 100.0 |
| Lane 2 | 0 | 0 | 0.0 |
| Approach | 542 | 548 |  |

Roundabout Capacity Model: The US HCM 6 roundabout capacity model option is in use.
This model considers only the total circulating flow and not the flow rates in individual circulating lanes.
To model the effects of flow distribution in circulating lanes on the entry capacity results, you should use the SIDRA Standard roundabout capacity model.

| Gap Acceptance Cycle Parameters (Lanes) |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: |
| Opposed <br> Lane | Cycle <br> Time <br> sec | Blocked <br> Time <br> sec | Unblocked <br> Time <br> sec | Unblocked <br> Time Ratio | Minimum <br> Delay <br> sec |
| South: NB Commercial |  |  |  |  |  |
| 1 | 12.09 | 6.22 | 5.87 | 0.485 | 5.4 |


| 2 | 11.31 | 5.45 | 5.87 | 0.519 | 5.1 |
| :--- | :--- | :--- | :--- | :--- | :--- |
| East: WB Winneconne |  |  |  |  |  |
| 1 | 12.62 | 8.11 | 4.51 | 0.357 | 7.4 |
| 2 | 11.48 | 6.98 | 4.51 | 0.392 | 6.7 |
| North: SB Commercial |  |  |  |  |  |
| 1 | 12.19 | 5.89 | 6.30 | 0.517 | 5.1 |
| 2 | 11.48 | 5.18 | 6.30 | 0.549 | 4.8 |
| NorthWest: SB Church |  |  |  |  |  |
| 1 | 16.62 | 13.04 | 3.58 | 0.215 | 12.2 |
| West: EB Winneconne |  |  |  |  |  |
| 1 | 13.01 | 5.14 | 7.87 | 0.605 | 4.3 |
| 2 | 12.42 | 4.55 | 7.87 | 0.634 | 4.1 |

Roundabout Capacity Model: US HCM 6


Roundabout Capacity Model: US HCM 6

To: DOT ICE Review<br>From: M SA Professional Services, Inc.<br>Date: 12/1/2022<br>RE: n/a<br>Other<br>STH 114 (Winneconne Avenue) at STH 114 (Commercial Street)<br>City of Neenah, Winnebago County<br>Northeast Region

## Project Description:

The City of Neenah has identified the intersection of STH 144 (Winneconne Avenue) at STH 144 (Commercial Street) as a target for improvements due to ongoing operational/ capacity and safety issues. The project location is shown in Attachment 2.

STH 114, north of the intersection (Commercial Street), is a north-south four-lane urban principal arterial, with a posted speed limit of 25 mph . Sidewalks are present on both sides of the roadway. Winneconne Avenue, east of the intersection, is primarily a southwest-northeast two-lane urban minor arterial, with a posted speed limit of 25 mph . Sidewalk is only present on the south side of the roadway. Commercial Street, south of the intersection, is a north-south four-lane urban minor arterial, with a posted speed limit of 30 mph . Sidewalk is present on both sides of the roadway. STH 114, west of the intersection (Winneconne Avenue), is a southwest-northeast four-lane urban principal arterial, with a posted speed limit of 30 mph . Sidewalks are present on both sides of the roadway. Parking is restricted within the functional area of the intersections. No bicycle lanes are present on any of the approaches.

Church Street is a north-south two-lane urban collector roadway with a posted speed limit of 25 mph . Sidewalks are present on both sides of the roadway; however, no crossings are provided where Church Street intersects Winneconne Avenue (one block west of the Commercial Street intersection).

The intersection of Winneconne Avenue at Commercial Street is currently traffic signal controlled. The southbound approach contains two lanes: a shared left-turn/through lane and a shared through/rightturn lane. A commercial driveway is present on the east side of the approach, approximately 90 -feet from the intersection. The westbound approach contains two lanes: an exclusive left-turn lane with approximately 90 -feet of dedicated storage and a shared through/right-turn lane. One commercial driveway is located on the south side of the approach, approximately 60 -feet from the intersection. The northbound approach contains two lanes: an exclusive left-turn lane with approximately 190-feet of dedicated storage and a shared through/right-turn lane. Commercial driveways are located on both sides of the road, approximately 100 -feet from the intersection. The eastbound approach contains three lanes: an exclusive left-turn lane with approximately 65 -feet of dedicated storage (however, enhanced lane separation markings extend approximately 350 -feet further upstream - for a total length of 415feet), an exclusive through lane, and a channelized exclusive right-turn lane, with approximately 145feet of dedicated storage. The channelized right-turn lane is controlled by a Yield sign. The Church Street intersection is on the north side of this approach, approximately 100 -feet from the intersection. A
commercial driveway is located on the south side of this approach, approximately 185 -feet from the intersection.

The area is surrounded by mostly commercial developments, with residential development surrounding the commercial development. Valley Transit operates bus routes through the area. Routes currently use all approaches except for the east leg of the intersection. Bus routes are also shown to use Church Street as well.

Due to the pandemic, traffic counts were re-used from the 2018 traffic study, which included the Winneconne Avenue at Commercial Street intersection. Traffic was projected to 2022 and 2042 using growth rates provided by WisDOT planning-level forecast data. Site 700227 along STH 114 in the City of Neenah was used for establishing the growth rate ( $0.87 \%$ ). The base count data and projected volumes are included in Attachment 3. These volumes were utilized to complete preliminary operational analyses for the intersection.

## Description of Altematives:

Based on alternatives reviewed as part of initial brainstorming, a modified traffic signal control or a roundabout are the most reasonable alternatives, as shown in Attachment 4. Given the proximity of the Church Street intersection to Commercial Street, two roundabout alternatives will be considered:

1. Replacing the existing traffic signal with a multilane roundabout and retaining the T-intersection of Winneconne Avenue at Church Street
2. Replacing the existing traffic signal with a five-leg multilane roundabout which incorporates Church Street into the intersection with Winneconne Avenue and Commercial Street.

## Safety Considerations:

Over the 5-year period of 2017-2021, 34 crashes were reported at the intersection. This translates to a rate of approximately 0.83 crashes per million entering vehicles or approximately 6.8 crashes per year. A diagram of the reported crashes for provided in Attachment 5.

Observed Crash History Years: 2017-2021

| Crash Type | Fatal | Injury A | Injury B | Injury C | KABC | PDO | Total |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Rear-End <br> (Front-to-Rear) | 0 | 0 | 0 | 2 | 2 | 14 | 16 |
| Angle <br> (Front-to-Side) | 0 | 0 | 2 | 0 | 2 | 6 | 8 |
| Single Vehicle/Other | 0 | 0 | 3 | 0 | 3 | 1 | 4 |
| Sideswipe <br> (Same Direction) | 0 | 0 | 0 | 0 | 0 | 3 | 3 |
| Head-On <br> (Front-to-Front) | 0 | 0 | 0 | 1 | 1 | 1 | 2 |
| Sideswipe <br> (Opposite Directions) | 0 | 0 | 0 | 0 | 0 | 1 | 1 |
| Total | 0 | 0 | 5 | 3 | 8 | 26 | 34 |

Crash Trends: The intersection has a significant number of front-to-rear crash events, with most occurring on the eastbound approach. The majority of this crash type were property damage only;
however, two were of severity C (possible injury). Front-to-side crash events were the next most common, with no particular approach having a significant number of this crash type. Two of these crashes resulted in severity B (suspected minor injury) magnitude injuries. Three of the single-vehicle crashes resulted in injuries - all severity B (suspected minor injury) magnitude injuries. One of these events involved a pedestrian being struck by a southbound left-turning vehicle; one of the events involved a bicyclist being struck by a southbound right-turning vehicle.

Contributing Factors: W eather may have been a factor in two of the crashes (rain). Road conditions may have been a factor in at least ten crashes: five wet, three snow, one slush, and one ice. Drug impairment was cited in two crashes. Failure to yield was cited in 11 crashes. Distracted driving was identified in nine crashes. Disregard of a red light was cited in three crashes. Speed was cited in two crashes (too fast for conditions). Improper crossing was cited in the crash that involved a pedestrian.

## Operational Considerations:

The existing traffic signal operates with unacceptable level of service (LOS), capacity, and delay during the base year (2022). Queues of 200-300-feet or greater are already observed on all approaches. The southbound right-turn movement is calculated to be near capacity currently. Operations continue to degrade through the 2042 design horizon without any additional improvements.

Traffic Signal Improvements
Lane modifications to the southbound and eastbound approaches combined with signal phasing and timing modifications are shown to provide acceptable operations through the 2042 design horizon.

## Roundabout Improvements

Either a multilane four or five-legged roundabout design are expected to provide acceptable operations through the 2042 design horizon.

Preliminary operational analyses are included in Attachment 6 for the signalized and roundabout alternatives.

## Other Considerations:

Right-of-way (R/W) will need to be acquired regardless of the alternative selected.
A modified traffic signal will require adding a southbound exclusive right-turn lane. The addition of this lane would require R/W to be acquired in the northwest corner of the intersection.

Either roundabout alternative would require a significant amount of R/W to be acquired, including a majority of the parcel in the northwest corner of the intersection (the parcel encompasses the entire block of Winneconne Avenue between Commercial Street and Church Street).

With the close proximity of the Church Street intersection, for safety reasons, southbound left-turns should be restricted from Church Street if the five-leg roundabout is not selected. Due to additional operational deficiencies with the inclusion of a fifth approach to a signalized intersection and considering the existing signal's operational deficiencies, an alternative which ties the Church Street approach into the signalized intersection is not being considered at this time.

## Feasibility of Alternatives:

Preliminary analyses indicate a modified traffic signal or a roundabout (with 4 or 5 legs) would operate acceptably through the 2042 design year. Both alternatives would require R/W to be acquired; however, preliminary reviews indicate that a roundabout would require a full business acquisition.

## Conclusion:

Based on the operational analyses and preliminary R/W needs, both a modified traffic signal and a roundabout ( 4 or 5 legs) are viable alternatives. A Phase II ICE is recommended to further vet the alternatives. As part of the Phase II ICE, the following alternatives will be investigated further:

1. M odified Traffic Signal
2. 4-leg Multilane Roundabout
3. 5-leg M ultilane Roundabout with Inclusion of Church Street

## Attachments:

Attachment 1: ICE Submittal Checklist
Attachment 2: Project Location M ap
Attachment 3: Traffic Volumes
Attachment 4: Phase I: ICE Brainstorming Guide
Attachment 5: Intersection Crash Diagram
Attachment 6: Synchro and SIDRA Output
Note: All Attachments can be found in the appendix of the Phase 2 ICE Report included as part of Attachment A.

Phase I: ICE Brainstorming Guide
Date: 11/22/2022
Project ID: $\mathrm{n} / \mathrm{a}$
Control: Signal
Major Road AADT: 13,300
Minor Road AADT: 10,000



[^0]:    ${ }^{1}$ The Winneconne Avenue approaches are oriented in a southwest to northeast direction, but will be referred to as west and east legs for simplicity of discussion.

[^1]:    ${ }^{1}$ NCHRP Report 672, Roundabouts: An Informational Guide, Second Edition. TRB, 2010.

[^2]:    Additional Queues are 95th-percentile, rounded to the nearest 25 ft ( 25 ft minimum) Information

[^3]:    | Additional | Queues are 95th-percentile, rounded to the nearest 25 ft ( 25 ft minimum) |
    | :--- | :--- | Information

[^4]:    ${ }^{2}$ NCHRP Report 672, Roundabouts: An Informational Guide, Second Edition. TRB, 2010.

[^5]:    Additional Information

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